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Combustion synthesis of YAG:Ce phosphors via the thermite reaction of aluminum

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Abstract

Cerium-doped yttrium aluminum garnet (YAG:Ce) as a yellow phosphor for white light-emitting diodes (LEDs) was synthesized via a facile combustion method using Y_2O_3 , CeO_2 , Al_2O_3 , Al, and NaClO_4 as raw materials. The combustion synthesis approach utilizes the strong exothermic oxidation of aluminum to realize a self-sustaining reaction. In this study, we investigated the effects of the ratios of Al_2O_3 to Al, fluxes, and coprecipitated materials as raw materials on the luminescence properties of the synthesized YAG:Ce phosphors. When the amount of Al_2O_3 x was varied, the combustion reaction proceeded at $x \leq 1.8$, with $x = 1.725$ being the optimum condition for producing a high-performance product. When 5 mass% BaF_2 was added, the luminescence intensity was significantly improved owing to a decrease of YAP (YAlO_3) formation with improved uniformity. However, the addition of CaF_2 and NaF did not improve the luminescence properties. To suppress the segregation of CeO_2 , we used the coprecipitated material $\text{Y}_2\text{O}_3\text{--CeO}_2$ as a raw material. Unlike with separate addition of Y_2O_3 and CeO_2 , Ce ions were uniformly distributed in the coprecipitated material, resulting in improved luminescence properties. The combination of BaF_2 and coprecipitated material significantly improved the internal quantum efficiency to 83.0%, which is close to that of commercial phosphors.

Keywords: phosphor, yttrium aluminum garnet, combustion synthesis, flux, coprecipitated material

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1. Introduction

Ce-doped $\text{Y}_3\text{Al}_5\text{O}_{12}$ (YAG:Ce) phosphors have been widely used as yellow phosphors for white light-emitting diodes (LEDs) owing to their high emission efficiency under blue light excitation. In conventional solid-state reactions, the synthesis of pure YAG:Ce phosphors requires high-temperature ($> 1500\text{ }^\circ\text{C}$) treatment, which is both energy- and time-consuming. Therefore, lower temperature syntheses, such as spray pyrolysis[1], sol-gel processing[2-4], coprecipitation method[5, 6], citrate sol-gel combustion preparation[7-10], and hydrothermal synthesis[11], have been proposed. However, these processes require the use of nitrates, such as $\text{Al}(\text{NO}_3)_3$ and $\text{Y}(\text{NO}_3)_3$, which still necessitate the use of high temperature treatments. To resolve this problem, this paper proposes a combustion synthesis (self-propagation high-temperature synthesis) of YAG:Ce phosphor using aluminum oxidation heat. Combustion synthesis using the thermite reaction of Al employs the propagation of a strong exothermic reaction, namely, Al oxidation, which is a self-sustaining reaction. This method has advantages of low energy consumption and short reaction times, and has been applied to produce a variety of advanced materials, such as oxides[12-14], nitride/oxynitride ceramics[15-17], and intermetallics[18, 19].

In this study, we examined the facile and effective combustion synthesis of YAG:Ce phosphors via the thermite reaction of Al, where the oxidation heat of Al is used for self-propagation of the high-temperature synthesis. The key for successful combustion synthesis of YAG:Ce phosphors is regulating the reaction temperature, which can be optimized by controlling the ratio of Al and Al_2O_3 in

the raw materials. We also investigated the effects of fluxes and coprecipitated materials on the luminescence properties of the synthesized YAG:Ce phosphors. It is known that flux addition greatly influences ion diffusion and crystallization processes, resulting in improved phase uniformity and luminescence properties [1, 20]. For single crystalline YAG growth, fluxes such as PbO-PbF₂ and PbO-PbF₂-B₂O₃ have been used[21]. Among the various available fluxes, fluoride-type fluxes such as BaF₂, CaF₂, MgF₂, and AlF₃ have been found to be effective for aluminate-type phosphors [20, 22, 23]. However, the effect of these fluxes on combustion-synthesized phosphors is unknown. In addition, we studied the effect of utilizing coprecipitated Y₂O₃-CeO₂ as a raw material. Because Y and Ce ions are uniformly distributed in the coprecipitated material, suppression of CeO₂ segregation and increased uniformity are expected.

2. Material and methods

YAG:Ce phosphors with a Ce ratio of 1.0 at% were prepared from commercially available Y_2O_3 (99.99% purity), CeO_2 (99.99% purity), Al_2O_3 (99.99% purity), Al (99.99% purity), and NaClO_4 (98% purity) powders. Al_2O_3 acts as a diluent to control the combustion flame temperature. The reaction formula for the combustion synthesis can be written as shown in Eq. 1.

Here, x refers to the amount of Al_2O_3 . The adiabatic flame temperature decreases with the increase of x . First, seven sets of raw materials were prepared by balancing the molar ratios with x ranging from 1.5 to 1.9. BaF_2 (99.9% purity), NaF ($\geq 99.9\%$ purity), and CaF_2 (99.9% purity) were used as fluxes, at ratios of 0–7 wt%, 0–5 wt%, and 0–5 wt%, respectively. Y_2O_3 – CeO_2 as a coprecipitated material with a Ce concentration of 5 at% (Nippon Yttrium Co., Ltd.) was also used as raw material.

The raw powders were mixed well in a rolling ball mill at a rate of 100 rpm for 4 h. The mixed raw powders were then placed in graphite crucibles (120 mm $\times$ 40 mm $\times$ 40 mm), which were ignited and combusted in an Ar-filled reactor, as shown in Fig. 1. The main components of the reactor are a stainless steel chamber, a control unit, and a gas control system. Before ignition, the reactor was evacuated using a rotary pump, and Ar gas was supplied to maintain atmospheric pressure. A disposable carbon foil was placed in contact with one

end of the reactant, which was then electrically ignited using a voltage of 50 V and a current of 100 A at room temperature. After ignition, the exhaust valve was opened for 15 min until the product cooled down. The collected products were crushed and washed with distilled water to remove any soluble impurities (mainly NaCl).

The product phases were analyzed using X-ray diffraction (XRD, Miniflex600, Rigaku) with Cu K_{α} radiation ($\lambda = 1.54056$ nm). The photoluminescence properties were recorded using a spectrofluorometer (FP-6200, JASCO) at room temperature with an excitation wavelength of 460 nm. The internal quantum efficiency was quantitatively determined using a fluorescence spectrometer (FP-8500, JASCO) equipped with an integrating sphere (ISF+834, JASCO). For cross-sectional elemental analysis of the particles, the obtained particles of 0.1 g were mixed with 2 g fine copper powder, and then hot pressed for 1 h at 250 °C to form a bulk sample, which was cut, polished, and ion milled using a cross-section polisher (IB-09010CP, JEOL). SEM-EDS (JSM-7001FA, JEOL) was used to confirm the elemental distribution. The valence of Ce ions in the synthesized phosphor was analyzed using XPS (JPS-9200, JEOL).

Fig. 1 Schematic diagram of the experimental apparatus for preparing samples by combustion synthesis.

3. Results and discussion

3.1. Effect of Al_2O_3 ratio in raw materials

In this work, the combustion synthesis of YAG:Ce was promoted by the oxidation of Al by O_2 , which was released from NaClO_4 . The reaction temperature for the oxidation of Al can be in excess of 5300 °C, which can cause melting and extreme sintering of the products. Therefore, we added Al_2O_3 as a diluent, and studied the optimum amount x of Al_2O_3 . Figure 2 shows photographs of samples obtained by combustion synthesis at different x values, as indicated in Eq. 1. The raw materials were in the form of gray powders. The combustion synthesis afforded yellow porous bulk materials with precipitated white powders of NaCl. The raw materials were ignited from one end of the crucible. For samples with $x = 1.5$ – 1.8 , yellow products were obtained throughout the crucible, which indicates that the raw materials were successfully ignited and the combustion reaction was propagated. However, excluding the ignition area, which showed a color change to yellow, the sample at $x = 1.9$ appeared the same as the raw material, indicating that combustion propagation failed owing to an excess amount of Al_2O_3 as a diluent. For samples with $x = 1.5$ – 1.6 , the obtained yellow product seemed to be considerably melted, and a large amount of dark sintered agglomerates was obtained, which might be caused by a very high reaction temperature at higher Al ratios. For samples with $x = 1.75$ – 1.8 , gray powders remained on the surface of the products, especially for samples with higher x values, indicating unreacted materials. In contrast, the products obtained at $x = 1.7$ – 1.725 showed the cleanest yellow color, suggesting the best conditions for producing YAG:Ce.

Fig. 2 Photographs of products after combustion synthesis at different x values.

Figure 3 shows XRD patterns of the products obtained at $x = 1.5$ – 1.9 . For $x = 1.5$ and 1.6 , the dark sintered agglomerates were removed from the XRD samples owing to difficulties in crushing these materials. The white product collected from the wall of the crucible and the product before washing are also shown for comparison. The XRD pattern of the white product was consistent with that of NaCl, which could be removed by washing with water. The main phase of all products was YAG, and a small amount of the YAP (YAlO_3) phase was also detected at $x = 1.5$ – 1.8 . Although the peak intensity of YAP was nearly unchanged at $x = 1.5$ – 1.725 , it gradually increased with x in the range of 1.725 – 1.8 . The Al_2O_3 – Y_2O_3 system has three phases: $\text{Y}_4\text{Al}_2\text{O}_9$ (YAM), YAlO_3 (YAP), and $\text{Y}_3\text{Al}_5\text{O}_{12}$ (YAG). It is assumed that YAG is formed through the following three reactions[24]:

If the heat treatment starts beneath a molar ratio for Al_2O_3 to Y_2O_3 of 5:3, a YAM phase is initially stabilized in the range from 1100°C to 1400°C. Within the temperature range of 1200–1600°C, a YAP phase forms, and YAG is produced over 1300°C. Therefore, a heat treatment of over 1600°C is required to produce a pure YAG phase without YAP formation[25]. YAP is known to form as a byproduct during solid-state reactions under insufficient heat treatment temperature or time[24]. In the case of our study, increased amount of Al_2O_3 (x) decreased the reaction temperature, resulting the increased YAP formation with x in the range of 1.725–1.8.

Fig. 3 XRD patterns of the products after combustion synthesis at different x values. The white product collected from the wall of the crucible and the product before washing with water are also shown for comparison.

Figure 4 shows the luminescence spectra ($\lambda_{\text{ex}} = 460 \text{ nm}$) of the YAG:Ce samples with $x = 1.50\text{--}1.80$. The samples exhibited broad emission peaks in the range of 470–700 nm. This characteristic peak is attributed to the $\text{Ce}^{3+} 5d \rightarrow 4f$ intershell transition[26], and the luminescence spectra are similar to those of YAG:Ce samples in other studies[26, 27]. The emission intensity increased with x in the range of 1.5–1.725, and the intensity was almost constant for $x = 1.7\text{--}1.75$. In particular, the highest emission intensity was measured at $x = 1.725$. However, the emission intensity significantly decreased at $x = 1.8$ because of the

increase of unreacted materials and the decreased heat for crystal growth. The maximum emission peak wavelengths and intensities are shown in the inset of Fig. 4. The peak wavelengths ranged from 527 to 531 nm, with a gradual shift to longer wavelengths for $x = 1.5$ – 1.725 , and a shift to shorter wavelengths for $x = 1.75$ – 1.8 . Generally, luminescence spectra are red-shifted at higher Ce^{3+} concentrations [10, 27]. Therefore, these results indicate that the concentration of Ce^{3+} in the YAG matrix increased for $x = 1.5$ – 1.725 and decreased for $x = 1.75$ – 1.8 . From the above results, it is concluded that $x = 1.725$ – 1.75 is the optimum condition for introducing Ce into the YAG matrix as Ce^{3+} .

Fig. 4 Emission spectra ($\lambda_{\text{ex}} = 460$ nm) for the combustion-synthesized products with different x values. The inset shows the maximum intensity of the luminescence spectra at different x values and the corresponding peak wavelengths.

3.2. Effect of fluxes

To improve the luminescence properties, the addition of flux (BaF_2 , NaF , or CaF_2) at different ratios during combustion synthesis was investigated. The amount of Al_2O_3 (x) was fixed as 1.725 based on the results in section 3.1. Under all experimental conditions, the combustion reaction occurred and final products were obtained without unreacted materials. When the produced materials were observed under ultraviolet light, the sample obtained using BaF_2 showed stronger yellow emission than those obtained with NaF and CaF_2 . Figure 5 shows the XRD pattern of the products synthesized with different amounts of BaF_2 . Each sample consisted mainly of the YAG phase, but small amounts of the YAP phase are also observed. Temperature-time profile for combustion synthesis of YAG:Ce with 5 wt% BaF_2 was recorded, where the combustion temperature exceeded 1400°C . As we discussed above, YAG is produced over 1300°C . However, the reaction time of combustion synthesis is still short. In addition, the temperature distribution also exists into the crucible, in which the temperature at center is relatively high compared to surface. By such reasons, small amount of YAP phase was still present. Further, the amount of residual BaF_2 increased as the amount of BaF_2 added increased. The XRD patterns of the sample obtained using NaF and CaF_2 are obtained, in which the YAG phase and small amounts of the YAP phase are detected. Peaks originating from the fluxes are not observed. The luminescence properties of the sample with added BaF_2 were examined, as shown in Fig. 6. BaF_2 addition increased the luminescence properties, with a maximum emission intensity achieved at 5 wt%, but addition of 6–7 wt% BaF_2 decreased the emission intensity owing to residual BaF_2 after combustion. The

luminescence properties of the NaF and CaF₂ samples were measured, in which similar yellow emission was observed, but these fluxes, especially CaF₂, significantly decreased the luminescence properties compared with those with no added flux. From these results, we conclude that the addition of 5 wt% BaF₂ is the optimum condition for achieving higher luminescence intensity.

Fig. 5 XRD patterns of the products after combustion synthesis with different amounts of BaF₂.

Fig. 6 Emission spectra ($\lambda_{\text{ex}} = 460 \text{ nm}$) for the combustion-synthesized products with different amounts of flux. The inset shows the relationships between amount of BaF_2 and emission intensity at 528 nm.

To investigate the role of BaF_2 flux, the synthesized powders were characterized by SEM and EDS. Figure 7 shows SEM images of the particle surface and the corresponding elemental mappings. The SEM images reveal that the sample with no flux and that with BaF_2 both have smooth surfaces. Elemental mapping from EDS also suggests a uniform distribution of Al and Y, with Ba located at the interface between two particles (Fig. 7(d)). Subsequently, we prepared cross-sectional samples of the particles using mechanical and ion milling. Figure 8 shows compositional images of the cross-sections of the sample with no flux addition and that with 5 wt% BaF_2 . In the sample with no flux (Fig. 8(a)), three phases with different contrasts are observed, namely, a dark gray matrix, light gray areas, and bright dots. In principle, for compositional images

using backscattered electrons, the image contrast depends on the atomic number. Because YAG:Ce is composed of Y (39), Al (13), and Ce (58), the brightness of the constituent elements is predicted to be in the order of $Ce > Y > Al$ in the compositional images. Therefore, the bright dots in Fig. 8(a) correspond to segregated Ce, the light gray areas are a Y-rich phase, and the dark gray matrix is an Al-rich phase. The elemental mapping shown in Fig. 8(b) agrees with this elemental distribution. The Y:Al ratios in YAP and YAG are 1:3 and 3:5, respectively. Therefore, the light gray Y-rich phase is YAP, and the dark gray matrix is YAG. In contrast to no flux addition, the utilization of BaF_2 flux suppressed segregation and the elemental uniformity was improved. Although the YAP phase was still present in the BaF_2 sample, as observed by XRD, the improved elemental uniformity effectively increased the luminescence properties.

Table 1 shows the chemical composition of the samples synthesized with and without BaF_2 , as obtained by analyzing 30 points in the dark gray matrix by SEM-EDS. The chemical composition is consistent with the YAG phase, and there is no difference between the sample with no flux added and that with 5 wt% BaF_2 . However, as shown in Fig. 8(d), in the sample with 5 wt% BaF_2 , segregation of Ba is observed along the interface of particles, which suggests that elemental uniformity is improved by utilizing BaF_2 flux.

Fig. 7 SEM images and elemental mappings of the products synthesized with (a,b) no flux and (c,d) 5 wt% BaF_2 .

Fig. 8 (a,c) Compositional images of the cross-sections of samples without flux

and with 5 wt% BaF₂. (b,d) Corresponding EDS mappings.

Table 1 Composition of YAG:Ce synthesized with and without BaF₂, as measured by SEM-EDS point analysis.

	O (at%)	Al (at%)	Y (at%)	Ce (at%)
No flux	56.38	23.21	20.35	0.042
5 wt% BaF ₂	53.76	24.59	21.58	0.054

A mechanism by BaF₂ doping can affect YAG particle formation is proposed in Fig. 9. After ignition of the carbon foil, the combustion of Al with oxygen from NaClO₄ proceeds, and the temperature rapidly increases (Fig. 9(a)). According to Capper et al., Y₂O₃ and Al₂O₃ can dissolve in molten BaF₂ at high temperature[20]. When the sample temperature exceeds the melting point of BaF₂ (1353 °C), liquid BaF₂ can cover the surfaces of Y₂O₃ and Al₂O₃ (Fig. 9(b)). According to the time profile of the reaction temperature, the combustion temperature does exceed the boiling point of BaF₂. Ohno et al. also reported a decrease of the melting point for mixtures of BaF₂ and Y₂O₃ owing to YF₃ formation[28]. The phase diagram of BaF₂ and YF₃ clearly reveals that the melting point of this mixture is decreased to below 950 °C[29]. Owing to this decreased melting point, it was predicted that the liquid phase of YAG and flux would be stable around 1000 °C, as shown in Fig. 9(c). During the temperature decrease after the combustion reaction, the solid YAG phase precipitates from the

uniform liquid phase (Fig. 9(d)) and grows into large particles (Fig. 9(e)). After solidification is completed, BaF_2 remains at the interface of the grains, as observed in Fig. 7(d) and Fig. 8(d). In summary, the enhanced liquid phase stability that is achieved by utilizing BaF_2 flux effectively increases the elemental uniformity of the final products.

Fig. 9 Proposed mechanism by which BaF_2 doping affects YAG particle formation.

3.3. Effect of coprecipitated material

In addition to BaF_2 flux, we also evaluated the effect of using a coprecipitated material of Y_2O_3 and CeO_2 . Because Y and Ce ions are uniformly distributed on the atomic scale in the coprecipitated material, segregation is expected to be suppressed. Figure 10 shows the XRD pattern of the powder synthesized using the coprecipitated material, in which the YAP phase is still generated. Figure 11 shows the emission spectrum and a photograph of the product. The sample with the coprecipitated material showed improved emission intensity of approximately 8.4% compared with the sample with only BaF_2 added. The internal quantum efficiency (IQE) of the samples was also analyzed, as shown in Table 2. Similar to the change in emission intensity shown in Fig. 11, the IQE increased from 54.9% for the sample with no flux to 83.0% for the sample with flux and the coprecipitated material.

Fig. 10 XRD patterns of the products after combustion synthesis under different conditions: no flux, 5 wt% BaF_2 , and $\text{Y}_2\text{O}_3\text{-CeO}_2 + 5$ wt% BaF_2 .

Fig. 11 Emission spectra ($\lambda_{\text{ex}} = 460 \text{ nm}$) for the combustion-synthesized products under different conditions: no flux, 5 wt% BaF_2 , and $\text{Y}_2\text{O}_3\text{--CeO}_2 + 5 \text{ wt\% BaF}_2$. The inset shows a photograph of the synthesized powders under near-ultraviolet light.

Table 2 Internal quantum efficiency (IQE) of products synthesized under different conditions.

Sample	IQE (%)
$\text{Y}_2\text{O}_3\text{--CeO}_2 + 5 \text{ wt\% BaF}_2$	83.0
5 wt% BaF_2	73.2
No flux	54.9

Figure 12 shows compositional images and corresponding EDS mappings of the cross-sections of the products synthesized with 5 wt% BaF₂ and Y₂O₃–CeO₂ + 5 wt% BaF₂. The distribution of Al and Y appears uniform in both samples, but segregation of Ce was only observed in the BaF₂ sample. For smaller particles synthesized using Y₂O₃–CeO₂ + 5 wt% BaF₂, segregation of Ce disappeared. However, the larger particles still included segregated Ce. We also investigated the valence of Ce in the various samples using XPS. In the YAG structure, Ce is doped as Ce³⁺ ions. In contrast, segregated CeO₂ contains Ce⁴⁺ ions. The ratio of Ce³⁺ and Ce⁴⁺ ions was determined from the shift in the binding energies in the Ce 3d XPS spectra (Fig. 13), in which four peaks (Ce⁴⁺ 3d_{5/2}, Ce⁴⁺ 3d_{3/2}, Ce³⁺ 3d_{5/2}, and Ce³⁺ 3d_{3/2}) were separated using peak fitting[2, 30, 31]. From the peak fitting results, the peak positions, half-widths, and areas were determined, and the Ce³⁺/Ce⁴⁺ ratios were calculated, as shown in Tables 3 and 4. Compared with the BaF₂ sample, the Ce³⁺ ratio in the sample obtained using the coprecipitated material was 1.36% higher. These results indicate that the utilization of the coprecipitated material improves the luminescence properties by improving the uniformity of the sample. Because of the short reaction time during combustion synthesis, diffusion of each element might be insufficient, which causes segregation of Ce.

Fig. 12 Compositional images and corresponding EDS mappings of the cross-sections of the products synthesized using 5 wt% BaF₂ and Y₂O₃-CeO₂ + 5 wt% BaF₂.

Fig. 13 Ce 3d XPS spectra of YAG:Ce powders synthesized with (a) 5 wt% BaF₂ and (b) Y₂O₃-CeO₂ + 5 wt% BaF₂.

Table 3 XPS results and ratio of Ce^{3+} and Ce^{4+} in YAG:Ce synthesized with 5 wt% BaF_2 .

	$\text{Ce}^{4+} 3d_{5/2}$	$\text{Ce}^{4+} 3d_{3/2}$	$\text{Ce}^{3+} 3d_{5/2}$	$\text{Ce}^{3+} 3d_{3/2}$
Peak (eV)	883	901	887	905
Half-width	1.5	2.1	2.4	3.8
Area	499	612	1660	1471
Sum	1111		3131	
Ratio (%)	26.2		73.8	

Table 4 XPS results and ratio of Ce^{3+} and Ce^{4+} in YAG:Ce synthesized with $\text{Y}_2\text{O}_3\text{--CeO}_2 + 5 \text{ wt\% BaF}_2$.

	$\text{Ce}^{4+} 3d_{5/2}$	$\text{Ce}^{4+} 3d_{3/2}$	$\text{Ce}^{3+} 3d_{5/2}$	$\text{Ce}^{3+} 3d_{3/2}$
Peak (eV)	883	901	887	905
Half-width	1.5	2.3	2.5	3.7
Area	575	707	2029	1852
Sum	1281		3881	
Ratio (%)	24.8		75.2	

3.4. Equilibrium theory for phosphor synthesis

In the above sections, we reported the luminescence properties, particle morphologies, and elemental distributions of the combustion-synthesized products. In this section, we use equilibrium theory to discuss why YAG:Ce phosphors can be synthesized in a shorter time by combustion synthesis than by solid-state reaction.

First, focusing on the synthesis of the YAG matrix, the reaction formulas of the two methods can be expressed by Eq. 5 (combustion synthesis) and Eq. 6 (solid-state reaction).

Figure 14(a) shows the temperature dependence of the standard free energy (ΔG^0 , calculated using HSC Chemistry version 8.0) for Eq. 5 and Eq. 6. The ΔG^0 value for Eq. 5 is considerably lower than that for Eq. 6, indicating that Eq. 5 has a higher driving force and can progress more easily than the reaction in Eq. 6. Second, we examined the reduction of CeO_2 to Ce_2O_3 . It is important to reduce Ce^{4+} to Ce^{3+} for the formation of YAG:Ce phosphors with Ce doped in the Y site. In solid-state reactions, a reduction atmosphere is always needed, and the following reactions can be considered:

In combustion synthesis, a different reduction reaction can be considered:

Fig. 14 (a) Temperature dependence of the standard free energy (ΔG^0) for the synthesis of YAG by combustion (Eq. 5) and solid-state reaction (Eq. 6). (b) Temperature dependence of ΔG^0 for the reduction of CeO_2 to Ce_2O_3 by CO (Eq. 7), H_2 (Eq. 8), and Al (Eq. 9).

The ΔG^0 values of these reactions as a function of temperature are shown in Fig. 14(b). To obtain a negative ΔG^0 value, a temperature higher than 1530 °C is required for Eq. 7, whereas a temperature higher than 1290 °C is required for Eq. 8, which correspond to the lowest temperatures for the reduction of Ce^{4+} to Ce^{3+} . However, interestingly, for Eq. 9, negative ΔG^0 values are obtained over a wide temperature range, including room temperature, which indicates that combustion synthesis not only forms the YAG matrix, but also easily introduces Ce^{3+} as a dopant into the YAG matrix. For these reasons, YAG:Ce phosphors were successfully synthesized by combustion synthesis, which has obvious advantages, such as low energy consumption and short reaction times.

4. Conclusion

YAG:Ce phosphors were successfully prepared by combustion synthesis via the thermite reaction of Al. The reaction temperature was controlled by varying x , the ratio of Al_2O_3 to Al. The combustion reaction proceeded at $x \leq 1.8$, and $x = 1.725$ was the optimum condition for producing a high-performance product. When 5 wt% BaF_2 was added, the luminescence intensity was significantly improved owing to decreased YAP formation with improved elemental uniformity through the effect of the flux on the liquid phase. We also evaluated the effect of a coprecipitated material of Y_2O_3 and CeO_2 . The combination of BaF_2 and the coprecipitated material significantly improved the IQE to 83.0%, which is close to that of commercial phosphors. Equilibrium theory indicates that combustion synthesis not only forms the YAG matrix, but also introduces Ce^{3+} into the YAG matrix more easily than in a solid-state reaction. These results demonstrate the potential of this facile combustion synthesis method for synthesizing high-performance phosphors via the thermite reaction of Al in a short time by utilizing flux and coprecipitated raw materials.

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Graphical abstract

Schematic diagram of the experimental apparatus for combustion synthesis and Emission spectra for the combustion-synthesized products under different conditions: no flux, 5 wt% BaF_2 , and $\text{Y}_2\text{O}_3\text{-CeO}_2 + 5 \text{ wt\% BaF}_2$. The inset shows a photograph of the synthesized powders.