A Vector Finite Element Method With the High-Order Mixed-Interpolation-Type Triangular Elements for Optical Waveguiding Problems

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Abstract—A vector finite element method with the high-order mixed-interpolation-type triangular elements is described for the analysis of optical waveguiding problems. It is a combination of linear edge elements for transverse components of the electric or magnetic field and quadratic nodal elements for the axial one. The use of mixed-interpolation-type elements provides a direct solution for propagation constants and avoids spurious solutions. This approach can yield more accurate results compared with the conventional approach using the lowest order mixed-interpolation-type elements, namely, constant edge elements and linear nodal elements. The accuracy of this approach is investigated by calculating the propagation characteristics of optical rib waveguides. Results obtained for both $E^x$ and $E^y$ polarizations are validated using benchmark results produced by established methods.

I. INTRODUCTION

DIFFERENT types of the vector finite element method (VFEM) have been developed for the analysis of optical waveguiding problems. Of the various formulations, the VFEM using full vector electric or magnetic field is quite suitable for a wide range of practical complicated problems [1]–[13]. This approach has been widely used for various optical waveguiding structures and recently has been utilized as the optical waveguide solver of CAD packages [14]. The most serious problem associated with this approach is the appearance of spurious solutions. The penalty function method [1]–[14] has been used to cure this problem, but in this technique an arbitrary positive constant, called the penalty coefficient, is involved and the accuracy of solutions depends on its magnitude. Furthermore, in the full vectorial formulation the propagation constant is first given as an input datum, and subsequently the operating wavelength is obtained as a solution. There is another serious problem in the full vectorial approach. As was made clear by Birman [15] and Birman and Solomyak [16], such an approach is quite difficult for dealing with corner singularities and interface singularities so long as the conventional Lagrange interpolation polynomial functions are used to approximate vector fields. More recently, the VFEM with the lowest order mixed-interpolation-type triangular elements, namely, constant edge elements for transverse components of the electric or magnetic field and linear nodal (conventional Lagrange [1]–[14]) elements for the axial one, has been developed [17]–[19]. The use of mixed-interpolation-type elements provides a direct solution for propagation constants [18] and avoids spurious solutions [17]–[19], but the accuracy of the finite element analysis using the lowest order elements is, in general, insufficient.

In this paper, in order to provide more accurate numerical solutions and faster convergence in applications, a vector finite element method with the high-order mixed-interpolation-type triangular elements is formulated in detail. It is a combination of linear edge elements for transverse components of the electric or magnetic field and quadratic nodal (conventional Lagrange) elements for the axial one. This approach can yield more accurate results compared with the conventional approach using the lowest order elements. The accuracy of this approach is investigated by calculating the propagation characteristics of optical rib waveguides. Results obtained for both $E^x$ and $E^y$ polarizations are validated using benchmark results produced by established methods.

II. BASIC EQUATIONS

We consider an optical waveguide with an arbitrary cross section $\Omega$ in the $xy$ plane. With a time dependence of the form $\exp(j\omega t)$ being implied, from Maxwell's equations the following vectorial wave equation is derived:

$$\nabla \times (p \nabla \times \phi) - k_0^2 [q] \phi = 0$$  \hspace{1cm} (1)

with

$$[p] = \begin{bmatrix} p_x & 0 & 0 \\ 0 & p_y & 0 \\ 0 & 0 & p_z \end{bmatrix}$$  \hspace{1cm} (2)

$$[q] = \begin{bmatrix} q_x & 0 & 0 \\ 0 & q_y & 0 \\ 0 & 0 & q_z \end{bmatrix}$$  \hspace{1cm} (3)

where $\omega$ is the angular frequency, $k_0$ is the free-space wavenumber, $\phi$ denotes either the electric field $E$ or the magnetic field $H$, and the components of $[p]$ and $[q]$ are given...
III. MIXED-INTERPOLATION-TYPE TRIANGULAR ELEMENTS

The electromagnetic fields have to be tangentially continuous across material interfaces.

Fig. 1(a) shows the lowest order mixed-interpolation-type triangular element [17]–[19] which is composed of a constant edge element with three tangential unknowns, \( \phi_{t1} \) to \( \phi_{t3} \), and a linear nodal (conventional Lagrange) element with six axial unknowns, \( \phi_{a1} \) to \( \phi_{a3} \). Since both \( \phi_{t} \) and \( \phi_{a} \) are tangential to material interfaces, the tangential continuity can be straightforwardly imposed in the mixed-interpolation-type element analysis. In this lowest order element the tangential component \( \phi_{t} = \phi \cdot t \) is constant along each side of triangles, where \( t \) is the unit tangential vector whose direction is coincident with that of \( \phi_{t} \), as shown in Fig. 1(a). It is for this reason that the edge element in Fig. 1(a) is called the constant edge element.

\[
p_x = p_y = p_z = 1, \quad q_x = n_x^2, \quad q_y = n_y^2, \quad q_z = n_z^2, \quad \text{for } \phi = E \\
p_x = 1/n_x^2, \quad p_y = 1/n_y^2, \quad p_z = 1/n_z^2, \quad q_x = q_y = q_z = 1, \quad \text{for } \phi = H. \tag{5}
\]

Here \( n_x, n_y, n_z \) are the refractive indices in the \( x, y, z \) directions, respectively.

The functional for (1) is given by

\[
F = \iint_{\Omega} \left[ (\nabla \times \phi)^* \cdot ([p]\nabla \times \phi) - k_0^2 [q] \phi^* \cdot \phi \right] dx dy \tag{6}
\]

where the asterisk denotes complex conjugate.

IV. FINITE ELEMENT DISCRETIZATION

Dividing the waveguide cross section \( \Omega \) into a number of mixed-interpolation-type triangular elements, as shown in Fig. 1, we expand the transverse components \( \phi_x, \phi_y \) and the axial component \( \phi_z \) in each element as

\[
\phi = \begin{bmatrix} \phi_x \\ \phi_y \\ \phi_z \end{bmatrix} = \begin{bmatrix} \{U\}^T \{\phi_t\}_e \\ \{V\}^T \{\phi_t\}_e \\ \{N\}^T \{\phi_t\}_e \end{bmatrix} \tag{7}
\]

where \( \{\phi_t\}_e \) is the edge variables in the transverse plane for each element, \( \{\phi_t\}_e \) is the nodal axial-field vector for each element, and \( T \) denotes a transpose. The shape function vectors for edge elements \( \{U\} \) and \( \{V\} \) and the ordinary shape function vector for nodal elements \( \{N\} \) are given in Table I, where the area coordinates \( L_k \) \((k = 1, 2, 3)\), the area of the element \( A_e \), the length of the side between two corner points \((x_k, y_k)\) and \((x_l, y_l)\), \( |L_k| \), and coefficients \( a_k, b_k, c_k \) are given by

\[
\begin{bmatrix} L_1 \\ L_2 \\ L_3 \end{bmatrix} = \frac{1}{2A_e} \begin{bmatrix} a_1 & b_1 & c_1 \\ a_2 & b_2 & c_2 \\ a_3 & b_3 & c_3 \end{bmatrix} \begin{bmatrix} 1 \\ x \\ y \end{bmatrix}. \tag{8}
\]
TABLE II

<table>
<thead>
<tr>
<th>Elements</th>
<th>( {U_2} )</th>
<th>( {V_2} )</th>
<th>( {N_x} )</th>
<th>( {N_y} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>Constant edge and linear</td>
<td>( \frac{1}{2A_e} )</td>
<td>( \frac{1}{2A_e} )</td>
<td>( \frac{1}{2A_e} )</td>
<td>( \frac{1}{2A_e} )</td>
</tr>
<tr>
<td>nodal elements</td>
<td>(-l_1)</td>
<td>(-l_2)</td>
<td>(-l_3)</td>
<td>(-l_4)</td>
</tr>
<tr>
<td>Linear edge</td>
<td>( \frac{1}{4A_e^2} )</td>
<td>( \frac{1}{4A_e^2} )</td>
<td>( \frac{1}{4A_e^2} )</td>
<td>( \frac{1}{4A_e^2} )</td>
</tr>
<tr>
<td>and quadratic</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>nodal elements</td>
<td>( l_1 b_{y0} )</td>
<td>( l_2 b_{y0} )</td>
<td>( l_3 b_{y0} )</td>
<td>( l_4 b_{y0} )</td>
</tr>
<tr>
<td></td>
<td>(-l_1 b_{x0} )</td>
<td>(-l_2 b_{x0} )</td>
<td>(-l_3 b_{x0} )</td>
<td>(-l_4 b_{x0} )</td>
</tr>
<tr>
<td></td>
<td>( b_i (4L_i - 1) )</td>
<td>( b_i (4L_i - 1) )</td>
<td>( b_i (4L_i - 1) )</td>
<td>( b_i (4L_i - 1) )</td>
</tr>
<tr>
<td></td>
<td>( c_i (4L_i - 1) )</td>
<td>( c_i (4L_i - 1) )</td>
<td>( c_i (4L_i - 1) )</td>
<td>( c_i (4L_i - 1) )</td>
</tr>
</tbody>
</table>

Substituting (7) into (6) and using the same procedure as [18], we obtain the following final eigenvalue problem which gives a solution directly for the propagation constant \( \beta \) and the corresponding field distribution and involves only the edge variables in the transverse plane \( \phi_k \):

\[
[K_{tt}] \{ \phi_k \} - \beta^2 [M_{tt}] + [K_{zz}] [K_{zz}]^{-1} [K_{zt}] \{ \phi_k \} = \{0\}
\]

with

\[
[K_{tt}] = \sum_e \int \left[ g_x k_0^2 \{U\} \{U\}^T + g_y k_0^2 \{V\} \{V\}^T - p_x \{U\} \{U\}^T - p_z \{V\} \{V\}^T \right] \, dx \, dy
\]

\[
[K_{zz}] = \sum_e \int \left[ p_y \{N_x\} \{N_x\}^T + p_x \{V\} \{V\}^T \right] \, dx \, dy
\]

\[
[M_{tt}] = \sum_e \int \left[ p_y \{N_y\} \{N_y\}^T \right] \, dx \, dy
\]

where \( \{0\} \) is a null vector, \( \{U\} = \partial\{U\}/\partial y \), \( \{V\} = \partial\{V\}/\partial x \), \( \{N_x\} = \partial\{N\}/\partial x \), \( \{N_y\} = \partial\{N\}/\partial y \), and their explicit forms are given in Table II. The integrals necessary to construct element matrices are summarized in the Appendix.

Using (9) to (13) and the Appendix, we can easily construct the matrices \([K_{tt}], [K_{zz}], [K_{zt}], [K_{zt}], [M_{tt}]\).

V. NUMERICAL RESULTS

First, in order to check the accuracy of the VFEM with mixed-interpolation-type triangular elements, a half-filled dielectric waveguide as shown in Fig. 2(a) was considered, where \( W = 2h \). Fig. 2(b) shows a typical element division profile.

Fig. 3 shows the relative error of the computed \( \beta \) for the fundamental LSE\(_{10}\) mode in a rectangular waveguide.
Fig. 2. Dielectric-loaded waveguide. (a) Waveguide structure. (b) Element division.

Fig. 3. Convergence of finite element solutions for the fundamental LS$_{10}$ mode in a dielectric-loaded waveguide.

Fig. 4. Optical rib waveguide. (a) Waveguide structure. (b) Element division.

inhomogeneously loaded with dielectric of refractive index 1.5, where $\phi = H, k_0 h = 3.0, N_t$ and $N_x$ are the numbers of nodes for tangential and axial components, respectively, and $N_t + N_x$ corresponds to the number of degrees of freedom. The relative error is given by

$$\text{relative error} = \frac{\beta_{\text{exact}} - \beta_{\text{FEM}}}{\beta_{\text{exact}}} \quad (20)$$

where $\beta_{\text{exact}}$ and $\beta_{\text{FEM}}$ are the exact and computed values, respectively. It is confirmed from Fig. 3 that the VFEM with the high-order mixed-interpolation-type elements (linear edge and quadratic nodal elements) can give more accurate results than the VFEM with the lowest order ones (constant edge and linear nodal elements).

Next, the VFEM with mixed-interpolation-type triangular elements was used to analyze a series of rib waveguides [8], [25]–[27] having, in the notation of Fig. 4(a), rib width $W = 3 \mu m$ and superstrate depth $t + h = 1 \mu m$, where $h$ is the etch depth. The outer slab depth varies from $0 \mu m$ to 0.9 $\mu m$. The refractive indices of the film, substrate, and cover are $n_f = 3.44, n_s = 3.40$, and $n_c = 1.0$, respectively. The operating wavelength is 1.15 $\mu m$. Fig. 4(b) shows a typical element division profile, where symmetry conditions are used and only one-half of the waveguide cross section is subdivided into linear edge and quadratic nodal elements.

Fig. 5 shows the normalized propagation constant $b$ for the fundamental $E_x (E_{11}^x)$ and the fundamental $E_y (E_{11}^y)$ modes, where $b$ is defined as

$$b = \frac{(\beta/k_0)^2 - n_s^2}{n_f^2 - n_s^2} \quad (21)$$

and $\phi = H$ and $\phi = E$ for the calculation of the $E_{11}^x$ and $E_{11}^y$ modes, respectively. The results of the VFEM with constant edge and linear nodal elements, the VFEM combined with the penalty function method [8], the effective index method (EIM) [25], the scalar finite difference method (SFDM) [26], and the scalar finite element method (SFEM) [27] are also given in Fig. 5. When using a VFEM with the high-order or the lowest-order mixed-interpolation-type elements, the number of elements is 288 or 352, respectively.

The results of the VFEM with the high-order mixed-interpolation-type elements for the $E_{11}^x$ mode agree excellently with those of the VFEM combined with the penalty function method [8]. Note that the penalty function method cannot provide a direct solution for the propagation constant and that an extra stage of iteration may be needed if the solution is required at a particular wavelength. The results of the penalty function method have not been reported for the $E_{11}^y$ modes. It is readily seen from Fig. 5 that the accuracy of the VFEM
with the lowest-order mixed-interpolation-type elements is not sufficient. It is also found that for both the \( E_{T1}^+ \) and \( E_{T1}^- \) modes, the results of the VFEM with the high-order mixed-interpolation-type elements agree well with those of the SFDM [26] and the SFEM [27]. For detailed comparison the results are summarized in Table III.

Numerical computations for the test problems show the nonappearance of spurious solutions when both the high-order and the lowest-order mixed-interpolation-type elements are used without any other supplementary technique.

### VI. CONCLUSION

A vector finite element method for the analysis of optical waveguiding problems was formulated using the high-order mixed-interpolation-type triangular elements in detail. It is a combination of linear edge elements for transverse components of the electric or magnetic field and quadratic nodal elements for the axial one. This approach can yield more accurate results compared with the conventional approach using the lowest-order mixed-interpolation-type elements, namely, constant edge elements and linear nodal elements. The accuracy of this approach was investigated by calculating the propagation characteristics of optical rib waveguides.

### VII. APPENDIX

The integrals necessary to construct element matrices are calculated as follows.

**Constant Edge and Linear Nodal Elements:**

\[
\begin{align*}
\int_U \{U\}^T \{U\} \, dx \, dy &= \frac{1}{4A_e} l_i l_j \left[ y_{i+2} y_{j+2} - y_e (y_{i+2} + y_{j+2}) \right. \\
&\quad + \frac{1}{12} (y_1^2 + y_2^2 + y_3^2 + 9y_e^2) \\
\int_V \{V\}^T \{V\} \, dx \, dy &= \frac{1}{4A_e} l_i l_j \left[ x_{i+2} x_{j+2} - x_e (x_{i+2} + x_{j+2}) \right. \\
&\quad + \frac{1}{12} (x_1^2 + x_2^2 + x_3^2 + 9x_e^2)
\end{align*}
\]

This approach can be applied easily to the optical waveguides including lossy and/or active media.
\[
\begin{align*}
\int_{e} \{U\} \{N_x\}^T dx \ dy &= \frac{1}{4A_e} l_i b_j (y_{i+2} - y_c) \quad (A4) \\
\int_{e} \{V\} \{N_y\}^T dx \ dy &= \frac{1}{4A_e} l_i c_j (x_c - x_{i+2}) \quad (A5) \\
\int_{e} \{N\} \{N\}^T dx \ dy &= \begin{cases} A_e/6, & \text{for } i = j \\ A_e/12, & \text{for } i \neq j \end{cases} \quad (A6) \\
\int_{e} \{N_x\} \{N_x\}^T dx \ dy &= \frac{1}{4A_e} b_i b_j \quad (A7) \\
\int_{e} \{N_y\} \{N_y\}^T dx \ dy &= \frac{1}{4A_e} c_i c_j \quad (A8)
\end{align*}
\]

with
\[
\begin{align*}
x_c &= (x_1 + x_2 + x_3)/3 \quad (A9) \\
y_c &= (y_1 + y_2 + y_3)/3 \quad (A10)
\end{align*}
\]

where \([,]_{ij} (ij = 11, 12, \ldots, 33)\) indicates the \((i, j)\) component of the matrix \([,]\), and the subscripts \(i, j\) always progress modulo 3.

Linear Edge and Quadratic Nodal Elements:
\[
\begin{align*}
\int_{e} \{U\} \{U\}^T dx \ dy &= \begin{cases} A_e/6 u_i u_j & \text{for } ij = 11, 22, 33, 44, 55, 66, 16, 61, 24, 42, 35, 53 \quad (A11) \\ A_e/12 u_i u_j, & \text{for others} \end{cases} \\
\int_{e} \{V\} \{V\}^T dx \ dy &= \begin{cases} A_e/6 v_i v_j & \text{for } ij = 11, 22, 33, 44, 55, 66, 16, 61, 24, 42, 35, 53 \quad (A12) \\ A_e/12 v_i v_j, & \text{for others} \end{cases}
\end{align*}
\]
\[
\begin{align*}
\int_{e} \{U\} \{U\}^T dx \ dy &= A_e u_{i+y} u_{yj} \quad (A13) \\
\int_{e} \{V\} \{V\}^T dx \ dy &= A_e v_{i+y} v_{xj} \quad (A14) \\
\int_{e} \{U\} \{V\}^T dx \ dy &= A_e u_{i+y} v_{xj} \quad (A15)
\end{align*}
\]
\[
\int_V \{N_y\}^T \{N\} dx dy = \frac{A_e}{180} \begin{bmatrix}
6 & -1 & -1 & 0 & -4 & 0 \\
-1 & 6 & 1 & 0 & 0 & -4 \\
0 & 0 & -4 & 32 & 16 & 16 \\
16 & 32 & 16 & 32 & 16 & 32
\end{bmatrix}
\tag{A29}
\]

\[
\int_V \{N_x\}^T \{N_x\} dx dy = \frac{A_e}{6} \left[ \begin{array}{c}
C^{(1)}_{y_1} C^{(1)}_{y_2} + C^{(2)}_{y_1} C^{(2)}_{y_2} + C^{(3)}_{y_1} C^{(3)}_{y_2} \\
C^{(1)}_{y_1} C^{(2)}_{y_2} + C^{(2)}_{y_1} C^{(1)}_{y_2} + C^{(3)}_{y_1} C^{(2)}_{y_2} \\
C^{(1)}_{y_1} C^{(3)}_{y_2} + C^{(3)}_{y_1} C^{(1)}_{y_2} + C^{(2)}_{y_1} C^{(3)}_{y_2} \\
C^{(1)}_{y_1} C^{(4)}_{y_2} + C^{(4)}_{y_1} C^{(1)}_{y_2} + C^{(2)}_{y_1} C^{(4)}_{y_2} \\
C^{(1)}_{y_1} C^{(5)}_{y_2} + C^{(5)}_{y_1} C^{(1)}_{y_2} + C^{(3)}_{y_1} C^{(5)}_{y_2} \\
C^{(1)}_{y_1} C^{(6)}_{y_2} + C^{(6)}_{y_1} C^{(1)}_{y_2} + C^{(4)}_{y_1} C^{(6)}_{y_2}
\end{array} \right]
\tag{A30}
\]

\[
\int_V \{N_y\}^T \{N_y\} dx dy = \frac{A_e}{6} \left[ \begin{array}{c}
C^{(1)}_{y_1} C^{(1)}_{y_2} + C^{(2)}_{y_1} C^{(2)}_{y_2} + C^{(3)}_{y_1} C^{(3)}_{y_2} \\
C^{(1)}_{y_1} C^{(2)}_{y_2} + C^{(2)}_{y_1} C^{(1)}_{y_2} + C^{(3)}_{y_1} C^{(2)}_{y_2} \\
C^{(1)}_{y_1} C^{(3)}_{y_2} + C^{(3)}_{y_1} C^{(1)}_{y_2} + C^{(2)}_{y_1} C^{(3)}_{y_2} \\
C^{(1)}_{y_1} C^{(4)}_{y_2} + C^{(4)}_{y_1} C^{(1)}_{y_2} + C^{(2)}_{y_1} C^{(4)}_{y_2} \\
C^{(1)}_{y_1} C^{(5)}_{y_2} + C^{(5)}_{y_1} C^{(1)}_{y_2} + C^{(3)}_{y_1} C^{(5)}_{y_2} \\
C^{(1)}_{y_1} C^{(6)}_{y_2} + C^{(6)}_{y_1} C^{(1)}_{y_2} + C^{(4)}_{y_1} C^{(6)}_{y_2}
\end{array} \right]
\tag{A31}
\]

where \([i,j] \ (i,j = 11, 12, \ldots, 66)\) indicates the \((i,j)\) component of the matrix \([\cdot]\), and the values of \(u_i, v_i, u_{y_i}, v_{y_i}, C^{(1)}_{z_i}\) to \(C^{(4)}_{y_i}\) are listed in Table IV.

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References


Manasori Koshiba, photograph and biography not available at the time of publication.

Shinji Maruyama, photograph and biography not available at the time of publication.

Koichi Hirayama, photograph and biography not available at the time of publication.