<table>
<thead>
<tr>
<th>Title</th>
<th>Wavelength division multiplexing and demultiplexing with photonic crystal waveguide couplers</th>
</tr>
</thead>
<tbody>
<tr>
<td>Author(s)</td>
<td>Koshiba, Masanori</td>
</tr>
<tr>
<td>Citation</td>
<td>JOURNAL OF LIGHTWAVE TECHNOLOGY, 19(12), 1970-1975</td>
</tr>
<tr>
<td>Issue Date</td>
<td>2001-12</td>
</tr>
<tr>
<td>Doc URL</td>
<td><a href="http://hdl.handle.net/2115/5582">http://hdl.handle.net/2115/5582</a></td>
</tr>
<tr>
<td>Rights</td>
<td>©2001 IEEE. Personal use of this material is permitted. However, permission to reprint/republish this material for advertising or promotional purposes or for creating new collective works for resale or redistribution to servers or lists, or to reuse any copyrighted component of this work in other works must be obtained from the IEEE.</td>
</tr>
<tr>
<td>Type</td>
<td>article</td>
</tr>
<tr>
<td>File Information</td>
<td>JLT19-12.pdf</td>
</tr>
</tbody>
</table>

Hokkaido University Collection of Scholarly and Academic Papers : HUSCAP
Wavelength Division Multiplexing and Demultiplexing With Photonic Crystal Waveguide Couplers

Masanori Koshiba, Senior Member, IEEE

Abstract—A multiplexer–demultiplexer (MUX–DEMUX) based on PC waveguide couplers is proposed, and its wavelength demultiplexing properties are theoretically investigated. First, a two-channel MUX–DEMUX is designed and characterized, and then, by cascading, two stages of photonic crystal (PC) waveguide couplers with different coupling coefficients are constructed. The device sizes are expected to be drastically reduced from a scale of a few tens of micrometers to a scale of a few hundreds of micrometers in a MUX–DEMUX with a channel spacing of about 20 nm required for wide-passband wavelength division multiplexing (WDM) systems. The simulation results are obtained using a time-domain beam propagation method (BPM) based on a finite element scheme and a simpler coupled-mode theory.

Index Terms—Beam propagation method (BPM), finite element method, multiplexer–demultiplexer (MUX–DEMUX), photonic crystal, time-domain analysis, wavelength division multiplexing (WDM).

I. INTRODUCTION

PHOTONIC crystals (PCs) [1] have inspired great interest because of their potential ability to control lightwave propagation, and the possibilities of implementing PC-based optical filters into wavelength division multiplexing (WDM) systems have been discussed [2]–[6], focusing on dense-WDM (DWDM) systems for use in point-to-point core networks. DWDM systems require highly accurate wavelength control of the WDM light source and the wavelength multiplexer–demultiplexer (MUX–DEMUX). Recently, a MUX–DEMUX using vertical couplers with stronger coupling has been proposed, and a four-channel MUX–DEMUX with 17-nm channel spacing and a two-channel MUX–DEMUX with 11-nm channel spacing have been designed and fabricated [11]. Compared with the conventional couplers, the device sizes become smaller, but still are on the order of millimeters to centimeters.

Another approach for reducing the size of MUX–DEMUX is to use PCs. Here, we present the first demonstration of WDM with PC waveguide couplers. After a two-channel MUX–DEMUX based on PC waveguide couplers is designed and characterized, a four-channel MUX–DEMUX is constructed by cascading two stages of PC waveguide couplers with different coupling coefficients. The device sizes are drastically reduced from a scale of a few tens of micrometers to a few hundreds of micrometers because of very strong coupling peculiar to PC waveguide couplers.

II. TWO-CHANNEL MUX–DEMUX

We consider a PC composed of dielectric pillars in air on square array with lattice constant $a$, as shown in Fig. 1, where the radius and the refractive index of rods are, respectively, taken as $r = 0.18a$ and $n = 3.4$. The crystal has a photonic bandgap (PBG) for transverse electric (TE) modes which extends from $\omega a/(2\pi c) = a/\lambda = 0.302$ to 0.443, but not for transverse magnetic (TM) modes, where $\omega$ is the angular frequency, $c$ the light velocity, and $\lambda$ the wavelength in free space.
Fig. 2. PC waveguide coupler with two rows of dielectric rods in the interaction region.

Fig. 3. Dispersion curves of even and odd modes in a PC waveguide coupler with two rows of rods in the interaction region.

Fig. 4. Field patterns for (a) even and (b) odd modes in a PC waveguide coupler with two rows of rods in the interaction region.

Fig. 5. Coupling length of a PC waveguide coupler with two rows of rods in the interaction region.

Fig. 6. Transmission spectrum of a PC waveguide coupler with two rows of rods for input pulses launched into (a) port 1 and (b) port 2.

Now, we propose a two-channel MUX–DEMUX based on a PC waveguide coupler with two rows of dielectric rods in the interaction region, as shown in Fig. 2, where $l$ is the interaction length and in order to separate two input and output waveguides, low-loss 90° bends [12] are introduced. Gently curved elements such as $S$ bends are not necessary because the PC waveguides with PBG have no radiation loss. Fig. 3 shows the dispersion curves of the guided even and odd modes propagating in the parallel PC waveguides where the dashed line is for the isolated single waveguide. The corresponding field patterns with the transverse profiles on the line defined by the centers of rods are shown in Fig. 4, where $\omega a/(2\pi c) = 0.35$. The difference between the effective indexes of the even and the odd modes is significantly large and, therefore, the coupling length $L_c$ is drastically reduced, as shown in Fig. 5, compared with the conventional dielectric waveguide couplers. The transmission spectrum for the structure in Fig. 2 with $l = 48\alpha$ is shown in Fig. 6 where an input pulse with a transverse profile corresponding to the fundamental mode of the isolated single waveguide and a Gaussian profile in the longitudinal direction is launched into port 1 or port 2. The interaction length of $48\alpha$ corresponds to the coupling length at frequency of $\omega_1'$, and is two to six times as large as the coupling lengths at $\omega_2'$ to $\omega_6'$, respectively (see Fig. 5).

Fig. 7 shows the field patterns observed in frequency domain. Irrespective of input ports, signals with frequencies of $\omega_1'$ and $\omega_2'$ are transferred to the opposite guide (cross state), and signals with frequencies of $\omega_2'$ and $\omega_4'$ are outputted from the original guide (bar state).
Fig. 7. Field patterns observed in frequency domain for input pulses launched into (a) port 1 and (b) port 2.

The channel spacing may be further reduced by increasing the device length or the wavelength dependence of the coupling coefficient. Here, as one of the latter examples, we consider a PC waveguide coupler as shown in Fig. 8, where the two straight waveguides are coupled through only one row of rods. Fig. 9 shows the dispersion curves. We can see from the unusual behaviors of the guided even and odd modes that the effective index of the even mode is smaller than that of the odd mode. This seems to be due to the fact that the modal field of the even mode resembles that of the higher order mode propagating in a conventional five layered dielectric waveguide, as shown in Fig. 10, where $\omega a/(2\pi c) = 0.35$. Fig. 11 shows the coupling length $L_{c1}$, which is further reduced, compared with that of the previous coupler with two rows of rods in the interaction region. The transmission spectrum for the structure in Fig. 8 with $l = 36a$ is shown in Fig. 12. As is expected, the channel spacing is reduced, compared with the structure in Fig. 2, but the return loss becomes larger.

III. FOUR-CHANNEL MUX–DEMUX

By cascading two stages of PC waveguide couplers with different coupling coefficients, a four-channel MUX–DEMUX is realized, as shown in Fig. 13. The iteration lengths, $l_1$, $l_2$, and $l_3$, are determined as

$$l_1 = L_{c2}(\omega_1) = 2L_{c2}(\omega_2) = 3L_{c2}(\omega_3) = 4L_{c2}(\omega_4)$$

(1)

$$l_2 = l_1/2 = L_{c2}(\omega_2) = 2L_{c2}(\omega_1)$$

(2)

$$l_3 = mL_{c1}(\omega_3) = mr' L_{c1}(\omega_3)$$

(3)

where $L_{c1}$ and $L_{c2}$ are the coupling lengths of PC waveguide couplers with one row and two rows of rods in the interaction region, respectively, and the difference between $m$ and $m'$ must be odd numbers. Multiplexed signals with frequencies of $\omega_1$ to $\omega_4$ launched into the left input port are demultiplexed and are outputted from ports 1–4, respectively.

The interaction lengths are now determined as $l_1 = 44a$, $l_2 = 22a$, and $l_3 = 23.4a$, based on the data of coupling lengths shown in Fig. 14. As the interaction length normalized by a
lattice constant $a$ in a PC waveguide coupler must be an integer, the length $l_3$ is approximated as $23a$. Fig. 15(a) shows the transmission spectrum. The response of port 3 is relatively low, compared with the others. This can be further improved by fine tuning the second stage of PC waveguide couplers. Fig. 15(b) shows the transmission spectrum for $l_3 = 24a$, resulting in a higher response from port 3.

If the lattice constant is assumed to be 0.54 $\mu$m, the perfect transmission in a 90° bend [12] is realized at the wavelength of 1.55 $\mu$m, and the device size is about 50 $\mu$m long and 30 $\mu$m wide.

IV. DISCUSSION ON CHANNEL SPACING

Numerical techniques are very powerful and can give accurate results, but large central processing unit times and memory allocations are, in general, required. In order to roughly estimate the interaction length necessary for a desired channel spacing, we use a simpler, well-established coupled-mode theory (CMT).
First, the validity of CMT is checked by reconsidering a four-channel MUX–DEMUX in Fig. 13. The normalized powers outputted from ports 1–4 are expressed as

\[ P_1 = \sin^2 \kappa_1 \cos^2 \kappa_4 I_3 \]  
\[ P_2 = \cos^2 \kappa_1 \sin^2 \kappa_2 I_3 \]  
\[ P_3 = \sin^2 \kappa_2 \cos^2 \kappa_3 I_3 \]  
\[ P_4 = \cos^2 \kappa_2 \cos^2 \kappa_3 I_3 \]  

with

\[ \kappa_i = \frac{\pi}{2L_i} = \frac{1}{L_i} \left( \beta_{e,i} - \beta_{o,i} \right) \]

where \( \kappa_i \) is the coupling coefficient, \( \beta_{e,i} \) and \( \beta_{o,i} \) are, respectively, the propagation constants for the even and the odd modes, and the subscripts \( i = 1 \text{ and } 2 \) stand for the PC waveguide couplers with one row and two rows of rods in the interaction region, respectively.

Fig. 16 shows the transmission spectrum calculated by CMT. With CMT, of course, reflections from 90° bends and local reflections in periodic PC structures cannot be evaluated. However, channel frequencies and channel spacings are surprisingly in good agreement with the previous results of FETD-BPM in Fig. 15.

Next, a two-channel MUX–DEMUX in Figs. 2 and 8 is considered, and the transmission spectrum is shown in Figs. 17 and 18, respectively, where the solid and dashed lines are for the bar and cross states, respectively. Assuming the lattice constant \( a = 0.54 \mu m \) as described before, the interaction length \( L \) for realizing 20-nm channel spacing required in WWDM systems is about 150\( a \) = 81 \( \mu m \) and 50\( a \) = 27 \( \mu m \) in the structures in Figs. 2 and 8, respectively.

Even for realizing 0.8-nm channel spacing required in DWDM systems, the interaction length \( L \) is only 3000\( a \) = 1620 \( \mu m \) and 1200\( a \) = 648 \( \mu m \) in the structures in Figs. 2 and 8, respectively. The channel spacing is approximately proportional to the interaction length.

For both 20-nm and 0.8-nm channel spacings, the interaction length of the structure in Fig. 8 is considerably reduced, compared with the one in Fig. 2.
ACKNOWLEDGMENT

The author would like to thank Dr. Y. Tsuji of Hokkaido University for interesting discussions and his support during the work, and the reviewer for his very valuable comments.

REFERENCES


Masanori Koshiba (SM’84) was born in Sapporo, Japan, on November 23, 1948. He received the B.S., M.S., and Ph.D. degrees in electronic engineering from Hokkaido University, Sapporo, Japan, in 1971, 1973, and 1976, respectively.

In 1976, he joined the Department of Electronic Engineering, Kitami Institute of Technology, Kitami, Japan. From 1979 to 1987, he was an Associate Professor of Electronic Engineering at Hokkaido University, and in 1987, he became a Professor there. He has been engaged in research on wave electronics, including microwaves, millimeter waves, lightwaves, surface acoustic waves (SAW), magnetostatic waves (MSW), electron waves, and computer-aided design and modeling of guided-wave devices. He is an author or coauthor of more than 200 research papers in English and of more than 100 research papers in Japanese, both in refereed journals. He authored the books Optical Waveguide Analysis and Optical Waveguide Theory by the Finite Element Method, and coauthored the books Analysis Methods for Electromagnetic Wave Problems, Ultrasound and Ultra-parallel Optoelectronics, and Finite Element Software for Microwave Engineering.

Dr. Koshiba is a member of the Institute of Electronics, Information, and Communication Engineers (IEICE) of Japan, the Institute of Electrical Engineers of Japan, the Institute of Image Information and Television Engineers of Japan, the Japan Society for Simulation Technology, the Japan Society for Computational Methods in Engineering, the Japan Society of Applied Electromagnetics and Mechanics, the Japan Society for Computational Engineering and Science, and the Applied Computational Electromagnetics Society (ACES). He was awarded the 1986, 1996, and 1998 Excellent Paper Awards from the IEICE, and in 1998, he received the Electronics Award from the IEICE Electronics Society. From 1999 to 2000, he served as a President of IEICE Electronics Society, and since 2000, he has been a member of the Board of Directors of ACES.