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Abstract

Soil carbon dioxide (CO$_2$) efflux was measured continuously for two years using an automated chamber system in an oil palm plantation on tropical peat. This study investigated the factors controlling the CO$_2$ efflux and quantified the annual cumulative CO$_2$ emissions through soil respiration and heterotrophic respiration, which is equivalent to oxidative peat decomposition. Soil respiration was measured in close-to-tree (<2.5 m, CT) and far-from-tree (>3 m, FT) plots, and heterotrophic respiration was measured in root-cut (RC) plots by a trenching method. The daily mean CO$_2$ efflux values (mean ± 1 standard deviation) were 2.80 ± 2.18, 1.59 ± 1.18, and 1.94 ± 1.58 µmol m$^{-2}$ s$^{-1}$ in the CT, FT, and RC plots, respectively. Daily mean CO$_2$ efflux increased exponentially as the groundwater level or water-filled pore space decreased, indicating that oxidative peat decomposition and gas diffusion in the soil increased due to enhanced aeration resulting from lower groundwater levels. Mean annual gap-filled CO$_2$ emissions were 1.03 ± 0.53, 0.59 ± 0.26, and 0.69 ± 0.21 kg C m$^{-2}$ yr$^{-1}$ in the CT, FT, and RC plots, respectively. Soil CO$_2$ emissions were significantly higher in the CT plots ($P < 0.05$), but did not differ significantly between the FT and RC plots. This implies that root respiration was negligible in the FT plots. Heterotrophic respiration accounted for 66% of soil respiration. Annual CO$_2$ emissions through both soil and heterotrophic respiration were smaller than those of other oil palm plantations on tropical peat, possibly due to the higher groundwater levels, land compaction, and continuous measurement of soil CO$_2$ efflux in this study. Mean annual total subsidence was 1.55 to 1.62 cm yr$^{-1}$, of which oxidative peat decomposition accounted for 72 to 74%. In conclusion, water management to raise groundwater levels would mitigate soil CO$_2$ emissions from oil palm plantations on tropical peatland.
Keywords
Automated chamber system; Carbon dioxide efflux; Groundwater level; Heterotrophic respiration; Soil respiration; Subsidence; Trenching

1. Introduction

Peatland stocks approximately one-third of the global terrestrial carbon (C) in 3% of the global terrestrial area (Maltby and Immirzi, 1993), and approximately 25 Mha are in Southeast Asia, especially in Indonesia and Malaysia (Page et al., 2011). However, tropical peatland has been rapidly reclaimed since the 1990s, mainly for oil palm and Acacia plantations. By 2015, oil palm plantations had expanded to cover an area of 4.3 Mha on peat in Indonesia and Malaysia (Miettinen et al., 2016). Because the agricultural use of tropical peatland is commonly accompanied by drainage, the aerobic mineralization of peat soil is promoted, resulting in large carbon dioxide (CO$_2$) emissions (e.g., Furukawa et al., 2005; Couwenberg et al., 2010; Hooijer et al., 2012). Peat is usually compacted using heavy machinery before planting in Malaysia to enhance its bearing capacity for trees and to increase soil moisture via capillary water rise (Dislich et al., 2016). This compaction practice is expected to depress peat oxidative decomposition due to the increase in soil water content and decrease in soil gas diffusivity (Melling et al., 2005, 2013a).

It has been reported that CO$_2$ emissions from tropical drained peatland are an important part of the global C cycle (Sjögersten et al., 2014; Miettinen et al., 2017), and therefore it is important to quantify oxidative peat decomposition or heterotrophic respiration ($R_{H}$) from total soil respiration ($R_{S}$) separately. However, there have been few
studies of $R_H$ in tropical peatland, despite $R_H$ being an important component of $R_S$ that corresponds to oxidative peat decomposition. For oil palm plantations on peat, some studies have measured $R_H$ periodically at intervals of one or more months for periods equal to or less than 1 year (Melling et al., 2005, 2013a, 2013b; Dariah et al., 2014; Husnain et al., 2014; Marwanto and Agus, 2014; Sakata et al., 2015; Comeau et al., 2016). Due to the limitations of field studies, the controlling factors of soil CO$_2$ efflux are not well understood at the process level. For example, it was reported that no significant relationship exists between $R_S$ and groundwater level (GWL) (Jauhiainen et al., 2008), probably due to the disconnection of capillary force under dry conditions, resulting in soil moisture in the topsoil becoming decoupled from the GWL (Ishikura et al., 2017). Soil moisture in the topsoil can be a better predictor than GWL for soil CO$_2$ efflux (Melling et al., 2005, 2013a), because soil moisture is affected more by capillary rise than GWL when a peat soil is compacted (Price, 1997; Michel et al., 2001). However, the relationship between soil CO$_2$ efflux and soil moisture in tropical peat ecosystems is still not well understood. For a better understanding, long-term continuous measurement of both $R_S$ and $R_H$ is necessary to capture diurnal variation, detect the response of soil CO$_2$ efflux to dynamic environmental variations, and reduce the uncertainties in assessment of annual CO$_2$ emissions. To our knowledge, no studies have measured $R_S$ and $R_H$ continuously in an oil palm plantation on peat.

Oxidative peat decomposition induces subsidence together with physical consolidation and shrinkage (Stephens and Stewart, 1976; Wösten et al., 1997; Hooijer et al., 2012). If the contribution of peat oxidation to total subsidence is determined, CO$_2$ emissions through peat decomposition can be estimated from subsidence monitoring (Couwenberg and Hooijer, 2013). However, the extent of this contribution has not yet been determined,
because it depends on peat conditions, such as GWL and the time since drainage. Field studies involving simultaneous measurement of peat subsidence and oxidative peat decomposition could enable this to be determined, but only a few studies have been reported (Wakhid et al., 2017).

Therefore, $R_S$ and $R_H$ due to oxidative peat decomposition were measured continuously for two years using an automated chamber system, together with GWL, soil moisture, and peat subsidence in an oil palm plantation established on tropical peat. The objectives of this study were to investigate seasonal changes in $R_S$ and $R_H$ in relation to soil water conditions, quantify annual cumulative $R_S$ and $R_H$ values, and evaluate the contribution of oxidative peat decomposition to subsidence.

2. Material and methods

2.1 Site description

This study was conducted in an oil palm (Elaeis guineensis Jacqu.) plantation (2°11’N, 111°50’E) in a watershed of the Rajang River in Sibu, Sarawak, Malaysia (Fig. 1) at an elevation of approximately 25 m above sea level. The mean annual air temperature and precipitation between 2004 and 2016 were 26.5 ± 0.2°C and 2,915 ± 213 mm yr$^{-1}$ (mean ± 1 standard deviation (SD)), respectively, at the Sungai Salim B meteorological station (Department of Irrigation and Drainage Malaysia), which is 7.4 km from the study site.

In September 2004, a mixed peat swamp forest on an ombrotrophic peat dome was converted to an oil palm plantation, with the installation of ditches and water gates; artificial compaction to prevent palms from leaning and toppling was performed during land preparation. The soil type was a Sapric Histosol (IUSS Working Group WRB, 2015), with a peat depth of 12.7 m. Palm seedlings were planted on a triangular grid spacing of...
8.5 m between trees (153 trees ha\(^{-1}\); Fig. 2), and the ground was sparsely covered by fern plants (*Stenochlaena palustris* (Burm. f.) Bedd.). The lower fronds of oil palm trees were periodically lopped and piled in inter-row spaces. Thus, little leaf litter accumulated on the ground, except for some areas with fern plants. In 2014, the palm trees were 9 years old, and the canopy height was about 8 m. Oil palm plantations are commonly replanted every 25–30 years (Basiron, 2007), so the study site was in the first cycle of cultivation. The following fertilizers were applied together four times a year (January, March, July–August, and September–October) within 1 m of each stem: 74–147 kg N ha\(^{-1}\) yr\(^{-1}\) of urea, 7–9 kg P ha\(^{-1}\) yr\(^{-1}\) of rock phosphate, and 239–311 kg K ha\(^{-1}\) yr\(^{-1}\) of muriate of potash (KCl). Copper, zinc, and boron were applied as micronutrients at 8–16 kg ha\(^{-1}\) yr\(^{-1}\) in May–June every year, and kieserite (MgSO\(_4\)-H\(_2\)O) was also applied at rates of 80 kg ha\(^{-1}\) in October 2014, 119 kg ha\(^{-1}\) in May 2015, and 80 kg ha\(^{-1}\) in January 2016, respectively.

### 2.2 Experimental design and chamber measurement

In April 2014, an experimental area without fern plants was established, and the following treatments were applied (Fig. 2):

- Close-to-tree (CT, four plots): distance from the nearest tree < 2.5 m, corresponding to \(R_s\).
- Far-from-tree (FT, four plots): distance from the nearest tree > 3 m, corresponding to \(R_s\).
- Root-cut (RC, four plots): distance from the nearest tree > 3 m with trenching, corresponding to \(R_h\).

In each RC plot, four stainless steel plates were inserted surrounding an area of 40 × 80 cm\(^2\). The depth of insertion was 80 cm, which was almost equivalent to the lowest GWL. In May 2014, 1 month later, an automated chamber system was installed in the
experimental area. The system consisted of 16 chambers, an infrared CO\(_2\) analyzer (LI-820, LI-COR, Inc., Lincoln, Nebraska, USA), a programmable data logger (CR1000, Campbell Scientific Inc., Logan, Utah, USA), and an air pump and solenoid valves (Hirano et al., 2009). The chamber consisted of an opaque polyvinyl chloride (PVC) cylinder (height: 40 cm; inner diameter: 25 cm). Chambers were inserted 2–3 cm deep into the soil. One chamber was installed in each CT and FT plot, and two chambers were installed in each RC plot (Fig. 2).

An opaque PVC lid was attached to the chamber top that opened vertically and closed under the control of the data logger. Each chamber closed for 225 s in sequence, one after the other, and it took 1 h for all chambers to close/open in rotation. The air in the headspace of each chamber was circulated through the CO\(_2\) analyzer when the chambers were closed. The CO\(_2\) concentration was measured at 10-s intervals and recorded in the data logger. In August 2015, a greenhouse gas analyzer (Ultraportable Greenhouse Gas Analyzer 915-0011, Los Gatos Research, Inc., San Jose, California, USA) was placed in the air circulation line to measure CO\(_2\), methane, and water vapor concentrations.

Although measurements began in May 2014, data for a two-year period from January 2015 were used, because additional CO\(_2\) emissions resulting from the decomposition of dead roots left in the trenched plots were expected to occur for several months after trenching (Hanson et al., 2000; Comeau et al., 2016). One palm tree fell on a chamber in a CT plot in August 2015, and the chamber was then moved to an FT position. Thus, the number of CT plots decreased to three, while the number of FT plots increased to five in 2016. CO\(_2\) data from the CO\(_2\) analyzer were primarily used; data from the greenhouse gas analyzer were used as an alternative when the LI-820 malfunctioned. During the two years of 2015 and 2016, 23% of the data was lost, mainly due to power problems.
Soil CO\textsubscript{2} efflux was calculated from the increase in CO\textsubscript{2} concentration in the chamber headspace during the 90–220 s after the chamber closing:

\[ F = \frac{PH}{RT_{\text{air}}} \frac{dC}{dt} \]  

(1)

where \( F \) is soil CO\textsubscript{2} efflux (\( \mu \text{mol m}^{-2} \text{s}^{-1} \)), \( P \) is air pressure (101.325 kPa), \( H \) is the aboveground height of a chamber, \( R \) is the gas constant (8.314 Pa m\textsuperscript{3} K\textsuperscript{-1} mol\textsuperscript{-1}), \( T_{\text{air}} \) is air temperature (K), and \( \frac{dC}{dt} \) is the rate of increase of the CO\textsubscript{2} concentration (\( \mu \text{mol mol}^{-1} \text{s}^{-1} \)). The quality of soil CO\textsubscript{2} efflux data was controlled as follows:

1. Significant slope: the Pearson’s correlation coefficient for the rate of increase in the CO\textsubscript{2} concentration should be higher than 0.661376 (\( P < 0.01, n = 14 \));
2. Stationary slope: the rates of increase in CO\textsubscript{2} concentration from 90–150 s and from 160–220 s after closing were calculated separately. The difference between the means of the two rates and the rate during the whole period (90–220 s) should be less than 30% (Aguilos et al., 2013);
3. Outliers: the CO\textsubscript{2} flux should be within 0–40 \( \mu \text{mol m}^{-2} \text{s}^{-1} \).

After these quality control criteria were applied, 43% of the data remained available. Because no litter accumulated in any chamber, CO\textsubscript{2} emissions resulting from leaf litter decomposition were not included in either \( R_S \) or \( R_H \) in this study. The CO\textsubscript{2} fluxes measured by the two CO\textsubscript{2} analyzers did not differ significantly from each other (Fig. S1).

2.3 **Environmental properties**

Precipitation was observed at a height of 1 m in an open space about 5 m away from the experimental area. However, some data were lost due to power problems, and precipitation data from the Sungai Salim B meteorological station were therefore used to record annual precipitation. The friction velocity (\( u^* \), m s\textsuperscript{-1} ) was measured at a height of
21 m above the vegetation canopy using a sonic anemometer (CSAT3, Campbell Scientific Inc.) and was used as an index of atmospheric turbulence.

Air and soil temperatures (°C) at a depth of 5 cm were measured using thermocouple thermometers in the same two chambers in FT plots. The GWL (m, negative values represent belowground) was measured using a piezometer (HTV-050KP, Sensez, Tokyo, Japan) at one point (Fig. 2), and volumetric soil water content (m³ m⁻³) at 0–30-cm depth was measured using a time-domain reflectometry (TDR) sensor (CS616, Campbell Scientific Inc.) in FT and RC plots, respectively (Fig. 2). Half-hourly means of these belowground variables were also recorded to the data logger used for the chamber system. Missing daily mean GWLs were gap-filled by a tank model (He and Inoue, 2015). The water retention curve was fitted to the relationship between daily mean GWL and soil water content using van Genuchten’s model (van Genuchten, 1980):

\[ \theta = \theta_{\text{res}} + \frac{\theta_{\text{sat}} - \theta_{\text{res}}}{(1 + (\alpha h)^n)^{1-1/n}} \]  

(2)

where \( \theta \) is the soil water content, \( \theta_{\text{sat}} \) is the saturated soil water content (equivalent to the porosity explained below), \( h \) is the pressure head (= −100 × GWL, cm), and \( \alpha, n, \) and \( \theta_{\text{res}} \) are fitting parameters, respectively. Missing daily mean soil water contents were gap-filled from the GWL using the water retention curve (Fig. S3).

In June 2014, six undisturbed soil cores of 100 cm³ were taken to a depth of 60 cm at intervals of 10 cm using a stainless soil core cylinder. Bulk density (Mg m⁻³) and porosity (m³ m⁻³) were determined using a digital soil volume analyzer (DIK-1110, Daiki Rika Company, Saitama, Japan). A further three disturbed soil samples were taken to a depth of 60 cm at intervals of 10 cm, and the total C and nitrogen (N) contents (%) were analyzed by the dry combustion method (TruMac CN, LECO Corporation, St. Joseph,
Michigan, USA. Other undisturbed soil cores of 100 cm$^3$ were taken from depths of 0–5, 5–10, 10–20, and 20–30 cm every month during the study period, and the volumetric soil water content was determined using the digital soil volume analyzer. Volumetric soil water content measured by the TDR sensor was calibrated using the soil water content measured by the soil core method. Water-filled pore space (WFPS, m$^3$ m$^{-3}$) was calculated from the proportion of soil water content to soil porosity.

In February 2017, disturbed topsoil at a depth of 0–30 cm was sampled in four replicate locations around the experimental area. Soil pH (1:2.5 H$_2$O) was measured using a digital pH meter (827 pH Lab, Metrohm AG, Herisau, Switzerland). Ash content (%) was analyzed by loss-on-ignition (TGA701, LECO Corporation) at 800°C for more than 1 h.

To measure fine root biomass (diameter: <2 mm), 100 cm$^3$ soil cores were taken at a depth of 0–10 cm at 1, 2, and 3 m from the four nearest palm trees, respectively. The soil samples were washed and sieved through a 2-mm mesh. Living fine roots were picked out by visual assessment and elasticity, and dried at 75°C for more than 48 h to measure biomass.

2.4 Subsidence and the contribution of peat decomposition

In May 2014, a subsidence pole with a marking disk was installed vertically into the soil until it reached the mineral soil beneath the peat. Because the measurement height of the pole from the ground surface was affected by the roughness of the ground, the marking disk was used to take an average. The disk could move freely along the anchored pole, and thus was always resting on the ground surface. The heights from the disk on the ground to the top of the pole were measured manually on four sides and averaged every month from June 2014. Annual subsidence was calculated as the cumulative subsidence from January in one year to January in the following year.

Subsidence through oxidative peat decomposition ($S_{RH}$, cm period$^{-1}$) was calculated
using the following equation (Wakhid et al., 2017):

$$S_{RH} = \frac{\text{Cumulative } R_H}{10 \cdot BD \cdot TC}$$  \hspace{1cm} (3)

where cumulative $R_H$ (kg C m$^{-2}$ period$^{-1}$) is the cumulative CO$_2$ emission in RC plots, BD (Mg m$^{-3}$) is bulk density, and TC (g C g$^{-1}$) is the total C content of the soil.

### 2.5 Data analysis

Nonlinear mixed-effects modeling was applied to analyze the dependencies of the daily mean soil CO$_2$ efflux ($\mu$mol m$^{-2}$ s$^{-1}$) on GWL (m) and WFPS (m$^3$ m$^{-3}$) for each of the CT, FT, and RC plots by fitting the following equations:

$$\text{CO}_2 \text{ efflux} = R_0 \cdot \exp(b \cdot \text{GWL})$$  \hspace{1cm} (4)

$$\text{CO}_2 \text{ efflux} = R_0 \cdot \exp(b \cdot (1 - \text{WFPS}))$$  \hspace{1cm} (5)

where $R_0$ and $b$ are regression coefficients, and chambers are treated as the random coefficients of $R_0$ and $b$. The residual maximum likelihood (REML) estimation method was used for regression analysis, and the goodness-of-fit was evaluated by the coefficient of determination ($R^2$).

The daily mean soil CO$_2$ efflux was gap-filled from the daily mean GWL or WFPS using a regression equation [Eqs. (4) or (5)], and annual cumulative CO$_2$ emissions were summed for each chamber. The differences in the means of the annual cumulative CO$_2$ emissions among years (2015 and 2016) and treatments (CT, FT, and RC plots) were tested by a two-way analysis of variance (ANOVA) and a multiple comparison using the Tukey–Kramer method. The ratios of $R_H$ to $R_S$ were calculated by dividing the annual soil CO$_2$ emissions of RC plot by those of CT and FT plots.

Subsidence through the physical processes of shrinkage/swelling and consolidation...
was determined monthly as the difference between total subsidence and \( S_{RH} \). It was assumed that physical subsidence \( (S_{phys}) \) progressed logarithmically over time due to secondary consolidation and fluctuated with GWL by shrinkage/swelling [Eq. (6)].

In this simple model, C leaching, especially dissolved organic carbon (DOC) efflux through groundwater discharge (Moore et al., 2011), was incorporated into the first term on the right side. However, the regression of cumulative subsidence over time can be spurious, because cumulative subsidence is probably a unit root process. Therefore, a unit root test (augmented Dickey–Fuller test) was performed for \( S_{phys} \). As a result, \( S_{phys} \) was significantly stationary \((P < 0.05)\) so a linear regression was performed using the following equation:

\[
S_{phys} = a \cdot \log_{10}(Days) + b \cdot (GWL_i - GWL_0) \quad \text{(6)}
\]

where the term Days is the number of days from the beginning of subsidence measurement (June 23, 2014), GWL_0 is the daily mean GWL on the initial date (= −0.73 m), GWL_i is the daily mean GWL when subsidence was measured, and \( a \) and \( b \) are regression coefficients. Because soil CO\(_2\) efflux was available only from January 2015, \( S_{RH} \) in 2014 was estimated from the GWL using Eq. (4). Finally, the smoothed annual total subsidence \( (S_{sm}, \text{cm yr}^{-1}) \) was calculated using the following equation:

\[
S_{sm} = a \cdot \log_{10} \left( \frac{\text{Days}_{y+1}}{\text{Days}_y} \right) + b \cdot (\overline{GWL}_{y} - GWL_0) + S_{RH,y} \quad \text{(7)}
\]

where \( y \) is the target year (2015 or 2016), Days_\( y \) is the number of days after January 1 in \( y \) since the beginning of subsidence measurement (June 23, 2014), \( \overline{GWL}_{y} \) is the annual
mean GWL in y, and annual $S_{RH}$ is subsidence through $R_H$ in y.

All data analyses were conducted using R software (R Core Team, 2017).

3. Results

3.1 Environmental properties

The soil pH was $3.9 \pm 1.0$ (mean $\pm 1$ SD) and the soil C content was $52.8 \pm 0.8\%$; such a low pH and high C content are typical properties of ombrotrophic peat. Bulk density was $0.16 \pm 0.04$ Mg m$^{-3}$ at a depth of 0–10 cm and $0.12 \pm 0.02$ Mg m$^{-3}$ at a depth of 0–60 cm (Table S1). The ash content was relatively high at $7.1 \pm 7.9\%$ because of fertilizer applications. Fine root biomass values were $165 \pm 91$, $86 \pm 63$, and $93 \pm 25$ g m$^{-2}$ at a depth of 0–10 cm at 1, 2, and 3 m from the nearest tree, respectively.

Annual precipitation amounts in 2015 and 2016 were similar and close to the mean annual precipitation recorded over a 13-year period (2,915 mm yr$^{-1}$) (Fig. 3a, Table 1). Daily mean GWL varied from $-0.89$ to $-0.23$ m (Fig. S2), with similar annual means in 2015 and 2016 (Fig. 3b, Table 1). The WFPS did not change between 2015 and 2016 (Table 1) and values were similar in the RC and FT plots. No significant difference was found in daily mean soil temperatures between 2015 and 2016 (Table 1).

3.2 Diurnal changes in soil carbon dioxide efflux

Soil temperature at a depth of 5 cm displayed a typical diurnal pattern with a minimum at 7 h and a maximum at 14 h. The diurnal range was about 10°C (Fig. 4a). Soil temperature was higher than air temperature in the nighttime by about 2°C on average (Fig. 4a). The $u^*$ was higher in the daytime than in the nighttime (Fig. 4a). In contrast, soil CO$_2$ efflux was higher in the nighttime than in the daytime in all treatments (Fig. 4b). Its diurnal pattern was a mirror image of those of temperature and $u^*$. 
To examine the effects of temperature, soil water condition, and $u^*$ on diurnal changes in soil CO$_2$ efflux, a multiple regression was performed for hourly soil CO$_2$ efflux with soil temperature, GWL, the difference between air and soil temperature ($\Delta$T$_{\text{air-soil}}$, defined as air temperature minus soil temperature), and $u^*$ as predictors (Table 2). Soil temperature was a significant predictor only in RC plots, while GWL, $\Delta$T$_{\text{air-soil}}$, and $u^*$ were significant predictors in all treatments. From their standardized regression coefficients, $\Delta$T$_{\text{air-soil}}$ was the strongest predictor followed by $u^*$, with no general diurnal change expected in GWL. Hourly soil CO$_2$ efflux was plotted against $\Delta$T$_{\text{air-soil}}$ and $u^*$, respectively (Fig. 5). Soil CO$_2$ efflux had a significant negative relationship with $\Delta$T$_{\text{air-soil}}$ in each treatment when $\Delta$T$_{\text{air-soil}}$ was negative (Fig. 5a). A significant negative relationship was found between soil CO$_2$ efflux and $u^*$ in each treatment when $u^*$ was lower than around 0.4 m s$^{-1}$ (Fig. 5b).

### 3.3 Seasonal changes in soil carbon dioxide efflux

To remove bias due to diurnal changes, the daily mean soil CO$_2$ efflux was calculated only when the number of available data points was larger than six in both the daytime (7–18 h) and nighttime (19–6 h), respectively. The daily mean soil CO$_2$ efflux values during the two years were 2.80 ± 2.18, 1.59 ± 1.18, and 1.94 ± 1.58 µmol m$^{-2}$ s$^{-1}$ (mean ± 1 SD) in the CT, FT, and RC plots, respectively (Fig. 6). Nonlinear mixed-effects models using GWL and WFPS [Eqs. (4) and (5), respectively] were significantly fitted ($P < 0.001$) to daily mean soil CO$_2$ efflux (Fig. 7). It was found that the daily mean soil CO$_2$ efflux increased significantly as the GWL or WFPS decreased. The regression with GWL produced higher $R^2$ values than that with WFPS in the CT and FT plots, while the regression with WFPS produced slightly higher $R^2$ values than the regression with GWL in RC plots (Fig. 7).
3.4 Annual cumulative soil carbon dioxide emission

The daily mean soil CO₂ flux was gap-filled from the GWL using the model [Eq. (4), Fig. 7], and annual sums were calculated (Table 3). Annual cumulative soil CO₂ emissions did not differ between 2015 and 2016 ($F_{1,27} = 1.59, P = 0.22$), but differed significantly among the CT, FT, and RC plots ($F_{2,27} = 4.05, P < 0.05$). The highest soil CO₂ emission was measured in the CT plots ($1.03 \pm 0.53$ kg C m⁻² yr⁻¹), and the lowest was measured in the FT plots ($0.59 \pm 0.26$ kg C m⁻² yr⁻¹). The $R_H/R_S$ ratios were 0.66 and 1.16 for RC/CT and RC/FT, respectively (Table 3).

3.5 Subsidence

The ground surface subsided, but oscillated in correspondence with the GWL (Fig. 8). Total annual subsidence values were determined instantaneously from two measurements in January to be 1.23 and 2.02 cm yr⁻¹ in 2015 and 2016, respectively (Table 4). The annual $S_{RH}$ was calculated from the annual $R_H$, the bulk density, and C content of 60-cm-thick surface peat using Eq. (3). The result shows that the oxidative subsidence values were 1.22 and 0.99 cm yr⁻¹ in 2015 and 2016, respectively (Table 4). As a result, the contributions of oxidative peat decomposition to total subsidence were 100 and 49% in 2015 and 2016, respectively, with a mean of 74%.

Physical subsidence ($S_{phys}$) was significantly fitted with Eq. (6) as $S_{phys} = 1.42 \cdot \log_{10}(\text{Days}) - 6.46 \cdot (\text{GWL}_t + 0.73)$ ($P < 0.01$). The result indicated that the ground subsided physically by 0.65 cm for every GWL lowering of 10 cm. Annual smoothed subsidence ($S_{sm}$) values were 1.83 and 1.27 cm yr⁻¹, respectively, in 2015 and 2016. The $S_{RH}$ accounted for 67 and 78% of the smoothed subsidence in 2015 and 2016, respectively, with a mean of 72% (Table 4).
4. Discussion

4.1 Factors controlling soil carbon dioxide efflux

Soil CO$_2$ efflux displayed a clear diurnal pattern that was almost in reverse parallel with soil temperature (Fig. 4). The hourly soil CO$_2$ efflux had significant negative relationships with GWL, $\Delta T_{\text{air-soil}}$, and $u^*$ (Table 1). First, the effects of $\Delta T_{\text{air-soil}}$ and $u^*$ on the diurnal change in soil CO$_2$ efflux are considered.

Soil temperature was higher than air temperature at night (Fig. 4a), and soil CO$_2$ efflux increased significantly as $\Delta T_{\text{air-soil}}$ decreased when $\Delta T_{\text{air-soil}}$ was negative (Table 2, Fig. 5a). Ganot et al. (2014) found that soil CO$_2$ efflux was promoted by the upward mass flow due to thermal convection in porous mineral soils when the soil temperature was higher than the air temperature. In this study, unsaturated peat soil was more porous than mineral soil. Therefore, our results imply that soil CO$_2$ efflux was promoted by thermal convection in the unsaturated peat profile. Furthermore, the nighttime thermal convection probably decreased soil CO$_2$ concentrations more than diffusion, which potentially suppressed soil CO$_2$ efflux during the following daytime period under stable thermal conditions. On the other hand, Lai et al. (2012) reported that soil CO$_2$ flux was underestimated by the closed chamber method during periods with a high $u^*$ in boreal peatland because wind pumps out the soil air just below the ground surface, which decreases the soil CO$_2$ concentration. The chamber method can measure only the diffusive CO$_2$ efflux in the closed space, but cannot measure the CO$_2$ mass flow due to atmospheric turbulence. In this study, the hourly soil CO$_2$ efflux decreased significantly as $u^*$ increased (Fig. 5b), which may have led to an underestimation of soil CO$_2$ efflux in the daytime when $u^*$ was high on average (Fig. 4a). Therefore, the diurnal change probably resulted from the combination of an increased flux in the nighttime due to
thermal convection, a decreased flux in the daytime due to the aftereffect of nighttime
thermal convection, and an underestimated flux in the daytime due to pumping by
atmospheric turbulence. In the calculation of the daily soil CO\textsubscript{2} efflux, the positive and
negative effects of thermal convection can be compensated for by making continuous
measurements, although some underestimation due to mass flow through pumping is
inevitable in a porous soil when the chamber method is applied, especially in unsaturated
peat soils.

Soil CO\textsubscript{2} flux increases with soil temperature. The diurnal changes in soil temperature
at a depth of 5 cm, with a diurnal range of about 5\degree C (Fig. 4a), could have had a positive
effect on soil CO\textsubscript{2} efflux. However, the effect of soil temperature was not significant in
the CT and FT plots (Table 2). The effect of soil temperature was weaker than that of the
other environmental properties in the RC plots, although it was significant due to the large
sample size (Table 2). Oxidative peat decomposition would have occurred within the 60-
cm deep unsaturated peat horizon because the annual mean GWL was about \(-0.6\) m
(Table 1). Thus, soil CO\textsubscript{2} efflux resulting from the total peat decomposition was not
directly related to soil temperature, which was similar to the oxidative peat decomposition
observed in a burnt ex-peat swamp forest in Central Kalimantan, Indonesia (Hirano et al.,
2014).

The effects of GWL and WFPS on the daily mean soil CO\textsubscript{2} efflux were then considered.
The soil CO\textsubscript{2} flux had a negative exponential relationship with the GWL in all treatments
(Fig. 7), which indicates that soil CO\textsubscript{2} efflux was promoted by lowering of the GWL. A
negative relationship between soil CO\textsubscript{2} efflux and GWL has been reported in various
tropical peatlands (Furukawa et al., 2005; Hirano et al., 2009, 2014; Couwenberg et al.,
2010; Sundari et al., 2012; Ishikura et al., 2017), indicating that peat decomposition is
promoted by lowering of the GWL. Lowering of the GWL decreases WFPS and enhances aeration of the soil. As a result, oxidative mineralization of organic matter and gas diffusivity in the soil is accelerated, resulting in increased soil CO$_2$ efflux (Linn and Doran, 1984). The relationship between soil CO$_2$ efflux and WFPS in the 30-cm-thick surface peat was also significant, but was weaker than the relationship with GWL in the CT and FT plots, while the relationships were similar in the RC plots (Fig. 7). In contrast, Ishikura et al. (2017) suggested that WFPS might be better able to explain the variation in peat soil CO$_2$ efflux than GWL in Central Kalimantan, Indonesia, because disconnection of the capillary force between surface soil water and groundwater occurred under dry conditions. However, at the site used in the current study, such a disconnection probably did not occur (Fig. S3) because GWL was controlled by water gates and remained relatively high. Melling et al. (2013a) found that WFPS was a better predictor of soil CO$_2$ efflux than was GWL over a WFPS range of 0.6–0.9 m$^3$ m$^{-3}$. However, in the current study the range was narrower (0.60–0.75 m$^3$ m$^{-3}$), although the GWLs were similar between this study and that of Melling et al. (2013a). The bulk density in Melling et al. (2013a) was higher (0.21–0.23 Mg m$^{-3}$) than that recorded in this study (Table 4, S1). Therefore, the effect of a capillary rise on WFPS might have been higher in Melling et al. (2013a) than in this study due to the higher bulk density and lower porosity. These are reasons why WFPS was not a better predictor than GWL in this study.

4.2 Annual cumulative carbon dioxide emission

In this study, 57% of the data from continuous CO$_2$ flux measurements during the two years was lost due to power problems and quality controls. To calculate annual cumulative CO$_2$ emissions, the data gaps were filled on a daily basis from GWL using negative exponential equations (Fig. 7). Although gap filling causes uncertainties in the assessment
of annual emissions, these uncertainties are limited because the seasonal variation in
GWL was not large at this study site (Fig. 3b, S2). The annual values are expected to be
more reliable than those reported in previous studies, because previous studies estimated
annual values from data collected at intervals of one month or longer.

Annual soil CO₂ emission was significantly larger from the CT plots than from the RC
plots, and RH accounted for 66% of RS (Table 3). In contrast, the annual soil CO₂ emission
from the FT plots did not differ significantly from that of the RC plots (Table 3). Dariah
et al. (2014) measured soil CO₂ efflux at different distances from tree stems in an oil palm
plantation on tropical peat and reported that root respiration was negligible at distances
of more than 3 m. The distance of each FT plot from the nearest palm tree was greater
than 3 m. Thus, the soil CO₂ efflux in the FT plots was mostly derived from RH, and root
respiration was probably negligible.

The Intergovernmental Panel on Climate Change (IPCC, 2014) provides a default CO₂
emission factor of 1.1 kg C m⁻² yr⁻¹, with 95% confidence intervals of 0.56–1.7 kg C m⁻²
yr⁻¹, from tropical peat in oil palm plantations for their Tier 1 methodology, although this
value was derived from results obtained by the closed chamber and subsidence methods.
The annual RH measured in the RC plots was almost equivalent to the bottom 95%
confidence interval of the Tier 1 method. The annual RS in the CT plots was lower than
the range of 1.22–1.81 kg C m⁻² yr⁻¹ reported in previous studies conducted in oil palm
plantations on peat (Melling et al., 2005, 2013b; Dariah et al., 2014; Sakata et al., 2015).
The annual RH was lower than the previously reported range of 0.69–1.80 kg C m⁻² yr⁻¹
(Melling et al., 2013b; Dariah et al., 2014; Husnain et al., 2014; Marwanto and Agus,
2014). The low RS and RH in this study may have been caused by the higher annual mean
GWL (−1.24 to −0.58 m) than reported in previous studies (Table 1) and by the exclusion
of leaf litter decomposition. In addition, previous studies calculated annual soil CO$_2$
emissions either by linear interpolation of the monthly CO$_2$ flux (Melling et al., 2005,
2013b; Sakata et al., 2015) or by simply averaging periodic CO$_2$ flux measurements for
less than 1 year (Dariah et al., 2014; Husnain et al., 2014; Marwanto and Agus, 2014),
whereas in this study annual CO$_2$ emissions were calculated from the quality controlled
continuous flux, and data gaps were filled using continuous GWL data. The difference in
the calculation methods used would also affect the reported annual soil CO$_2$ emissions.
The contribution of oxidative peat decomposition to total soil respiration calculated as
RC/CT (Table 3) was comparable with the range of 60–86% reported in other oil palm
plantations on tropical peat (Dariah et al., 2014; Comeau et al., 2016), except for 38% in
Melling et al. (2013).

When considering other land uses on tropical peat, the $R_S$ in this study was lower than
the values of 1.23 and 1.35 kg C m$^{-2}$ yr$^{-1}$ reported in swamp forests (Sundari et al., 2012),
1.68–4.20 kg C m$^{-2}$ yr$^{-1}$ reported in an Acacia plantation (Jauhiainen et al., 2012), 3.29
kg C m$^{-2}$ yr$^{-1}$ reported in a rubber plantation (Wakhid et al., 2017), and 1.11–1.60 kg C
m$^{-2}$ yr$^{-1}$ reported in a sago palm plantation (Melling et al., 2005, 2013b). The $R_H$ in this
study was also lower than the ranges of 0.70–0.83 kg C m$^{-2}$ yr$^{-1}$ reported in swamp forests
(Itoh et al., 2017), 1.91–3.78 kg C m$^{-2}$ yr$^{-1}$ reported in an Acacia plantation (Jauhiainen
et al., 2012), and the value of 1.41 kg C m$^{-2}$ yr$^{-1}$ reported in a rubber plantation (Wakhid
et al., 2017), while it was similar to the range of 0.60–0.76 kg C m$^{-2}$ yr$^{-1}$ reported in sago
palm plantations (Melling et al., 2005, 2013b; Watanabe et al., 2009). In Acacia
plantations, GWL tends to be lower than in oil palm plantations (Hergoualc’h and Verchot,
2011), which would enhance oxidative peat decomposition.
4.3 Subsidence

The annual total subsidence that was determined instantaneously was higher in 2016 than in 2015, whereas the annual smoothed subsidence was higher in 2015 (Table 4); the interannual difference was larger for instantaneous subsidence. Instantaneous subsidence was calculated simply from two measurements at annual intervals, and therefore was dependent on peat surface oscillation due to short-term variations in GWL. Therefore, the smaller instantaneous subsidence in 2015 was caused by the higher GWL in January 2016 (Fig. 8). In addition, the interannual order of instantaneous subsidence (2015 < 2016) was inconsistent with that of annual $R_{hi}$ (2015 > 2016) (Table 4). Because such surface oscillation due to short-term GWL variation was excluded in the smoothed subsidence, annual values reflected the interannual variation in GWL (Table 1) and their order of magnitude was consistent with that of the annual $R_{hi}$ (2015 > 2016). However, the means of annual subsidence for the two years were similar in the two approaches.

The annual total subsidence in this study (Table 4) was lower than the range of 2.0–5.4 cm yr$^{-1}$ reported in previous studies of oil palm plantations on peat (Wösten et al., 1997; Hooijer et al., 2012; Couwenberg and Hooijer, 2013), and was also lower than the 5 cm yr$^{-1}$ in an Acacia plantation (Hooijer et al., 2012) and 5.96 cm yr$^{-1}$ in a rubber plantation (Wakhid et al., 2017) on tropical peat. These studies reported a higher oxidative peat decomposition of 0.69–2.13 kg C m$^{-2}$ yr$^{-1}$ than was found in this study, which probably resulted in higher subsidence. Previous studies in tropical peatland also reported a lower bulk density of 0.12–0.14 Mg m$^{-3}$ than was found in this study, except for the value of 0.24 Mg m$^{-3}$ reported by Wakhid et al. (2017). Subsidence increases bulk density, and an increased bulk density decreases subsidence (van Asselen, 2011). Thus, the lower subsidence reported in this study was probably attributable to the higher bulk density due
to peat compaction during land preparation before planting.

Peat oxidation accounted for 72 to 74% of total subsidence on an annual basis (Table 4), which was almost in the middle of the 50–92% range reported in previous studies conducted in tropical peatlands (Murayama and Bakar, 1996; Wösten et al., 1997; Hooijer et al., 2012), except for the value of 25% reported in a rubber plantation (Wakhid et al., 2017).

5. Conclusions

Soil CO\(_2\) efflux through both soil respiration and oxidative peat decomposition were measured continuously for two years in an oil palm plantation established on tropical peat. From the large amount of continuous data, it was found that soil CO\(_2\) efflux was lower in the daytime. The opposite diurnal variation for soil and air temperatures was attributable to the mass flow of soil air due to thermal convection at night and to atmospheric turbulence in the daytime. This indicates that periodic measurements conducted only in the daytime would lead to underestimation of soil CO\(_2\) efflux. In addition, further studies are necessary to determine the reliability of chamber methods on peat, which is one of the most porous soils.

The environmental controls on soil CO\(_2\) efflux using daily means were analyzed to exclude diurnal variation in CO\(_2\) efflux. As a result, exponential negative relationships were found between soil CO\(_2\) efflux and GWL even under a relatively narrow seasonal variation in GWL due to water management. Annual gap-filled CO\(_2\) emissions through soil respiration and oxidative peat decomposition were both lower than those in other oil palm plantations on tropical peat, possibly due to the higher GWL and peat compaction observed in this study compared to previous studies. Thus, water management to raise the
GWL is important to mitigate soil CO$_2$ emissions from oil palm plantations on tropical peat. The differences among studies could also be due to differences in precipitation patterns, land-use history, or other factors among plantations. Therefore, further field studies are necessary to reduce the uncertainties in the emission factor of CO$_2$ from oil palm plantations in Southeast Asia’s tropical peatland.

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Figure legends

Figure 1. Map of the study site

Figure 2. Allocation of chambers, subsidence pole, and groundwater level (GWL) pipe. CT, FT, and RC represent chamber treatments for close-to-tree (< 2.5 m), far-from-tree (> 3 m), and root-cut plots, respectively.

Figure 3. Variations in (a) monthly precipitation and (b) monthly mean GWL. Error bars denote 95% confidence intervals.

Figure 4. Diurnal changes in (a) air and soil temperatures and friction velocity ($u^*$) and (b) soil CO$_2$ flux in the CT, FT, and RC plots. Error bars denote 95% confidence intervals.

Figure 5. Relationship of soil CO$_2$ efflux with the difference between air and soil temperatures ($\Delta T_{\text{air-soil}}$, air minus soil) or friction velocity ($u^*$) in the CT, FT, and RC plots. Efflux data were binned into deciles by $\Delta T_{\text{air-soil}}$ or $u^*$. A linear regression was applied to data at $\Delta T_{\text{air-soil}} < 0^\circ$C and $u^* < 0.4$ m s$^{-1}$. Error bars denote 95% confidence intervals.

Figure 6. Seasonal changes in daily mean soil CO$_2$ efflux in the CT, FT, and RC plots. Circles and lines represent measured and gap-filled values, respectively. Error bars and the gray area denote 95% confidence intervals of measured and estimated soil CO$_2$ efflux among chambers, respectively.

Figure 7. Relationships of daily mean soil CO$_2$ efflux with (a) GWL and (b) water-filled
pore space (WFPS) in the CT, FT, and RC plots.

Figure 8. Cumulative instantaneous total subsidence ($S_{\text{inst}}$, closed circles), cumulative oxidative subsidence ($S_{\text{RH}}$, open circles) and daily mean GWL (gray line). Error bars denote 95% confidence intervals.
Table 1

Annual sum of precipitation, and annual mean groundwater level (GWL), water-filled pore space (WFPS, 0–30 cm depth) and soil temperature (5 cm depth).

<table>
<thead>
<tr>
<th>Variables</th>
<th>Treatment</th>
<th>2015</th>
<th>2016</th>
</tr>
</thead>
<tbody>
<tr>
<td>Precipitation (mm yr(^{-1}))</td>
<td></td>
<td>3000</td>
<td>2910</td>
</tr>
<tr>
<td>GWL (m)</td>
<td>FT</td>
<td>-0.62 ± 0.09</td>
<td>-0.57 ± 0.09</td>
</tr>
<tr>
<td>WFPS (m(^3) m(^{-3}))</td>
<td>FT</td>
<td>0.70 ± 0.03</td>
<td>0.69 ± 0.03</td>
</tr>
<tr>
<td></td>
<td>RC</td>
<td>0.68 ± 0.03</td>
<td>0.68 ± 0.03</td>
</tr>
<tr>
<td>Soil temperature (°C)</td>
<td>FT</td>
<td>26.8 ± 1.5</td>
<td>27.8 ± 2.2</td>
</tr>
</tbody>
</table>

FT: far-from-tree (> 3 m); RC: root-cut
Table 2

Results of a multiple regression analysis for hourly soil CO$_2$ efflux ($\mu$mol m$^{-2}$ s$^{-1}$) with soil temperature (°C), groundwater level (GWL, m), difference between air and soil temperatures ($\Delta T_{\text{air-soil}}$), and friction velocity ($u^*$, m s$^{-1}$). Std. coeff. represents the standardized regression coefficient.

<table>
<thead>
<tr>
<th>Treatment</th>
<th>Predictor</th>
<th>Coefficient</th>
<th>Std. coeff.</th>
<th>P-value</th>
<th>$R^2$</th>
</tr>
</thead>
<tbody>
<tr>
<td>CT</td>
<td>Intercept</td>
<td>2.89</td>
<td></td>
<td>&lt; 0.001</td>
<td>0.128</td>
</tr>
<tr>
<td></td>
<td>(n = 8618) Soil temperature</td>
<td>$-0.03$</td>
<td>$-0.014$</td>
<td>0.18</td>
<td></td>
</tr>
<tr>
<td></td>
<td>GWL</td>
<td>$-10.2$</td>
<td>$-0.296$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td></td>
<td>$\Delta T_{\text{air-soil}}$</td>
<td>$-0.20$</td>
<td>$-0.197$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td></td>
<td>$u^*$</td>
<td>$-0.57$</td>
<td>$-0.032$</td>
<td>&lt; 0.05</td>
<td></td>
</tr>
<tr>
<td>FT</td>
<td>Intercept</td>
<td>$-2.91$</td>
<td></td>
<td>&lt; 0.001</td>
<td>0.107</td>
</tr>
<tr>
<td></td>
<td>(n = 9506) Soil temperature</td>
<td>$0.07$</td>
<td>$0.006$</td>
<td>0.09</td>
<td></td>
</tr>
<tr>
<td></td>
<td>GWL</td>
<td>$-7.37$</td>
<td>$-0.303$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td></td>
<td>$\Delta T_{\text{air-soil}}$</td>
<td>$-0.08$</td>
<td>$-0.109$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td></td>
<td>$u^*$</td>
<td>$-0.65$</td>
<td>$-0.049$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td>RC</td>
<td>Intercept</td>
<td>$-1.80$</td>
<td></td>
<td>&lt; 0.001</td>
<td>0.064</td>
</tr>
<tr>
<td></td>
<td>(n = 17617) Soil temperature</td>
<td>$0.002$</td>
<td>$0.001$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td></td>
<td>GWL</td>
<td>$-6.37$</td>
<td>$-0.205$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td></td>
<td>$\Delta T_{\text{air-soil}}$</td>
<td>$-0.11$</td>
<td>$-0.125$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
<tr>
<td></td>
<td>$u^*$</td>
<td>$-0.92$</td>
<td>$-0.057$</td>
<td>&lt; 0.001</td>
<td></td>
</tr>
</tbody>
</table>

CT: close-to-tree (< 2.5 m); FT: far-from-tree (> 3 m); RC: root-cut
Table 3

Annual cumulative soil CO$_2$ emissions (mean ± 1 standard deviation ($n$)) and the ratio of heterotrophic to total soil respiration ($R_H/R_S$).

Mean values with the same letter are not significantly different ($P > 0.05$).

<table>
<thead>
<tr>
<th>Year</th>
<th>Annual cumulative soil CO$_2$ emission (kg C m$^{-2}$ yr$^{-1}$)</th>
<th>$R_H/R_S$ ratio</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>CT ($R_S$)</td>
<td>FT ($R_S$)</td>
</tr>
<tr>
<td>2015</td>
<td>1.13 ± 0.63 (3)</td>
<td>0.63 ± 0.30 (4)</td>
</tr>
<tr>
<td>2016</td>
<td>0.94 ± 0.53 (3)</td>
<td>0.55 ± 0.25 (5)</td>
</tr>
<tr>
<td>Mean</td>
<td>1.03 ± 0.53 b</td>
<td>0.59 ± 0.26 a</td>
</tr>
</tbody>
</table>

CT: close-to-tree (< 2.5 m); FT: far-from-tree (> 3 m); RC: root-cut
Table 4

Annual subsidence as a result of oxidative peat decomposition ($R_H$) and its contribution to total subsidence. Bulk density and total carbon (C) content of surface peat with 60-cm thickness are shown. The total annual subsidence rate was determined instantaneously from January’s measurements and smoothed using Eq. (7). Values are shown as means ± 1 standard deviation.

<table>
<thead>
<tr>
<th>Year</th>
<th>Annual $R_H$ (kg C m$^{-2}$ yr$^{-1}$)</th>
<th>Bulk density (Mg m$^{-3}$)</th>
<th>Total C content (%)</th>
<th>Subsidence through $R_H$ (cm yr$^{-1}$)</th>
<th>Total subsidence rate (cm yr$^{-1}$)</th>
<th>Contribution of $R_H$ to subsidence (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2015</td>
<td>0.76 ± 0.24</td>
<td>0.12 ± 0.02</td>
<td>52.8 ± 0.8</td>
<td>1.22 ± 0.45</td>
<td>1.23 ± 0.49</td>
<td>100</td>
</tr>
<tr>
<td>2016</td>
<td>0.61 ± 0.16</td>
<td></td>
<td></td>
<td>0.99 ± 0.32</td>
<td>2.02 ± 0.44</td>
<td>49</td>
</tr>
<tr>
<td>Mean</td>
<td>0.69 ± 0.21</td>
<td></td>
<td></td>
<td>1.11 ± 0.39</td>
<td>1.62 ± 0.46</td>
<td>74</td>
</tr>
</tbody>
</table>
Fig. 1

(a) Regional study site

(b) Sibu city, Rajang River, Experimental area

12 km
Fig. 2

- Oil palm
- 8.5 m
- Subsidence pole
- GWL pipe
- CT
- RC
- FT
Fig. 3

(a) Precipitation (mm month$^{-1}$)

(b) GWL (m)
Soil CO$_2$ efflux ($\mu$mol m$^{-2}$ s$^{-1}$)

Local time (hours)

Fig. 4
\[ \text{CO}_2 = 2.34 - 0.46 \times \Delta T_{\text{air-soil}} \]
\[ R^2 = 0.84, P < 0.01 \]

\[ \text{CO}_2 = 1.32 - 0.24 \times \Delta T_{\text{air-soil}} \]
\[ R^2 = 0.89, P < 0.01 \]

\[ \text{CO}_2 = 1.52 - 0.37 \times \Delta T_{\text{air-soil}} \]
\[ R^2 = 0.96, P < 0.001 \]

\[ \text{CO}_2 = 3.49 - 3.89 \times u^* \]
\[ R^2 = 0.90, P < 0.001 \]

\[ \text{CO}_2 = 2.29 - 2.34 \times u^* \]
\[ R^2 = 0.85, P < 0.001 \]

\[ \text{CO}_2 = 2.75 - 3.03 \times u^* \]
\[ R^2 = 0.85, P < 0.001 \]
Fig. 6

Soil CO\textsubscript{2} efflux (µmol m\textsuperscript{-2} s\textsuperscript{-1})
\[ \text{RC} \]
\[ \text{CO}_2 = 0.92 \times \exp(-2.09 \times \text{GWL}) \\
R^2 = 0.18, P < 0.001 \]

\[ \text{RC} \]
\[ \text{CO}_2 = 0.92 \times \exp(-2.09 \times \text{GWL}) \\
R^2 = 0.18, P < 0.001 \]

\[ \text{FT} \]
\[ \text{CO}_2 = 0.46 \times \exp(-2.17 \times \text{GWL}) \\
R^2 = 0.32, P < 0.001 \]

\[ \text{FT} \]
\[ \text{CO}_2 = 0.46 \times \exp(-2.17 \times \text{GWL}) \\
R^2 = 0.32, P < 0.001 \]
**Supplementary materials**

**Table S1**

Profile of soil physicochemical properties. *n* is sample size at each depth.

<table>
<thead>
<tr>
<th>Depth (cm)</th>
<th>Bulk density (Mg m⁻³)</th>
<th>Total C (%)</th>
<th>Total N (%)</th>
<th>C:N ratio</th>
</tr>
</thead>
<tbody>
<tr>
<td>0–10</td>
<td>0.16 ± 0.04</td>
<td>51.5 ± 0.1</td>
<td>2.0 ± 0.00</td>
<td>25.8</td>
</tr>
<tr>
<td>10–20</td>
<td>0.11 ± 0.01</td>
<td>52.6 ± 0.1</td>
<td>1.8 ± 0.01</td>
<td>29.2</td>
</tr>
<tr>
<td>20–30</td>
<td>0.11 ± 0.01</td>
<td>52.6 ± 0.0</td>
<td>1.9 ± 0.01</td>
<td>27.7</td>
</tr>
<tr>
<td>30–40</td>
<td>0.12 ± 0.01</td>
<td>53.0 ± 0.2</td>
<td>1.7 ± 0.01</td>
<td>31.2</td>
</tr>
<tr>
<td>40–50</td>
<td>0.10 ± 0.01</td>
<td>53.2 ± 0.3</td>
<td>1.7 ± 0.04</td>
<td>31.3</td>
</tr>
<tr>
<td>50–60</td>
<td>0.10 ± 0.01</td>
<td>54.0 ± 0.1</td>
<td>1.6 ± 0.00</td>
<td>33.8</td>
</tr>
<tr>
<td>Mean</td>
<td>0.12 ± 0.02</td>
<td>52.8 ± 0.8</td>
<td>1.8 ± 0.13</td>
<td>29.3</td>
</tr>
</tbody>
</table>
Fig. S1
Comparison of soil CO$_2$ flux between LI-COR’s and LGR’s CO$_2$ analyzer

$LGR = 0.084 + 1.017 \times LI-COR$

$R^2 = 0.95, P < 0.001$
Fig. S2
Seasonal change of (a) daily precipitation, (b) daily mean groundwater level (GWL), (c) daily mean soil water content, and (d) daily mean soil temperature. FT and RC in soil water content represent far-from-tree (> 3 m) and root-cut, respectively.
Fig. S3
Relationship between soil water content (SWC) and groundwater level (GWL).

\[
SWC = \frac{0.90 - 0.32}{(1 + (0.087 \times (-100 \times GWL)))^{0.27}} + 0.32
\]

\[R^2 = 0.77, \, P < 0.001\]