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Citation	Journal of the Optical Society of America B : Optical Physics, 18(11), 1742-1746 https://doi.org/10.1364/JOSAB.18.001742
Issue Date	2001-11-01
Doc URL	http://hdl.handle.net/2115/45331
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Type	article
File Information	JOSAB18-11_1742-1746.pdf



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Optical pulse compression to 5.0 fs by use of only a spatial light modulator for phase compensation

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Received March 13, 2001; revised manuscript received May 8, 2001

We experimentally demonstrate the generation of 5.0-fs optical pulses (2.5 μJ , 1-kHz repetition rate), using only a spatial light modulator for phase compensation. Pulse compression of the broadband pulse (500–1000 nm) from an argon-filled capillary fiber is achieved with a liquid-crystal spatial light modulator without any prechirp compensation. The output pulse width is found to be 4.1 fs by a fringe-resolved autocorrelator fitted with a transform-limited pulse and to be 5.0 fs by second-harmonic generation frequency-resolved optical gating with marginal correction. It is to our knowledge the shortest pulse ever generated by use of only a spatial light modulator for phase compensation. © 2001 Optical Society of America

OCIS codes: 320.7090, 320.5560, 320.7140, 230.6120, 320.5520, 190.7110.

1. INTRODUCTION

Optical pulses of ~ 5 fs have been generated directly from an oscillator^{1,2} and external compression by use of a fused-silica fiber,^{3–5} a capillary fiber filled with a noble gas,^{6,7} or optical parametric amplification⁸ for spectrum broadening. All these methods utilize chirped mirrors for chirp compensation. Chirped mirrors have the advantage of high throughput. However, difficulty in obtaining the large bandwidth, interdependence of different phase orders, and an inability to fine-tune the phase in the experimental setup are disadvantages. A pulse shaping technique⁹ that uses a liquid-crystal spatial light modulator (SLM) for pulse compression has the advantages of large bandwidth (300–1500 nm) and *in situ* adaptive phase control. Chirped pulses from an oscillator have been compressed from 80 to 11 fs by a SLM with a two-dimensional search algorithm for second- and third-order dispersion coefficients.¹⁰ Recently the SLM was used to compress the broadband pulses from an argon-

filled capillary fiber with prechirp compensation by a prism pair to yield 6-fs pulses¹¹ and sub-6-fs pulses.¹² Deformable mirrors were used as phase-only modulators to compress pulses from 92 to 15 fs.¹³ In this paper we demonstrate that a SLM can be used to compress broadband (500–1000-nm) pulses from an argon-filled capillary fiber, without any prechirp compensation, to generate 5.0-fs pulses. When prechirp compensation optics such as a prism pair is not used, the optical throughput increases, and alignment becomes easier. To evaluate accurately the pulses that are thus generated, we used not only a fringe-resolved autocorrelator (FRAC) but also a second-harmonic generation (SH) frequency-resolved optical gating (FROG) apparatus.^{4,5,7}

2. EXPERIMENTAL SETUP

The experimental setup is shown in Fig. 1. The output beam of a Ti:sapphire laser-amplifier system [Femto-

power Pro; center wavelength, 790 nm; pulse width, 30 fs; repetition rate, 1 kHz; pulse energy adjusted by a neutral-density filter (ND), 140 μ J] was focused into a capillary fiber with 34-cm length and 0.1-mm inner diameter, which was positioned in a chamber filled with argon.¹⁴ The chamber had two 1-mm-thick sapphire windows. The output beam from the chamber was collimated by a spherical mirror and was directed to a 4-*f* system by the SLM. The 4-*f* system consisted of two spherical mirrors with a focal length *f* = 20 cm and two silver reflective gratings (G1 and G2) with a ruling distance *d* = 1/150 mm. The optical path lengths from the gratings to the spherical mirrors and those from the spherical mirrors to the SLM were all set to be *f*. The liquid crystal SLM (Citizen Company) consisted of 648 97- μ m-wide pixels, with a 5- μ m gap between adjacent pixels. The transmission of the SLM was more than 70% at a 500–700-m wavelength but decreased at long wavelengths (e.g., 50% at 1000 nm). The pulse energy after the fiber chamber was 22 μ J, and the throughput of the 4-*f* system was 30%. In the setup we used periscopes (PSs) to change the height, the polarization direction, or both of the beam, and a flip mirror (FM) to change the beam direction for measurements of the FRAC and the SH FROG.

3. DETERMINATION OF THE SLM PHASE PATTERN

The SLM was used as a phase modulator, which can impose a phase variation of 2π for light whose wavelength is less than 1400 nm with a resolution of 192. The Phase $\phi_{\text{SLM}}(x)$ from the SLM at position *x* is given by a polynomial of the form

$$\phi_{\text{SLM}}(x) = \frac{\alpha}{2}[\omega(x) - \omega_0]^2 + \frac{\beta}{6}[\omega(x) - \omega_0]^3 + \frac{\gamma}{24}[\omega(x) - \omega_0]^4, \quad (1)$$

where ω_0 is the center angular frequency for a Taylor expansion, $\omega(x)$ is the angular frequency at position *x* and is given by $\omega(x) = 2\pi c / \{d \sin[\tan^{-1}(x/f) + \sin^{-1}(\lambda_c/d)]\}$, *c* is the speed of light, and $\lambda_c = 800$ nm is the wavelength at the central position of the SLM, *x* = 0. λ_c does not have to be equal to the center wavelength for Taylor expansion λ_0 , where $\lambda_0 = 2\pi c / \omega_0$. α , β , and γ are the group-delay dispersion (gdd), the third-order dis-

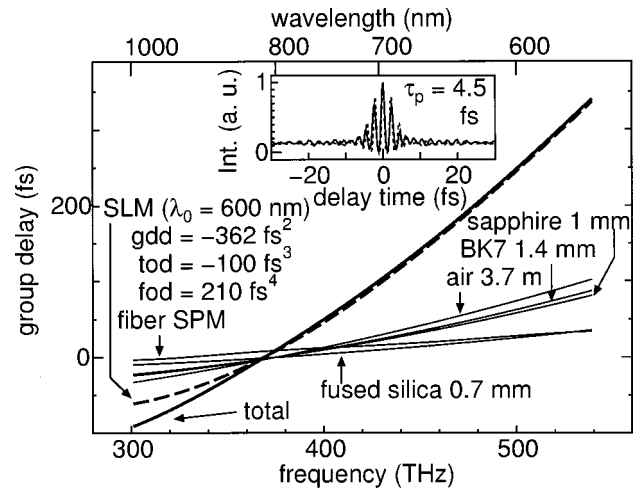


Fig. 2. Calculated group delay of each optical component (solid curves) at $\lambda_0 = 600$ nm at an argon pressure of 2.0 atm. The total group delay (thick solid curve) is compared with the negative of the experimentally optimized group delay applied by the SLM (dashed curve). Inset, experimental (solid curve) and 4.5-fs fitted transform-limited (dotted curve) FRAC traces at these parameters.

persion (tod), and the fourth-order dispersion (fod), respectively, at ω_0 . The group delay $t_{d,\text{SLM}}(x)$ imposed by the SLM was

$$t_{d,\text{SLM}}(x) = \frac{\partial \phi_{\text{SLM}}(\omega)}{\partial \omega} = \alpha[\omega(x) - \omega_0] + \frac{\beta}{2}[\omega(x) - \omega_0]^2 + \frac{\gamma}{6}[\omega(x) - \omega_0]^3. \quad (2)$$

Parameters α , β , and γ were initially estimated from the total group delay $t_d(\omega)$ of the optical components from a capillary fiber (including self-phase modulation) to a nonlinear crystal in the measuring apparatus. $t_d(\omega)$ was fitted in the form of Eq. (2), and α , β , and γ were obtained. Then the negative values of these fitted parameters were initially imposed by the SLM to satisfy $t_{d,\text{SLM}}(\omega) + t_d(\omega) \approx \text{constant}$ in the whole frequency range. Theoretically, this condition should produce the shortest pulses. However, in practice it was necessary to adjust the phase determined by the SLM to yield the shortest pulses because of the difference in group delay between calculations and experiments, which were due mainly to the approximations used in our calculations. Use of the Taylor expansion in Eq. (1) was found to be the natural way to perform fine adjustment of the phase. Parameters α , β , and γ were fine-tuned by a computer to yield the shortest pulse with the FRAC and later with the SH FROG apparatus. In Fig. 2 the group delay of each component in the optical path and its negative value obtained with the SLM, as well as the totals of these values, are shown for which the shortest FRAC trace (Fig. 2, inset, the 4.5-fs fitted transform-limited pulse) was obtained for conditions when λ_0 and the argon pressure were set to 600 nm and 2.0 atm, respectively. As shown in Section 5 below, FROG results for 5.0-fs pulses were obtained under

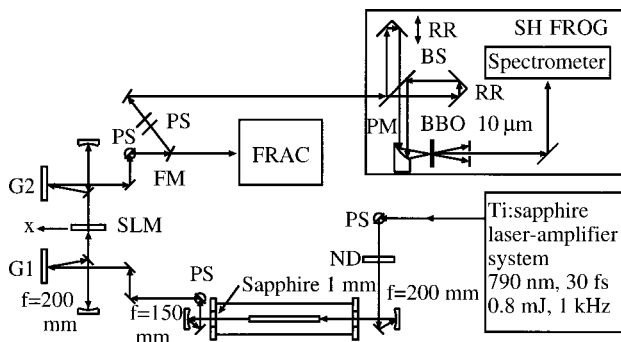


Fig. 1. Experimental setup for generation of 5.0-fs optical pulses. See text for definitions.

these conditions. Here, the effective group delay that arises from propagation in the capillary fiber was obtained from numerical nonlinear propagation calculations.¹⁴ For other optical components, we calculated the group delay by using the Sellmeier equations for fused silica (beam splitters of FRAC-FROG, 0.7 mm),¹⁵ BK7 glass (SLM substrates, 1.4 mm),¹⁶ sapphire (a chamber window, 1 mm),¹⁷ and air (3.7 m).¹⁸ As shown in Fig. 2, the agreement between the calculated group delay (thick solid curve) and the negative of the group delay from the SLM (dashed curve) when the parameters were optimized is reasonably good.

4. EFFECTS OF FINITE PIXEL SIZE OF THE SLM

λ_0 in Eq. (1) was initially set to be 800 nm with values of α , β , and γ different from those given in Section 3; the FRAC trace shown in Fig. 3, which was fitted well for the 4.1-fs transform-limited pulse, was obtained at an argon pressure of 2.8 atm. However, in this case the pulse width measured by the FROG (~ 6 fs) was longer than the transform-limited value. This underestimate of the pulse width may be understandable as having resulted from the poor fit of the pedestals in the autocorrelation trace¹⁹ and the asymmetric temporal intensity profile as well as the slightly different dispersion optics in the FRAC and the FROG apparatuses. Thus we were motivated to search for better parameters for the SLM. Because of the finite pixel size, the phase imposed by the SLM in Eq. (1) was stepwise, and, as the difference in phase between adjacent pixels [which we call $\Delta\phi(\lambda)$] became larger, phase compensation became more difficult because of the phase error introduced by the finiteness of the pixel width. For our experimental setup the frequency width for each pixel became larger as the wave-

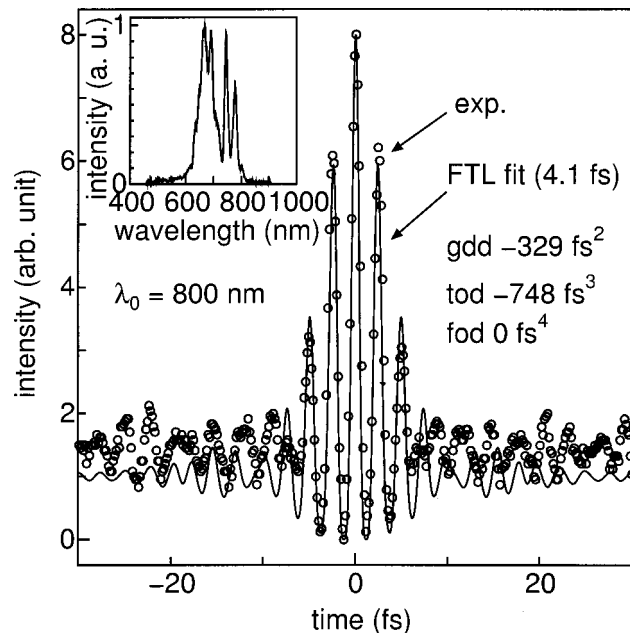


Fig. 3. Experimental (circles) and fitted transform-limited (FTL, solid curve) interferometric autocorrelation traces obtained at $\lambda_0 = 800$ nm at an argon pressure of 2.8 atm. Inset, the pulse spectrum.

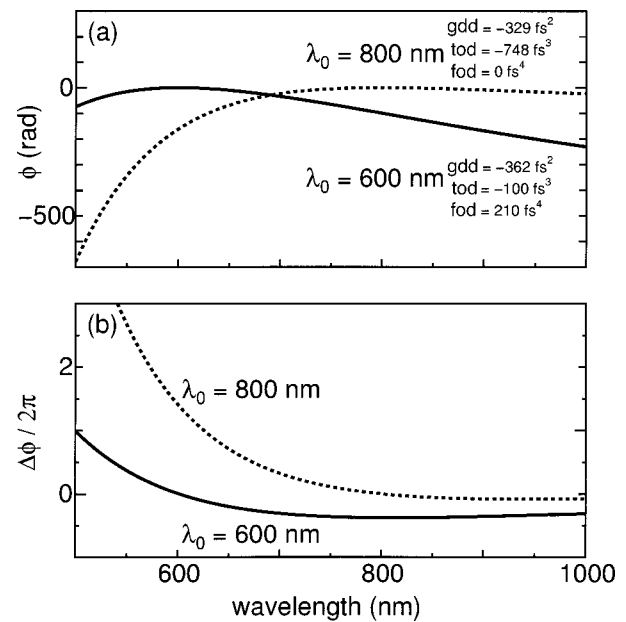


Fig. 4. (a) Applied phase $\phi(\lambda)$ and (b) phase change per pixel $\Delta\phi(\lambda)$ of the SLM for $\lambda_0 = 600$ nm (solid curves; parameters used in Fig. 2) and $\lambda_0 = 800$ nm (dotted curves; parameters used in Fig. 3).

length became shorter because of the almost-linear relationship between the pixel number and the wavelength of the SLM. Thus $|\Delta\phi(\lambda)|$ tended to become larger as the wavelength became shorter than λ_0 . In Fig. 4 the applied phase and the phase variation per pixel at the SLM for $\lambda_0 = 600$ nm (Fig. 2) and $\lambda_0 = 800$ nm (Fig. 3) are shown. In both cases the fitted group delays $t_{d,SLM}(\omega)$ were almost identical. However, the fitted phases were quite different, as shown in this figure. We analyzed $|\Delta\phi(\lambda)|$ of the SLM and found that for $\lambda_0 = 800$ nm it exceeded π for wavelengths below 672 nm; it was difficult to achieve phase compensation below this wavelength. This effect was pronounced because the spectrum that was generated had a peak at 670 nm owing to the low transmission of light in the infrared region at the SLM. When $\lambda_0 = 600$ nm, $|\Delta\phi(\lambda)|$ in the shorter-wavelength range decreased considerably, and it exceeded π only for the wavelength below 540 nm, yielding significantly better phase compensation; pulses much closer to the transform limit were obtained with the FROG measurements.

5. SH FROG RESULTS

In Fig. 5 the results of pulse measurements with the SH FROG at $\lambda_0 = 600$ nm are shown. Owing to the slight difference in the optics used in the FRAC and in the FROG apparatuses, we readjusted the SLM parameters slightly for the FROG measurements. In the SH FROG apparatus (Fig. 1) a 0.5-mm-thick broadband (400–1300-nm) dielectric beam splitter (BS) was used to separate the beam that was directed to the silver-coated retroreflector (RR) in a balanced configuration. Beam separation d_b at the parabolic mirror (PM) was 2 mm; beam diameter w_m was 1 mm. The time smearing⁴ was $\tau_d = \sqrt{2 \ln 2} d_b / (\pi c w_m) = 1.6$ fs at wavelength $\lambda = 650$ nm, with Gaussian space and time profiles as-

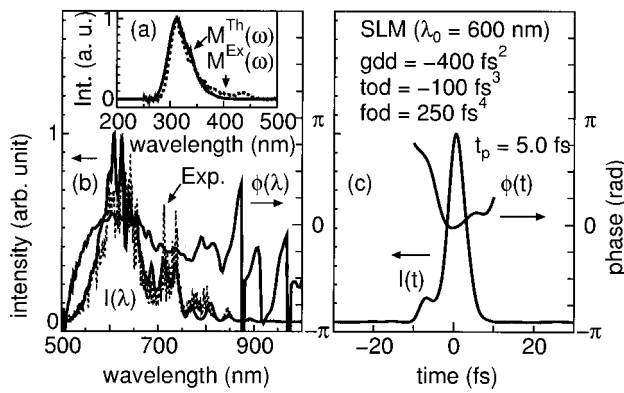


Fig. 5. Results of the corrected frequency marginal corrected FROG measurements with SLM parameters. (a) Margin calculated from the experimental spectrum $M^{Th}(\omega)$ (solid curve) and that obtained from the FROG trace $M^{Ex}(\omega)$ (dotted curve). (b) Spectrum intensity $I(\lambda)$ and phase $\phi(\lambda)$. Dotted curves experimental spectrum. (c) Temporal intensity $I(t)$ and phase $\phi(t)$.

sumed. The 10- μ m-thick β -barium borate crystal (BBO; Fig. 1) at a cutting angle of 40° was used in type 1 geometry. Owing to the limited bandwidth of the crystal, the frequency marginal²⁰ calculated from the FROG trace $M^{Ex}(\omega)$ and that from the spectrum intensity autoconvolution $M^{Th}(\omega)$ did not match, as can be seen from in Fig. 5(a). To correct for this effect we multiplied each value in the FROG trace by a frequency-dependent factor such that the marginal calculated from the FROG trace became identical to that obtained from the spectrum.²⁰ After correction of the marginal we used commercial FROG software (Femtosoft) to retrieve the pulse intensity and phase. In the measurements, a 1024-channel optical multichannel analyzer with an intensified CCD was used. The step number was 256 and the delay time was 1.34 fs. The time required for the measurement was \sim 1 min, and the stability of the pulses was excellent during that time. Also, we could usually reproduce the pulse width measured by FROG within 10% by using the same parameters several hours after they had been optimized. In Figs. 5(b) and 5(c) the spectrum and the temporal waveforms, respectively, of the pulse are shown. The FROG error was 0.0038. The measured and the calculated spectra agree quite well because of the correction of the marginals. However, the temporal width was not changed by that correction. The 5.0-fs pulse obtained had 2.4 cycles at the center wavelength (633 nm), and its width was 14% longer than the transform-limited pulse width (4.4 fs for the FROG measurement). If the geometrical smearing effect is taken into account, we estimate that the pulse width will be 4.7 fs. The residual phase was within $\pi/2$ in the wavelength range (550–800 nm), where the spectral intensity is significantly large.

6. CONCLUSION

SLM-only phase compensation to generate a 5.0-fs pulse has been experimentally demonstrated. It has been shown that the choice of the center wavelength for a Taylor expansion of the phase obtained from a SLM is important for obtaining pulses that are near the transform limit. The pulse width evaluated by correction of the

frequency marginal of a 5.0-fs SH FROG is to our knowledge the shortest pulse width ever generated by use of a SLM as the only phase compensator.

ACKNOWLEDGMENT

The authors thank K. Oka for accurate determination of the phase-change characteristics of the SLM.

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