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Comparison of numerical schemes for the solution of the advective age equation in ice sheets

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ABSTRACT. A one-dimensional model problem for computation of the age field in ice sheets, which is of great importance for dating deep ice cores, is considered. The corresponding partial differential equation (PDE) is of purely advective (hyperbolic) type, which is notoriously difficult to solve numerically. By integrating the PDE over a space–time element in the sense of a finite-volume approach, a general difference equation is constructed from which a hierarchy of solution schemes can be derived. Iteration rules are given explicitly for central differences, first-, second- and third-order (QUICK) upwinding as well as modified TVD–Lax–Friedrichs schemes (TVDLS). The performance of these schemes in terms of convergence and accuracy is discussed. Second-order upwinding, the modified TVDLF scheme with Minmod slope limiter and, with limitations of the accuracy directly at the base, first-order upwinding prove to be the most suitable for numerical age computations in ice-sheet models.

1. INTRODUCTION

In Greenland and Antarctica, several deep ice-core projects have been carried out during recent decades (Camp Century, Dye 3, GRIP and GISP2 in Greenland; Vostok and Byrd Station in Antarctica) or are currently under way (NorthGRIP in Greenland; Dronning Maud Land, Dome C and Dome Fuji in Antarctica). These ice cores reveal a wealth of direct and indirect information on palaeoclimatic conditions such as atmospheric composition, surface temperature and snowfall rate, going back some hundreds of thousands of years, and have therefore greatly improved our knowledge of Earth’s climate and its variability during the Pleistocene and Holocene (e.g. Dansgaard and others, 1993; Petit and others, 1999; Johnsen and others, 2001).

In order to obtain time series of these climatic parameters, proper age–depth relations for the ice and the boreholes are required. In the upper parts, these can be established rather precisely by counting annual signals of isotopic composition and impurities downward. However, beyond ages of a few tens of kyr these stratigraphic techniques fail due to layer thinning and diffusion, so flow models are needed to compute age–depth profiles in the lower parts of the boreholes (cf. Johnsen and others, 2001, and references therein).

Applications of the three-dimensional dynamic/thermo-dynamic ice-sheet model SICOPOLIS to compute ages for the Greenland Summit (GRIP/GISP2) region were discussed by Greve (1997) and Greve and others (1998, 1999), and for Dronning Maud Land (where a deep ice core is planned within the European Project for Ice Coring in Antarctica (EPICA)) by Calov and others (1998) and Savvin and others (2000). In these studies, the present state of the Greenland and Antarctic ice sheets was obtained via palaeoclimatic simulations over two glacial/interglacial cycles, and the three-dimensional age field was computed by solving the advective age evolution equation along with the thickness, temperature and flow-velocity equations. A major limitation in those calculations was the need for some artificial diffusion in the vertical direction in order to achieve numerical stability, which requires an unphysical boundary condition for the age at the ice base. Calov and others (1998) show that this leads to a basal boundary layer of $\sim 15\%$ of the ice thickness in which the computed ages are affected by this arbitrary boundary condition and therefore erroneous.

In this study, we consider a simple one-dimensional steady-state approximation for the age computation. This simplification allows an analytical solution for the age–depth relation against which numerical methods can be checked. After showing a general method to construct numerical solution schemes, we discuss a variety of different schemes in terms of their accuracy and convergence properties. The objective is to find out which scheme is most suitable for applications in full three-dimensional time-dependent simulations in order to provide age fields as precisely as possible over the whole depth of ice cores.

2. AGE EQUATION IN ICE SHEETS

2.1. General equation

Let us consider an ice sheet in Cartesian coordinates $x$, $y$ (which span the horizontal plane), $z$ (vertical) and time $t$. The equation which describes the evolution of the age field $A(x, y, z, t)$ in the accumulation zone of the ice sheet is then

$$\frac{dA}{dt} = 1, \quad A(z = h) = 0,$$  \hspace{1cm} (1)

where $d/dt$ is the material time derivative which follows the
motion of the ice particles with velocity \( \mathbf{v} = (v_x, v_y, v_z) \), and \( z = h(x, y, t) \) is the free surface of the ice sheet where the ice particles settle as snowflakes. In an Eulerian frame,

\[
\begin{align*}
\frac{\partial A}{\partial t} + v_x \frac{\partial A}{\partial x} + v_y \frac{\partial A}{\partial y} + v_z \frac{\partial A}{\partial z} &= 1, \\
A(z = h) &= 0,
\end{align*}
\]  

where \( \partial / \partial t \) is the local time derivative. Assuming incompressibility, \( \text{div} \mathbf{v} = 0 \), Equation (2) can be written in conservative form as

\[
\begin{align*}
\frac{\partial A}{\partial t} + \frac{\partial (Av_x)}{\partial x} + \frac{\partial (Av_y)}{\partial y} + \frac{\partial (Av_z)}{\partial z} &= 1, \\
A(z = h) &= 0.
\end{align*}
\]  

This equation is of hyperbolic type with a constant source term and a homogeneous Dirichlet boundary condition.

### 2.2. One-dimensional steady-state approximation

We now assume steady-state conditions and neglect horizontal advection in Equation (2), which is a coarse approximation of the flow conditions in the vicinity of many ice-core positions in Greenland and Antarctica situated on or close to ice domes or ridges (GRIP, GISP2, Dome C, DML05, etc.). Equation (2) then simplifies to

\[
v_z \frac{\partial A}{\partial z} = 1, \quad A(z = h) = 0, \quad \text{(4)}
\]

or equivalently in conservative form,

\[
\frac{\partial (Av_z)}{\partial z} = 1 + A \frac{\partial v_z}{\partial z}, \quad A(z = h) = 0. \quad \text{(5)}
\]

With the scales

\[
[z] = H, \quad [v_z] = a_s, \quad [A] = H/a_s,
\]

where \( H \) is the local ice thickness and \( a_s \) is the net accumulation rate, dimensionless quantities \( \bar{z}, \bar{v}_z, \bar{A} \) are introduced as

\[
z = [z] \bar{z}, \quad v_z = [v_z] \bar{v}_z, \quad A = [A] \bar{A}.
\]

If we choose \( z = 0 \) for the local ice base, then for the free surface \( z = h = H \), or \( \bar{z} = \bar{h} = 1 \), and the dimensionless forms of Equations (4) and (5) become

\[
\bar{v}_z \frac{\partial \bar{A}}{\partial \bar{z}} = 1, \quad \bar{A}(\bar{z} = 1) = 0. \quad \text{(8)}
\]

In the following, all quantities are taken dimensionless, and tildes are omitted for simplicity of notation.

For the vertical velocity, a Dansgaard–Johnsen type distribution (Dansgaard and Johnsen, 1969) is assumed, which consists of a constant vertical strain rate \( \partial v_z / \partial z \) from the free surface \( z = 1 \) down to a position \( z = z^* \), and a linearly decreasing vertical strain rate \( \partial v_z / \partial z \propto z \) below. With \( v_z(1) = -1 \) (vertical velocity balances accumulation at the free surface), \( v_z(0) = v^{p}_z < 0 \) (small offset at the base in order to avoid an infinite age) and continuity of \( v_z \) and \( \partial v_z / \partial z \) at \( z = z^* \), this yields

\[
\begin{align*}
v_z &= -c_1 z + c_2, \quad \text{for } z \geq z^*, \\
v_z &= -c_3 z^2 - c_4, \quad \text{for } z \leq z^*,
\end{align*}
\]

where

\[
\begin{align*}
c_1 &= \frac{2(1 + v^{p}_z)}{2 - z^*}, \\
c_2 &= \frac{z^* + 2v^{p}_z}{2 - z^*}, \\
c_3 &= \frac{1 + v^{p}_z}{z^*(2 - z^*)}, \\
c_4 &= -v^{p}_z.
\end{align*}
\]

Note that all constants \( c_1-c_4 \) are positive provided \( z^* = O(1) \) and \( |v^{p}_z| \ll 1 \). In the following, we will set \( z^* = 0.25 \), \( v^{p}_z = -2.5 \times 10^{-3} \).

The resulting profile is plotted in Figure 1. With the velocity distribution (9), an analytic solution of the age Equation (8), can readily be obtained. It reads

\[
\begin{align*}
A &= \frac{1}{c_1} \ln \frac{c_1}{c_1 z - c_2}, \quad \text{for } z \geq z^*, \\
A &= \frac{1}{\sqrt{c_3} c_4} \left( \arctan \frac{\sqrt{c_3} z}{\sqrt{c_4}} - \arctan \frac{\sqrt{c_3} z^*}{\sqrt{c_4}} \right) + \frac{1}{c_1} \ln \frac{1}{c_1 z^* - c_2}, \quad \text{for } z \leq z^*.
\end{align*}
\]

This solution is plotted in Figure 1. At the bottom, \( A = 2076 \), which for the GRIP ice core (\( H = 3028 \) m, \( a_s = 0.235 \) m ice equiv. a\(^{-1}\)); Dahl-Jensen and others, 1993) corresponds to 273.2 kyr. That age is in reasonable agreement with current estimates of about 250 kyr (Dansgaard and others, 1993; Greve, 1997).

### 3. NUMERICAL SCHEMES

#### 3.1. General considerations

We now turn to the numerical solution of the one-dimen-
sional age Equation (8). In order to investigate schemes that can be adopted for non-steady-state conditions, we do not attempt to solve this equation directly, but iterate
\[
\frac{\partial A}{\partial t} + \frac{\partial (Av_z)}{\partial z} = 1 + A \frac{\partial v_z}{\partial z}, \quad A(z) = 1 = 0 \quad (13)
\]
with the initial condition \(A(t = 0) = 0\) until steady state is reached. By introducing the flux \(F\) and source \(Q\) as
\[
F = Av_z, \quad Q = 1 + A \frac{\partial v_z}{\partial z}.
\]
Equation (13) can be written in compact fashion,
\[
\frac{\partial A}{\partial t} + \frac{\partial F}{\partial z} = Q, \quad A(z) = 1 = 0 \quad (15)
\]
Let us introduce a discretization of space and time,
\[
z_k = k \Delta z = 0 \ldots 1, \quad t^n = n \Delta t, \quad t = 0 \ldots n \Delta t,
\]
where \(\Delta z\) and \(\Delta t\) are the grid spacing and the time-step, respectively, and define averaged ages \(A^\prime_k\), fluxes \(F^\prime_{k+1/2}\) and sources \(Q^\prime_k\),
\[
A^\prime_k = \frac{1}{\Delta z} \int_{z_{k-1/2}}^{z_{k+1/2}} A(z, t^n) \, dz,
\]
\[
F^\prime_{k+1/2} = \frac{1}{\Delta t} \int_{t^n}^{t^{n+1}} F(z_{k+1/2}, t) \, dt,
\]
\[
Q^\prime_k = \frac{1}{\Delta z \Delta t} \int_{t^n}^{t^{n+1}} \int_{z_{k-1/2}}^{z_{k+1/2}} Q(z, t) \, dz \, dt.
\]
Then integration of Equation (5) over the space–time rectangle \([z_{k-1/2}, z_{k+1/2}] \times [t^n, t^{n+1}]\) in the sense of a finite-volume approach yields the difference equation
\[
A^\prime_{k+1} = A^\prime_k + Q^\prime_k \Delta t - \frac{\Delta t}{\Delta z} (F^\prime_{k+1/2} - F^\prime_{k-1/2}),
\]
which is still exact.

The bottom gridpoint \(k = 0\) needs to be treated separately. Here,
\[
A^\prime_0 = \frac{2}{\Delta z} \int_{z_0}^{z_{1/2}} A(z, t^n) \, dz,
\]
\[
F^\prime_{1/2} = \frac{1}{\Delta t} \int_{t^n}^{t^{n+1}} F(z_{1/2}, t) \, dt,
\]
\[
Q^\prime_0 = \frac{2}{\Delta z \Delta t} \int_{t^n}^{t^{n+1}} \int_{z_0}^{z_{1/2}} Q(z, t) \, dz \, dt,
\]
and by integration of Equation (5) over \([z_0, z_{1/2}] \times [t^n, t^{n+1}]\),
\[
A^\prime_{0}^{n+1} = A^\prime_0 + Q^\prime_0 \Delta t - \frac{2 \Delta t}{\Delta z} (F^\prime_{1/2} - F^\prime_0).
\]
Numerical solution schemes can be constructed by assigning approximate values to the averaged quantities in Equations (18) and (20). We will only consider explicit schemes with
\[
\begin{align*}
A^\prime_k &= A^\prime_k, \\
Q^\prime_k &= Q^\prime_k, \\
F^\prime_{k+1/2} &= A^\prime_{k+1/2} (v_0^k)_{k+1/2} - (v^\prime_{k+1/2}), \\
F^\prime_0 &= A^\prime_0 (v_0^k) - (v^\prime_0),
\end{align*}
\]
where \(v^\prime_0\) denote an optional dissipative limiter. Thus, the general iteration rule is
\[
A^\prime_{k+1} = A^\prime_k + Q^\prime_k \Delta t - \frac{\Delta t}{\Delta z} (A^\prime_{k+1/2} (v_0^k)_{k+1/2} - A^\prime_{k-1/2} (v_0^k)_{k-1/2})
\]
which is
\[
A^\prime_{0}^{n+1} = A^\prime_0 + Q^\prime_0 \Delta t - \frac{2 \Delta t}{\Delta z} (A^\prime_{1/2} (v_0^k)_{1/2} - A^\prime_0 (v_0^k)_0) + \frac{2 \Delta t}{\Delta z} (v^\prime_1 - v^\prime_0).
\]
We apply a numerical grid for which the ages \(A\) and sources \(Q\) are defined on gridpoints \(k\) and the velocities \(v_z\) on cell boundaries \(k \pm 1/2\) (staggered grid, Fig. 2). In addition, the basal velocity \(v_b\) is assumed to be known. Therefore, in Equation (22) the ages \(A^\prime_{k+1/2}\) do not conform to the grid, and the several numerical schemes derived from Equation (22) differ only in the method of computing the ages \(A^\prime_{k+1/2}\) from neighbouring ages \(A^\prime_k\) and in the selection of dissipative limiters \(v^\prime_0\).

### 3.2. Errors

We assess the error of several solution techniques by comparison with the analytic solution (Equation (12)). Near-basal ice is of particular interest, so we consider the relative error of the basal age,
\[
r^b = \frac{A^\prime_b - A^\prime_{b,\text{ana}}}{A^\prime_{b,\text{ana}}},
\]
where \(A^\prime_{b,\text{ana}}\) is the steady-state basal age of Equation (22) and \(A^\prime_{b,\text{ana}}\) is the exact analytic value given by Equation (12).

3.3. Central differences

The simplest calculation of \(A^\prime_{k+1/2}\)
\[
A^\prime_{k+1/2} = \frac{1}{2} (A^\prime_{k+1} + A^\prime_k), \quad v^\prime_{k+1/2} = v^\prime_0 = 0
\]
leads to the forward-time central-space scheme (FTCS)
\[ A_{\text{FTCS}}^{n+1} = 0, \]
\[ A_k^{n+1} = A_k^n + Q_k^n \Delta t - \frac{\Delta t}{2\Delta z} \left[ (A_{k+1}^n + A_k^n)(v_z)_k^{n+1/2} - (A_k^n + A_{k-1}^n)(v_z)_k^{n-1/2} \right], \quad k = 1 \ldots k_{\text{max}} - 1, \]
which is of first order in time and second order in space. However, the resulting iteration is always unstable (Morton and Mayers, 1994). Stability can be achieved by extending the time integration over two time-steps ("leap-frog"),
\[ A_{\text{CTCS}}^{n+1} = 0, \]
\[ A_k^{n+1} = A_k^{n-1} + 2Q_k^n \Delta t - \frac{\Delta t}{\Delta z} \left[ (A_k^n + A_0^n)(v_z)_k^{n+1/2} - (A_k^n + A_{k-1}^n)(v_z)_k^{n-1/2} \right], \quad k = 1 \ldots k_{\text{max}} - 1, \]
\[ A_0^{n+1} = A_0^n + Q_0^n \Delta t - \frac{2\Delta t}{\Delta z} \left[ (A_1^n + A_0^n)(v_z)_1^{n+1/2} - 2A_0^n(v_z)_0^n \right], \quad (26) \]
which is known as the central-time central-space scheme (CTCS, of second order in time and space). In order to restrict the growth of spurious numerical modes due to decoupling of even and odd iteration steps, every 101st time-step the CTCS scheme (Equation (27)) is replaced by the FTCS scheme (Equation (26)). This number was found to be sufficient to avoid decoupling. The calculation is also initialized with the FTCS scheme.

### 3.4. First-order upstream

The CTCS scheme tends to produce numerical oscillations due to the unphysical central discretization of the advection term. At any point in space, the flow of information is from the upstream direction only: To correct for this, non-central differences pointing in the upstream direction can be used. Schemes of that kind are called upstream (upwind) schemes, and the simplest one is constructed by choosing
\[ (v_z)_k^{n+1/2} > 0 : \quad A_{k+1/2}^n = A_k^n, \]
\[ (v_z)_k^{n+1/2} < 0 : \quad A_{k+1/2}^n = A_{k+1}^n, \]
\[ \varphi_{k+1/2}^n = \varphi_0^n = 0. \quad (28) \]

For our problem, \((v_z)_k^{n+1/2} < 0\) (Equation (9); Fig. 1), so that
\[ A_{\text{CTCS}}^{n+1} = 0, \]
\[ A_k^{n+1} = A_k^n + Q_k^n \Delta t - \frac{\Delta t}{\Delta z} \left[ (A_{k+1}^n(v_z)_k^{n+1/2} - A_k^n(v_z)_k^{n-1/2} \right], \quad k = 1 \ldots k_{\text{max}} - 1, \]
\[ A_0^{n+1} = A_0^n + Q_0^n \Delta t - \frac{2\Delta t}{\Delta z} \left[ (A_1^n(v_z)_1^{n+1/2} - 2A_0^n(v_z)_0^n \right]. \quad (29) \]
This is the first-order upstream scheme (UP1), which is of first order in time and space. By subtracting Equations (29) and (26), one obtains the difference
\[ \frac{\Delta t}{2\Delta z} \left[ (A_{k+1}^n - A_k^n)(v_z)_k^{n+1/2} - (A_k^n - A_{k-1}^n)(v_z)_k^{n-1/2} \right] \]
which corresponds to an additional diffusion term
\[ D = \frac{\partial}{\partial z} \left( \lambda_{\text{num}} \frac{\partial A}{\partial z} \right), \quad \lambda_{\text{num}} = \frac{|v_z| \Delta z}{2} \quad (30) \]
(numeral diffusivity \(\lambda_{\text{num}}\)) on the righthand side of the age equation (5), which is discretized by central differences. The numerical diffusion efficiently damps numerical oscillations, but a disadvantage is that regions with steep gradients within a smooth solution are smeared out over the spatial domain.

### 3.5. Second-order upstream

An improvement can be made in the numerical diffusion by replacing Equation (28) with a linear upstream interpolation,
\[ A_{\text{CTCS}}^{n+1} = 0, \]
\[ A_k^{n+1} = A_k^0 + Q_k^n \Delta t - \frac{\Delta t}{\Delta z} \left[ (A_{k+1}^n(v_z)_k^{n+1/2} - (A_k^n + A_{k-1}^n)(v_z)_k^{n-1/2} \right], \quad k = 1 \ldots k_{\text{max}} - 1, \]
\[ A_0^{n+1} = A_0^0 + Q_0^n \Delta t - \frac{2\Delta t}{\Delta z} \left[ (A_1^n(v_z)_1^{n+1/2} - 2A_0^n(v_z)_0^n \right], \quad (27) \]
\[ \varphi_{k+1/2}^n = \varphi_0^n = 0. \]
With \((v_z)_k^{n+1/2} < 0\) and central interpolation for \(A_{\text{CTCS}}^{n+1/2}\) the second-order upstream scheme (UP2)
\[ A_{\text{CTCS}}^{n+1} = 0, \]
\[ A_k^{n+1} = A_k^0 + Q_k^n \Delta t - \frac{\Delta t}{\Delta z} \left[ (A_{k+1}^n + A_k^n)(v_z)_k^{n+1/2} - (A_k^n + A_{k-1}^n)(v_z)_k^{n-1/2} \right. \]
\[ - (A_k^n + 3A_{k-1}^n)(v_z)_k^{n-3/2} \right], \]
\[ A_0^{n+1} = A_0^0 + Q_0^n \Delta t - \frac{\Delta t}{\Delta z} \left[ (A_1^n + 3A_0^n)(v_z)_1^{n+1/2} - (A_0^n + 3A_{-1}^n)(v_z)_0^{n-3/2} \right] \quad (31) \]
\[ \varphi_{k+1/2}^n = \varphi_0^n = 0. \]

is produced. This scheme has first-order accuracy in time and second-order accuracy in space.

### 3.6. QUICK

Another upstream scheme, the Quadratic Upstream Interpolation for Convective Kinematics (QUICK; Leonard, 1979\textsuperscript{a}) is defined by
\[ A_{\text{CTCS}}^{n+1} = 0, \]
\[ A_k^{n+1} = A_k^0 + Q_k^n \Delta t - \frac{\Delta t}{\Delta z} \left[ (A_{k+1}^n(v_z)_k^{n+1/2} - (A_k^n + A_{k-1}^n)(v_z)_k^{n-1/2} \right], \quad \]
\[ (v_z)_k^{n+1/2} > 0 : \quad A_{k+1/2}^n = -\frac{1}{8} A_k^n + \frac{3}{4} A_{k+1}^n + \frac{3}{8} A_{k+2}^n, \]
\[ (v_z)_k^{n+1/2} < 0 : \quad A_{k+1/2}^n = -\frac{1}{8} A_k^n + \frac{3}{4} A_{k+1}^n + \frac{3}{8} A_{k-1}^n, \]
\[ \varphi_{k+1/2}^n = \varphi_0^n = 0. \quad (32) \]
As in UP2, with \((v_z)_{h+1/2}^n < 0\) and central interpolation for \(A_{h-1/2}^n\) the corresponding iteration rule is
\[
A_{h+1}^{n+1} = A_{h}^{n} + Q_{h}^{n} \Delta t - \frac{\Delta t}{8\Delta z} \left[ (4A_{h+1}^{n} + 4A_{h}^{n} - (v_z)_h^{n})_{h+1/2} - (A_{h+1}^{n} + 6A_{h}^{n} - 3A_{h-1}^{n}) (v_z)_h^{n} - 3/2 \right],
\]

This scheme is of first order in time and of third order in space.

\[\text{A}\]
\[\text{As in UP2, with}\]
\[\text{\(n\)}\]
\[\text{\(n\)}\]
\[\text{\(k\)}\]
\[\text{\(\max\)}\]
\[\text{\(\max\)}\]
\[\text{\(\hat{A}\)}\]
\[\text{\(A\)}\]
\[\text{\(\frac{1}{10}\)}\]
\[\text{\(1\)}\]
\[\text{\(n\)}\]
\[\text{\(\frac{1}{\max}\)}\]
\[\text{\(\max\)}\]
\[\text{\(\hat{A}\)}\]
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In order to compute the steady-state solution of the age equation (15), we iterate from
which possesses first-order accuracy in time and up to second-order accuracy in space.

This leads to the scheme
\begin{align}
A_{k+1}^{n+1} &= A_k^n + Q_k^n \Delta t \\
&= \frac{\Delta t}{2\Delta z} \left\{ \left( A_{k+1/2}^n \right)^R + \left( A_{k+1/2}^n \right)^L \right\} (v)_k^n \frac{1}{2}
- \frac{\Delta t}{2\Delta z} \left\{ \left( A_{k-1/2}^n \right)^R + \left( A_{k-1/2}^n \right)^L \right\} (v)_{k-1/2}^n \\
&= \frac{\Delta t}{2\Delta z} \left\{ \left( A_{k+1/2}^n \right)^R - \left( A_{k-1/2}^n \right)^L \right\} (v)_k^n
- \frac{\Delta t}{2\Delta z} \left\{ \left( A_{k-1/2}^n \right)^R - \left( A_{k-1/2}^n \right)^L \right\} (v)_{k-1/2}^n \\
&= A_k^n + Q_k^n \Delta t
\end{align}

(45)

which possesses first-order accuracy in time and up to second-order accuracy in space.

4. DISCUSSION

In order to compute the steady-state solution of the age equation (15), we iterate from \( t = 0 \) until \( t_f = 1000 \), which is, considering the maximum age of the analytical solution \( A = 2076 \) at the bottom, easily sufficient to reach steady state. We test the solution schemes using a variety of domain grid densities, \( k_{\text{max}} = 20, 40, 60, 80, 100 \), which correspond to grind spacings \( \Delta z = 1/20, 1/40, 1/60, 1/80 \) and \( 1/100 \), respectively. The time-step is \( \Delta t = 0.5 \Delta z \), so that with \( |v| \leq 1 \) the Courant–Friedrichs–Lewy condition \( |v| \Delta t / \Delta z \leq 1 \) (Morton and Mayers, 1994) is fulfilled.

Table 1 shows the relative errors of the basal age, \( r_b \), of the computed age profiles for the numerical schemes we wish to test. For all schemes and all grid spacings, stable integration is achieved, and all schemes show clear convergence toward the analytical solution with decreasing grid spacing (increasing number of gridpoints). Surprisingly, for the smallest number of gridpoints \( k_{\text{max}} = 20 \), the UP1 scheme, which has the smallest spatial accuracy (first order) and the largest numerical diffusion, gives by far the best result with \( r_b \) less than 4%, whereas for the other schemes \( r_b \) is greater than 20%. Apparently, the discretization error and the error due to numerical diffusion cancel each other out to a large extent. However, this balance disappears for larger numbers of gridpoints, so that for \( k_{\text{max}} \geq 60 \) the result of UP1 is worst, and even for \( k_{\text{max}} = 100 \) the error is larger than for \( k_{\text{max}} = 20 \).

The spatially second-order schemes UP2 and MTVDLF/M give the best results throughout (except at \( k_{\text{max}} = 20 \), as noted above), and further, the results of the two schemes are identical. Closer inspection shows that this surprising finding does not hold in general, but is due to our particular problem (see Appendix). The errors \( r_b \) of both schemes are very small, \( \leq 1\% \) for \( k_{\text{max}} \geq 60 \). Even for the third-order scheme QUICK, \( r_b \) is distinctly greater than for UP2 and MTVDLF/M at all resolutions. As for the TVD schemes, application of the less diffusive limiters (MTVDLF/S, MTVDLF/W) reduces the accuracy, so that some numerical diffusion is evidently desirable.

The CTCS scheme is particularly bad for small numbers of gridpoints, \( k_{\text{max}} = 20, 40 \). This is because it tends to produce some oscillations over the whole spatial domain, which may even lead to unstable integrations. These oscillations become evident in Figure 3, which shows the relative errors of the computed age profiles as functions of \( z \) for \( k_{\text{max}} = 20, 100 \) (schemes MTVDLF/SW not considered). An attempt
may be used to minimize this problem by adjusting the frequency of FTCS steps (section 3.3), but nevertheless the CTCS scheme cannot be recommended due to this susceptibility to instabilities.

A comparison of the relative errors of UP1, UP2, MTVDLM/M and QUICK over the whole column is instructive (see Fig. 3). For UP1 the error is smallest close to the surface and increases essentially monotonically toward the base. By contrast, for UP2, MTVDLM/M and QUICK the errors are somewhat larger close to the surface, reach a minimum at approximately half the depth and increase again further down. This is probably because UP2, MTVDLM/M and QUICK use central interpolation like CTCS for the age $A^\nu_{bas} \cdot 1/2$ (see Equations (32) and (34)), so that the near-surface error resembles that of CTCS. The errors of UP1 and QUICK are smaller than those of UP2 and MTVDLM/M for $z > z^\nu$ (small age gradients), whereas for $z < z^\nu$ (large age gradients) UP2 and MTVDLM/M perform better. Nevertheless, except for the very basal gridpoint at $z \approx 0$ (see above discussion of the basal error) the simplest UP1 scheme yields results comparable to those of UP2 and MTVDLM/M for high and low resolutions.

At the transition point $z = z^\nu$, where the vertical velocity is discontinuous in the second and the age in the third $z$ derivative, the errors of UP1, UP2, MTVDLM/M and QUICK show some jumps, naturally more pronounced for high resolution. Further, some oscillations appear for high resolution close to the base. Generally, among those schemes the most artificial structure is introduced to the age profile by QUICK due to its high spatial order.

It is worth noting that in other similar models, different schemes are favoured. Wang and Hutter (2000) investigate the one-dimensional problem of a discontinuity (Heaviside step) of some field quantity $\psi$ which travels with constant velocity $c$ in direction $x$ in an infinitely extended system governed by the advective wave equation $\frac{\partial \psi}{\partial t} + \frac{\partial (\psi v)}{\partial x} = 0$. Apart from the missing source term, the constant velocity and the missing boundaries, this model equation is equivalent to our age equation (5). However, the moving discontinuity poses a challenge to numerical schemes that is not present for our continuous age profile. Wang and Hutter (2000) show that numerical diffusion in the UP1 scheme largely smears out the discontinuity, and CTCS, UP2 and QUICK produce some numerical oscillations in the vicinity of the discontinuity. Best reproduction is achieved by the MTVDLM schemes; however, in contrast to our problem the least dissipative limiters (MTVDLM/S, MTVDLM/W) are favourable because they best preserve the shape of the Heaviside step.

To conclude, our tests show clearly that second-order upstreaming (UP2), modified TVD Lax–Friedrichs (MTVDLM/S) solution techniques and, with limitations of the accuracy directly at the base for higher resolutions, even first-order upstreaming (UP1) yield the best results for typical age profiles in ice sheets (here approximated by a one-dimensional model problem). UP1 and UP2 are less expensive computationally, but spatial discontinuities of the age field (which are not included in our model problem) will either be smeared out (UP1) or will be accompanied by artificial oscillations (UP2). MTVDLM/M has the potential to reproduce such jumps more accurately at the cost of more computing time.

Generalization of the methods presented in section 3 to three-dimensional time-dependent situations described by Equation (3) is straightforward and will be carried out in the near future within the ice-sheet model SICOPOLIS. The applicability to such problems was successfully demonstrated by Wang (2001) in the context of wind-induced circulations in lakes, where three-dimensional advection occurs in the evolution equations for the flow velocity and the temperature field.

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REFERENCES


APPENDIX

EQUIVALENCE BETWEEN MTVDLF/M AND UP2

The equivalence between the two schemes MTVDLF/M and UP2 for our particular problem can be proved in the following manner. For the whole spatial domain \(0 \leq z \leq 1\), the analytical steady-state solution of the age equation (15) has the properties
\[
v_z < 0, \quad \frac{\partial A}{\partial z} < 0, \quad \frac{\partial^2 A}{\partial z^2} > 0 \quad (A1)
\]
(see Fig. 1). Provided the numerical solution at time \(t^n\) is sufficiently close to the analytical steady state so that these relations also hold for the numerical solution, then, due to (A1),
\[
A^n_k - A^n_{k-1} < A^n_k - A^n_{k-1}, \quad k = 1 \ldots k_{\text{max}} - 1, \quad (A2)
\]
and with (A2),
\[
\theta_k^n = \frac{A^n_k - A^n_{k-1}}{A^n_{k+1} - A^n_k} > 1 \Rightarrow \phi^\text{Minmod}(\theta_k^n) = 1, \quad (A3)
\]
so that the slope limiter (Equations (36) and (37)) computed with Minmod is
\[
\sigma_k^n = \frac{A^n_{k+1} - A^n_k}{\Delta z}, \quad k = 0 \ldots k_{\text{max}} - 1, \quad (A4)
\]
Thus, from Equation (42),
\[
(A^n_{k+1/2})^L = \frac{A^n_{k+1} + A^n_k}{2}, \quad k = 0 \ldots k_{\text{max}} - 1,
\]
\[
(A^n_{k+1/2})^R = \frac{-A^n_{k+2} + 3A^n_{k+1}}{2}, \quad k = 0 \ldots k_{\text{max}} - 2,
\]
\[
(A^n_{k_{\text{max}}-1/2})^R = \frac{A^n_{k_{\text{max}}} + A^n_{k_{\text{max}}-1}}{2}.
\]

When this result and condition (A1) in the form \(|v_z| = -v_z\) are inserted into the MTVDLF/M scheme (Equation (45)), it reduces to the UP2 scheme (Equation (32)) for all gridpoints \(k = 0 \ldots k_{\text{max}}\).

The equivalence of MTVDLF/M and UP2 can be similarly shown for the cases
\[
v_z < 0, \quad \frac{\partial A}{\partial z} > 0, \quad \frac{\partial^2 A}{\partial z^2} < 0, \quad (A6)
\]
\[
v_z > 0, \quad \frac{\partial A}{\partial z} > 0, \quad \frac{\partial^2 A}{\partial z^2} > 0, \quad (A7)
\]
\[
v_z > 0, \quad \frac{\partial A}{\partial z} < 0, \quad \frac{\partial^2 A}{\partial z^2} < 0. \quad (A8)
\]

For case (A6) the proof is analogous to (A1), whereas for (A7) and (A8),
\[
\phi^\text{Minmod}(\theta_k^n) = \theta_k^n, \quad k = 1 \ldots k_{\text{max}} - 1, \quad (A9)
\]
so that the slope limiter is
\[
\sigma_k^n = \frac{A^n_k - A^n_{k-1}}{\Delta z}, \quad k = 1 \ldots k_{\text{max}}, \quad (A10)
\]
which is (except for \(k = 0\)) the upstream direction for positive velocities \(v_z\).