



Title	Improvement of hybrid jig separation efficiency using wetting agents for the recycling of mixed-plastic wastes
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1 ORIGINALARTICLE

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3 Improvement of hybrid jig separation efficiency using wetting agents for the recycling of  
4 mixed-plastic wastes

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14  
15 **Abstract**

16  
17 We have developed the hybrid jig which combines the principles of jig separation and flotation. However,  
18 the selectivity of bubble attachment in water was poor because most plastic have inherently hydrophobic  
19 surfaces, so development of surface modification techniques for plastic particles would expand its  
20 application to the material recycling of plastics.

21 In this study, the hybrid jig separation of the polypropylene with glass fiber (PPGF) and high  
22 impact polystyrene (HIPS) having similar SG and surface wettability were investigated with three wetting  
23 agents (Di-2-ethylhexyl sodium sulfosuccinate (Aerosol OT, AOT), sodium lignin sulfonate (NaLS), and  
24 tannic acid (TA)). The results showed that the probability of bubble attachment was influenced by wetting  
25 agents because of their strong effects on the surface tension of solution and surface wettability of plastics.  
26 These results suggest that wetting agents could be utilized to control the selectivity of bubble attachment  
27 and improve the hybrid jig separation efficiency. In addition, since the hybrid jig separation of polyvinyl  
28 chloride (PVC) and polyamide, nylon-66 (PA) using AOT was imperfect, a two-step approach, composed  
29 of a pre-wetting step (first step) in a solution containing the wetting agent (AOT) and hybrid jig  
30 separation in water (second step), was proposed.

31  
32 **Keywords:** Recycling, jig, hybrid jig, plastic, wetting agent

## 34 **Introduction**

35 The total global production of plastics has grown from around 1.5 million tons in 1950 to 348 million  
36 tons in 2017 and worldwide consumption has been increasing annually at a rate of 5% with the largest  
37 increase reported in Asia [1, 2]. There are two common ways to recycle plastics: (i) material recycling  
38 whereby plastic wastes are recovered for the production of new plastics, and (ii) thermal recycling  
39 whereby plastic wastes are used as fuel for power generation. Between the two, material recycling is more  
40 sustainable and profitable but requires exceptionally efficient separation of different types of plastics from  
41 mixed-plastic wastes to obtain products with very high purities (>99.9%). Achieving this very high plastic  
42 purity in recycling is very difficult, so mixed-plastic wastes are more commonly used in thermal recycling.  
43 In recent years, however, several studies have utilized mineral processing techniques to separate  
44 mixed-plastic wastes into their individual components to facilitate material recycling (e.g., gravity  
45 separation [3-10], dense medium separation [11-13], electrical separation [14-16], flotation [12, 17-28]).

46 Flotation is one of the common mineral processing techniques for fine fraction (minerals: -75  
47  $\mu\text{m}$ ; coal: -150  $\mu\text{m}$ ) since normally, fine grinding is required ( $\mu\text{m}$ ) for ores to achieve sufficient liberation  
48 of target minerals [9, 29]. Most of minerals have hydrophilic surface so, a collector (e.g., xanthate,  
49 aerofloats [30]) is usually added to selectively change the surface wettability to enhance the separation  
50 efficiency. In contrast, plastic flotation is usually carried out with wetting agents (e.g., AOT [22], NaLS  
51 [22], CaLS [12, 22-24], TA [22, 25, 26], PVA [22, 26-28]) since most plastic have inherently hydrophobic  
52 surfaces. However, for resources recycling, especially plastics, sufficient liberation is already achieved in

53 even at coarser particle sizes (mm to cm) [30-32]. Moreover, additional size reduction (i.e., crushing and  
54 grinding) required for flotation that incurs higher costs and energy is needed [30].

55 One potentially effective technique for the separation of coarser size of plastics from  
56 mixed-plastic wastes is the use of jigs. Jigs can separate the particles at coarse size fractions (+0.5 mm)  
57 and jig is a gravity concentrator that separate the particles based on differences in their densities or  
58 specific gravities (SG) [7, 30, 33]. Among the various types of jigs, the TACUB (Takakuwa air chamber  
59 under bed) jig, commercially marketed as BATAAC jig, is a popular and commonly used type of jig  
60 especially in coal cleaning because of its more uniform pressure distribution inside the separation  
61 chamber that provides higher separation efficiency. This uniform pressure distribution is facilitated by a  
62 series of pneumatically operated multiple air chambers, usually two cells under the separation chamber,  
63 that extend to its full width. Pressurized air is injected into the air chambers, causing water within the  
64 separation chamber to pulsate and induce stratification [3, 6, 30].

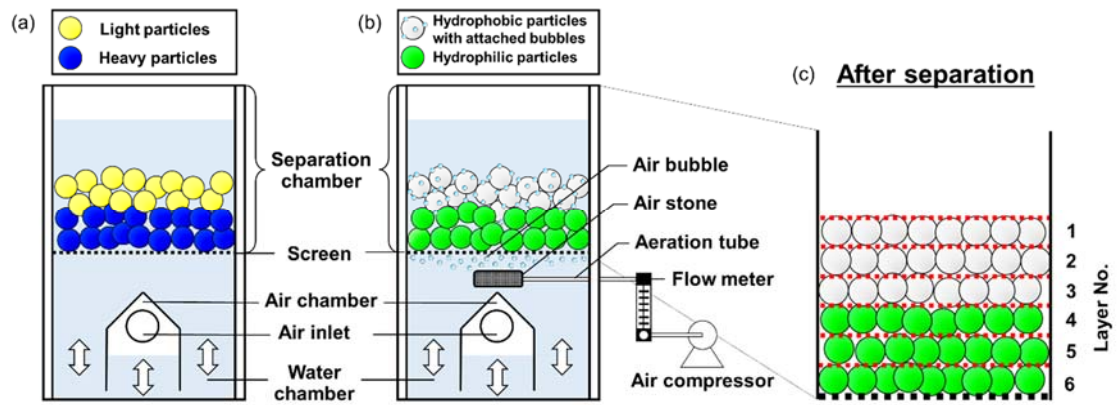
65 The TACUB jig was, however, ineffective for mixed-plastic wastes because SG differences of  
66 the various types of plastics in mixed-plastic wastes are very small. To address this problem, Tsunekawa  
67 et al. [3] developed the RETAC jig (R&E, Co., Ltd., Japan), an improved version of the TACUB jig, that  
68 facilitates plastic-plastic separation via precision control of the wave form during jig separation (Fig. 1(a))  
69 [3, 4]. The RETAC jig, for example, successfully separated polystyrene (PS), acrylonitrile butadiene  
70 styrene (ABS), and polyethylene terephthalate (PET) from crushed copy machines [3]. Although  
71 effective, separation efficiency of the RETAC jig dramatically decreases when the density difference of

72 plastics to be separated becomes small. Unfortunately, many types of plastics developed in recent years  
73 for identical applications have very similar SG. For example, two types of plastics used in the  
74 manufacture of large home appliances, polypropylene with glass fiber (PPGF) and high impact  
75 polystyrene (HIPS), both have SG equal to 1.04. In theory, separation of materials with similar SG is  
76 impossible using gravity separation techniques like jigs.

77 A new type of jig called the hybrid jig was developed to address this limitation. The hybrid jig  
78 works by combining the principles of gravity separation and flotation and could separate materials with  
79 similar SG so long as their surface wettability properties are different (Fig. 1(b)) [5]. Separation occurs  
80 due to the attachment of bubbles to more hydrophobic plastic particles that make them lighter than the  
81 less hydrophobic plastic particles that causes stratification during water pulsation.

82 In a previous study of the authors, hybrid jig separation of pure plastic mixtures (i.e.,  
83 polyethylene (PE), polyethylene terephthalate (PET), polyvinyl chloride (PVC)) in water was carried out  
84 and good separation efficiency was reported [5]. However, the selectivity of bubble attachment in water  
85 for other plastics was poor because most plastic have inherently hydrophobic surfaces, so development of  
86 surface modification techniques for plastic particles would expand its application to the material recycling  
87 of plastics. This means that surface modification of plastics is required for the improvement of  
88 mixed-plastic waste separation using the hybrid jig, so in this study, the effects of wetting agents on  
89 bubble attachment probability and hybrid jig separation efficiency were investigated. In addition, a  
90 two-step approach to improve hybrid jig separation efficiency using wetting agents is proposed.

91



92

93 **Fig. 1** Schematic illustrations of (a) RETAC jig, (b) Hybrid jig, and (c) how the products were partitioned

94 into 6 layers after separation.

95

96 **Materials**

97

98 **Samples**

99 Polypropylene with glass fiber (PPGF) and high impact polystyrene (HIPS) obtained from a recycling  
100 facility of home appliances in Japan, and virgin plastic boards of polyvinyl chloride (PVC) and polyamide,  
101 Nylon-66 (PA) were used in this study and the SG of these samples are listed in Table 1. The virgin  
102 plastic boards were crushed by an orient mill (VH16, Seishin Enterprise Co. Ltd, Japan) and screened to  
103 obtain suitable size fractions for the hybrid jig separation experiments.

104

105 Table 1. Plastic samples and their specific gravities (SG).

Samples	Abbreviation	Specific gravity
Polypropylene with glass fiber	PPGF	1.04
High impact polystyrene	HIPS	
Polyvinyl chloride	PVC	1.38
Polyamide, Nylon-66	PA	1.37

106

107

108 **Reagents**

109 Methyl isobutyl carbinol (MIBC, Wako Pure Chemical Industries Ltd., Japan), a reagent widely utilized  
110 in flotation to stabilize bubble formation in solution, was used in the hybrid jig separation experiments.  
111 Three types of wetting agents were evaluated in this study: (1) Di-2-ethylhexyl sodium sulfosuccinate  
112 (Aerosol OT, AOT, Wako Pure Chemical Industries Ltd., Japan), (2) sodium lignin sulfonate (NaLS,  
113 Tokyo Chemical Industry Co. Ltd., Japan), and (3) tannic acid (TA, Wako Pure Chemical Industries, Ltd.,  
114 Japan).



115 **Experimental methods**

116

117 **Surface tension and contact angle measurements**

118 Surface tension of solutions containing each of the wetting agents was measured using a

119 temperature-controlled reaction vessel connected to a tensiometer (Krüss K100, Krüss GmbH, Germany).

120 For the contact angle measurements, an air bubble generated from a syringe needle was introduced

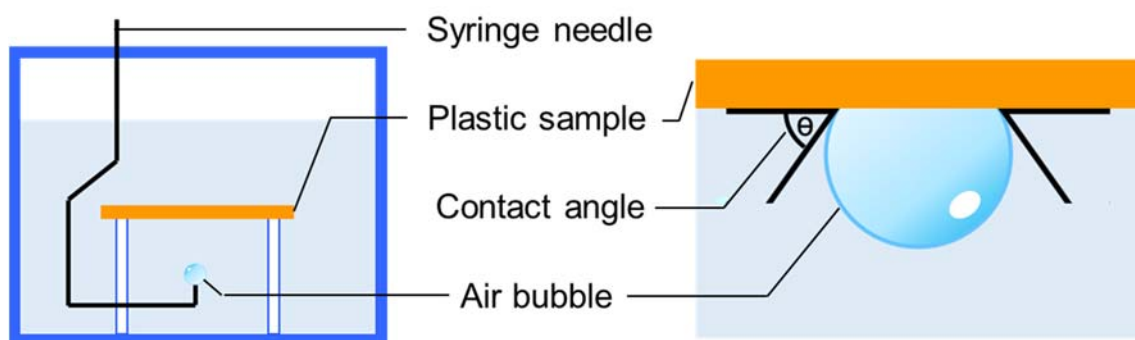
121 underneath the plastic sample submerged in solutions containing each of the wetting agents and the

122 contact angle (angles between particle surface (solid-liquid interface) and bubble surface (gas-liquid

123 interface)) (Fig. 2) was measured using a high-resolution digital microscope with image analysis

124 capability (VHX-1000, Keyence Corporation, Japan).

125



126

127

128 **Fig. 2** Schematic diagrams of the contact angle measurement

129

130 **Adsorption and desorption experiments**

131 To obtain adsorption isotherm of AOT on PA [34], the adsorption experiments of AOT on PA were carried  
132 out. The particles of PA (25 g) were stirred (400 rpm) in to AOT solution (30, 50, 80, 100, 150, 180, 200,  
133 and 250 ppm) for 10 min then, left for 120 min. The dissolved sulfur concentration of remaining solution  
134 was measured by inductively coupled plasma atomic emission spectroscopy (ICP-AES, ICPE-9820,  
135 Shimadzu Corporation, Japan) (margin of error =  $\pm 2\%$ ).

136 For desorption experiments, PA particles were put in 10 ppm AOT solution for 3 min and then,  
137 washed by water. The particles were then put in another beaker filled with water and the dissolved sulfur  
138 concentration of solution was measured by ICP-AES after 30, 60, 90, and 120 min to calculate the  
139 desorption amount of AOT from PA.

140

141 **Hybrid jig separation experiments**

142 Fig. 1(b) shows a schematic diagram of the desktop hybrid jig separation apparatus used in this study.

143 This device is a modified desktop RETAC jig that has additional aeration tubes fitted with air stones  
144 installed under the separation chamber (145 mm long, 155 mm wide and 320 mm high) to generate air  
145 bubbles. The hybrid jig separation experiments were done by putting plastic samples and a solution (20 L)  
146 containing water, MIBC, and one of the wetting agents into the separation chamber (Table 2). Air bubbles  
147 were introduced underneath the screen simultaneously as water pulsation begun (Fig. 1(b)). Table 2  
148 summarizes the conditions of hybrid jig separation experiments conducted in this study. The water

149 pulsation was decided based on the research of Hori et. al., 2009 [4]. After each run, the products were  
 150 divided from the top into six layers (Fig. 1(c)) and then collected using a vacuum sampling system.  
 151 Different plastics in each layer were separated by hand-picking to measure the purity of products.

152

153 Table 2. Conditions of the hybrid jig separation tests.

	Experiment 1	Experiment 2
	HIPS/PPGF	PVC/PA
Weight of sample [g]	250	
Particle size [mm]	+3.0 - 8.0	
Displacement [mm]	10	
Frequency of water pulsation [cycle/min]	30	
Separation time [min]	3	
Air rates [L/min]	1.5	
Concentration of stabilize bubble formation reagent [ppm or mg/L]	20	
Concentration of wetting agent [ppm or mg/L]	350 (NaLS, TA)	10 (AOT)

154

155

156 **Results and discussion**

157

158 **Separation of PPGF and HIPS using bubble attachment probability**

159 PPGF is typically used for drum-type washing machines while HIPS is a common type of plastic used in  
160 the manufacture of many home appliances because of its durability. Although the SG of PP is less than 1.0,  
161 addition of glass-fiber to create the stronger PPGF increased its SG to 1.04, which is equal to that of HIPS.  
162 Because both of these types of plastics are common components of large home appliances, they are mixed  
163 during recycling and should be separated to improve material recycling efficiency.

164 Preliminary experiments to separate PPGF and HIPS using the hybrid jig without any wetting  
165 agent showed that separation was impossible because of the indiscriminate attachment of bubbles on both  
166 types of plastics. Fig. 3(a) shows the hybrid jig experimental results for the PPGF-HIPS mixture (3.0 to  
167 8.0 mm) in solutions containing 350 ppm of AOT, NaLS or TA. Purity in the top (1<sup>st</sup>) and bottom (6<sup>th</sup>)  
168 layers (Fig. 1(c)) with AOT (Fig. 3(a-1)) was lower than those with NaLS (Fig. 3(a-2)) and TA (Fig.  
169 3(a-3)). With NaLS, the PPGF purity in the top layer and the HIPS purity in the bottom layer were 97%  
170 and 99%, respectively and with TA, the PPGF purity in the top layer and the HIPS purity in the bottom  
171 layer were 99% and 86%, respectively. These results suggest that separation of both plastics is possible,  
172 and the type of wetting agent and their concentrations are important parameters to improve the hybrid jig  
173 separation efficiency.

174 The effects of a wetting agent on particle-bubble interactions depend on tensile forces acting on

175 the particle that lead to the development of an angle between the particle surface and the bubble surface  
176 [30]. At equilibrium

$$177 \quad \gamma_{s/a} = \gamma_{s/w} + \gamma_{w/a} \cos \theta \quad (1)$$

178 where  $\gamma_{s/a}$ ,  $\gamma_{s/w}$ , and  $\gamma_{w/a}$  are the surface energies between solid and air, solid and water, and water and air,  
179 respectively, and  $\theta$  is the contact angle (angles between particle surface (solid-liquid interface) and bubble  
180 surface (gas-liquid interface)) (Fig. 1). The attachment of bubbles on the surface of particles is strongly  
181 dependent on the work of adhesion ( $W_{s/a}$ ), which is defined as the force required to break the  
182 particle-bubble interface and is equal to the work needed to separate the solid-air interface and produce  
183 separate solid-air, air-water and solid-water interfaces (Eq. 2) [30].

$$184 \quad W_{s/a} = \gamma_{w/a} (1 - \cos \theta) \quad (2)$$

185 The work of adhesion is further influenced by the surface wettability of the particle, determined  
186 by the contact angle ( $\theta$ ), and the surface tension of solution. More hydrophobic (i.e., larger contact angle)  
187 particles have larger work of adhesion when in contact with bubbles. Similarly, solutions with higher  
188 surface tension ( $\gamma_{w/a}$ ) increase the work of adhesion between particle and bubble. Both the surface tension  
189 and surface wettability of particles could be changed by adding surface acting agents called surfactants  
190 [30], so measurements of the contact angles of PPGF and HIPS as well as the surface tension of solutions  
191 containing each of the wetting agents were carried out.

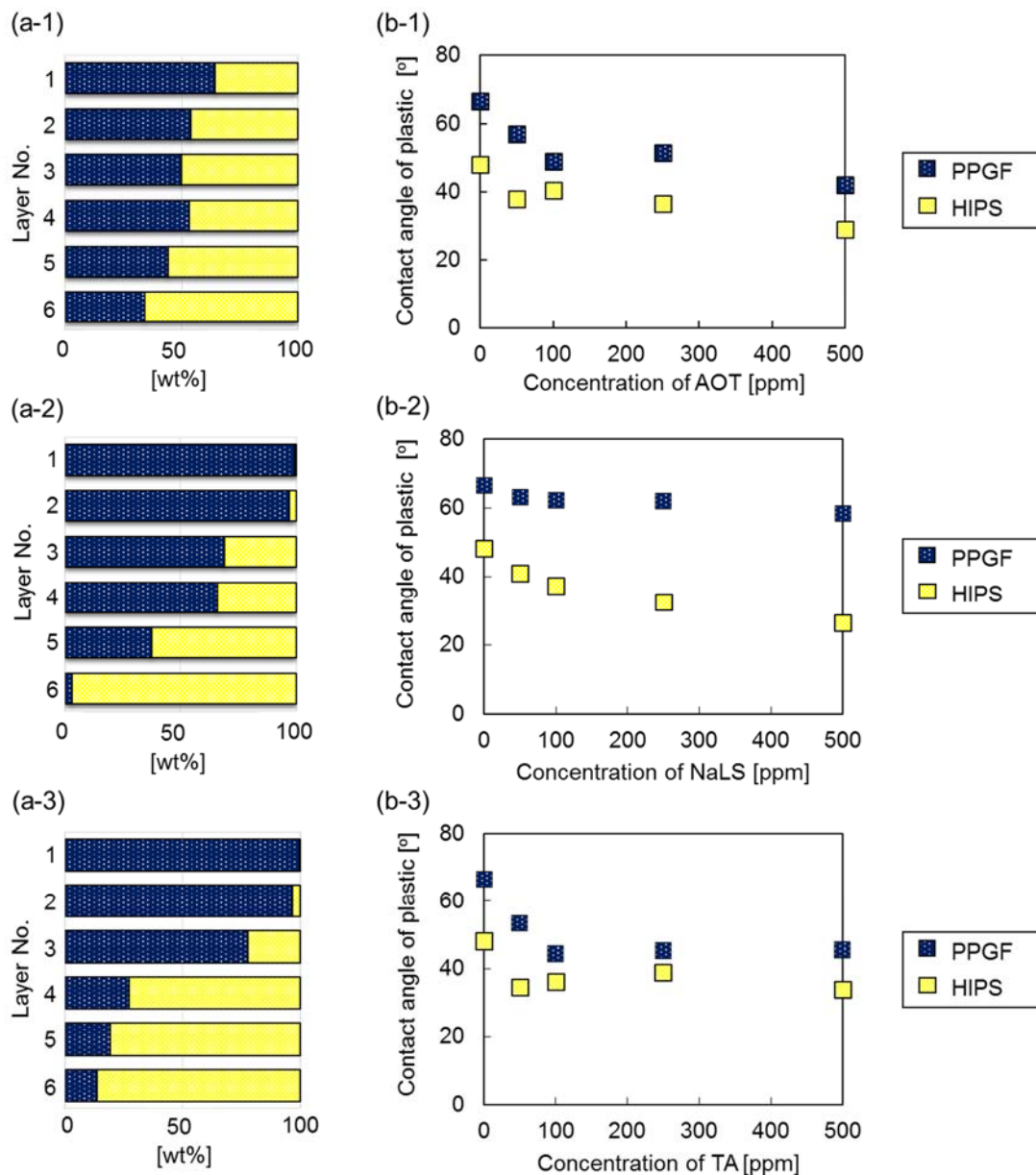
192 Figs. 3(b) and 4 show the contact angles of PPGF and HIPS as well as the surface tension of  
193 solutions containing the wetting agents (i.e., AOT, NaLS or TA). The results showed that PPGF is more

194 hydrophobic than HIPS regardless of the type and concentration of wetting agent (Fig. 3(b)).

195           Among the three wetting agents, only AOT lowered the surface tension of solution while the  
196 effects of NaLS or TA on it were negligible (Fig. 4). The lower surface tension of solution in the presence  
197 of AOT decreased the work of adhesion, resulting in fewer bubble attachments on the particle surface. In  
198 comparison, NaLS or TA had negligible effects on the surface tension but decreased the contact angle at  
199 higher concentrations (Fig. 4). These results suggest that the work of adhesion and bubble attachment  
200 probability decreased in the presence of either NaLS or TA likely because of the adsorption of these two  
201 wetting agents onto the surface of plastic particles that made them more hydrophilic. Similarly, the  
202 contact angles on both plastics decreased in the presence of AOT (Fig. 3(b-1)) but because this wetting  
203 agent also lowered the surface tension of solution (Fig. 4), the net effect was the limited bubble  
204 attachment that resulted in low separation efficiency even though both PPGF and HDPS became more  
205 hydrophilic (Fig. 3(a-1)). In the case of NaLS, the change in contact angle of HIPS was more dramatic  
206 than that of PPGF, which caused selective bubble attachment onto PPGF making it lighter than HIPS that  
207 facilitated better stratification during hybrid jig separation (Figs. 3(a-2) and 3(b-2)). In the case of TA, the  
208 contact angle of PPGF decreased with increasing TA concentration (Fig. 3(b-3)). However, the contact  
209 angle with TA was slightly higher than that with AOT, which likely caused selective bubble attachment on  
210 the PPGF surface. These results show that the control of surface characteristics by wetting agents could  
211 improve the separation efficiency of the hybrid jig. In the TA solution, similar results were obtained  
212 compared with that in NaLS even though the contact angles of HIPS and PPGF were similar. This

213 phenomenon remains unclear because of the difficulty in quantifying the amounts of bubbles attached on  
214 plastic particles. Many previous papers reported the interaction between air bubbles and plastic particles  
215 during flotation [35, 36] however, the particle and water movement during hybrid jig separation and  
216 flotation are different. This means that a reliable measurement technique to quantify bubble attachment  
217 volume during hybrid jig separation (with water pulsation) should be developed.

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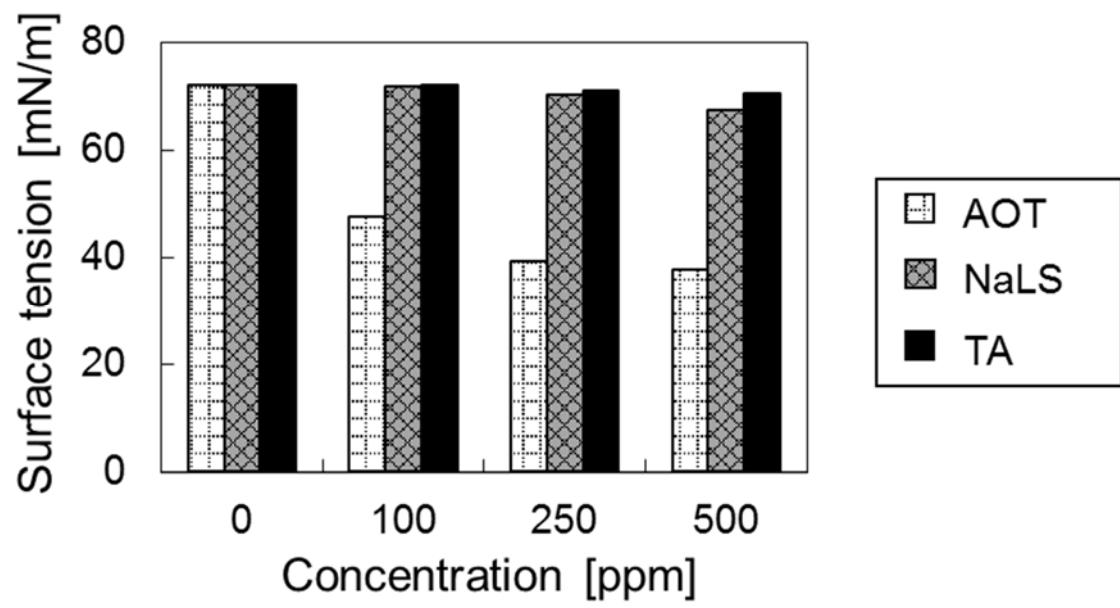
220 **Fig. 3** (a) The proportion of PPGF and HIPS in each layer after hybrid jig separation tests with (a-1) AOT

221 (350 ppm), (a-2) NaLS (350 ppm), and (a-3) TA (350 ppm) as wetting agents, and (b) contact angles of

222 PPGF and HIPS in (b-1) AOT, (b-2) NaLS, and (b-3) TA solutions

223





224

225 **Fig. 4** Surface tension of solutions containing each of the wetting agents at various concentrations

226

## 227 **Separation of PVC and PA using a two-step approach**

228 PVC is a common type of plastic used for a variety of applications such as in building and construction,  
229 packaging, electrical and electronics, and automobile while PA (or nylon) is an engineering plastic used in  
230 clothing, electrical and electronic, and automobile [1]. These types of plastics can be found together in  
231 waste electrical and electronic equipment (WEEE) and automotive shredder residue (ASR) from end of  
232 life vehicle (ELV) and due to their similar SG (1.38 and 1.37), in this study hybrid jig was applied to  
233 separate them into individual components to improve material recycling efficiency.

234 The results from the previous section showed that wettability control by selective bubble  
235 attachment with the aid of wetting agents could improve the hybrid jig separation efficiency. In this  
236 section, separation of PVC and PA using a two-step approach was investigated. Hybrid jig tests of PVC  
237 (SG = 1.38) and PA (SG = 1.37) were carried out in water containing 10 ppm of AOT. The results showed  
238 that these two plastics could not be separated without AOT (i.e., separation efficiency was almost 0%)  
239 because of the indiscriminate attachment of bubbles to both types of plastics. Fig. 5(a-1) shows the result  
240 of hybrid jig separation with 10 ppm of AOT. The PVC purity in the top layer and the PA purity in the  
241 bottom layer were 84% and 98%, respectively. Separation of PVC and PA occurred because AOT lowered  
242 the contact angle of PA but not that of PVC as shown in Fig. 5(b). However, bubble attachment  
243 probability on PVC slightly decreased with AOT addition (Fig. 5(b)) due to decrease of surface tension as  
244 discussed earlier (Fig. 4), that likely caused imperfect separation (Fig. 5(a-1)).

245 To improve the separation efficiency, a two-step hybrid jig method (pre-wetting of PA) is

246 proposed. In the first step, plastic mixture of PVC and PA are put in 10 ppm AOT solution for 3 min.

247 Then, solution is discharged, and water is filled instead (second step) and hybrid jig separation in water is

248 carried out. Fig. 5(a-2) shows that higher purities of PVC (94%) in the top layer and PA (99%) in the

249 bottom layers were obtained compared with the single-step approach because higher surface tension of

250 second step method than one-step method caused better bubble attachment on PVC (Fig. 5(a-1)).

251 However, due to the replacement of water in second step may cause some effect thus, effects of time after

252 water replacement was checked. The results showed that hybrid jig separation just after water

253 replacement was effective (Fig. 5(a-2)) however, several tens of minutes after water replacement showed

254 worse hybrid jig separation efficiency because bubble attachment to the PVC became difficult again. This

255 lower bubble attachment probability of PVC may cause by the decrease of surface tension due to the

256 detachment of AOT from PA surface. To understand the attachment and detachment behaviors of AOT on

257 PA, the adsorption and desorption experiments were carried out. The adsorption of AOT on PA was

258 confirmed (Fig. 6(a)) and desorption of AOT from PA with time (Fig. 6(b)) showed that AOT was readily

259 desorbed causing the surface tension of solution to decrease with time (Fig. 6(b)). In other words, the

260 separation results become bad with time because the wettability of PVC was enhanced due to the decrease

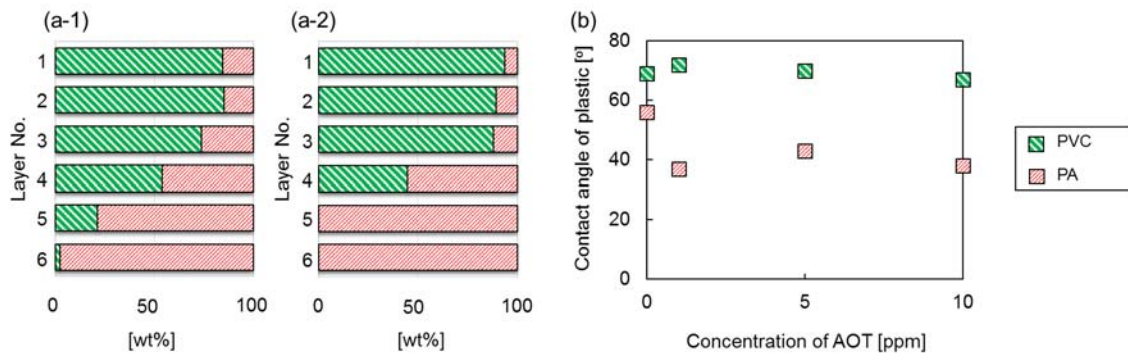
261 in surface tension of solution caused by the desorption AOT adsorbed on PA during the pre-wetting stage.

262 This means that although pre-wetting was effective, the adsorption-desorption behavior of wetting agent

263 could strongly affect the separation efficiency, so precise control of the wettability of samples is required.

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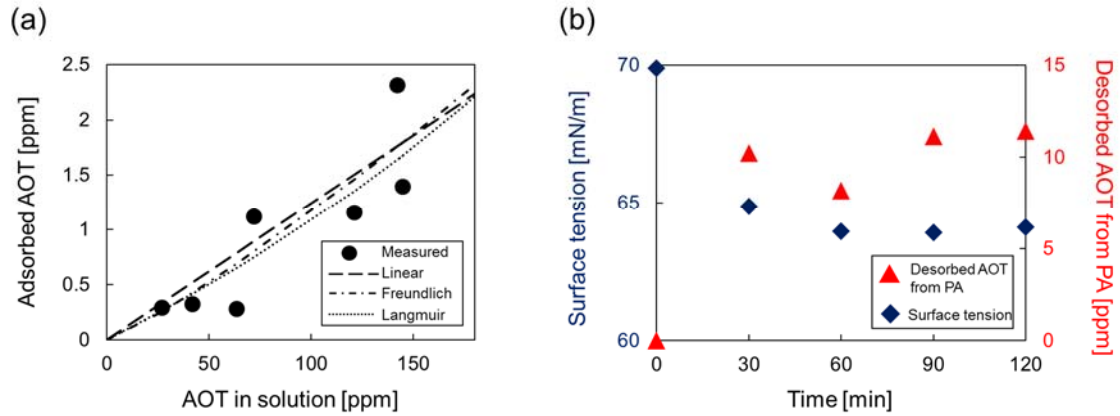
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267 **Fig. 5** (a) The proportion of PVC and PA in each layer after hybrid jig separation tests (a-1) in AOT (10

268 ppm) solution (one-step method) and (a-2) after solution replacement with water (two-step approach), and

269 (b) contact angles of PVC and PA in the AOT solutions

270



271

272

273 **Fig. 6** (a) Adsorption characteristics of AOT onto PA with linear, Freundlich and Langmuir isotherms, and

274 (b) desorbed AOT concentration from PA with time and the corresponding changes in the surface tension

275 of the solution

276

277 **Conclusions**

278

279 This paper evaluated the improvement of hybrid jig separation of mixed-plastic wastes using wetting  
280 agents and the findings of this study are summarized as follows:

281 • Wetting agents could change the surface tension of solutions by changing the water-air surface  
282 properties and the surface wettability (contact angle) of plastics by surface adsorption, both of which  
283 lowered the bubble attachment probability.

284 • For the separation of PPGF and HIPS, surface modification using wetting agents (i.e., AOT, NaLS  
285 or TA) could improve the separation efficiency.

286 • In the case of PPGF/HIPS with AOT, the changes in surface tension and the decrease of contact  
287 angles of both plastics caused lower bubble attachment probability, so selective attachment of  
288 bubbles was limited that caused lower separation efficiency.

289 • In the case of PPGF/HIPS with NaLS, the changes in surface tension were negligible and the contact  
290 angle on HIPS decreased while that on PPGF was unchanged, so selective attachment of bubbles on  
291 PPGF occurred and higher separation efficiency was obtained.

292 • In the case of PVC/PA with AOT, the surface tension decreased and the contact angle on PA  
293 decreased while that of PVC did not change, which caused selective attachment of bubbles on PVC.

294 • A two-step approach could increase the surface tension, increase the bubble attachment probability  
295 on PVC, and dramatically improved the hybrid jig separation efficiency.

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300

301 **References**

302

- 303 1. Statista (2019) Global plastic production from 1950 to 2017 (in million metric tons).  
304 <https://www.statista.com/statistics/282732/global-production-of-plastics-since-1950>. Accessed  
305 15 April 2018
- 306 2. PlasticsEurope (2018) Plastics - the facts 2018. an analysis of European plastics production,  
307 demand and waste data.  
308 [https://www.plasticseurope.org/application/files/6315/4510/9658/Plastics\\_the\\_facts\\_2018\\_AF\\_w](https://www.plasticseurope.org/application/files/6315/4510/9658/Plastics_the_facts_2018_AF_web.pdf)  
309 [eb.pdf](https://www.plasticseurope.org/application/files/6315/4510/9658/Plastics_the_facts_2018_AF_web.pdf). Accessed 22 April 2019
- 310 3. Tsunekawa M, Naoi B, Ogawa S, Hori K, Hiroyoshi N, Ito M, Hirajima T (2005) Jig separation  
311 of plastics from scrapped copy machines. *Int J Miner Process* 76:67-74.  
312 <https://doi.org/10.1016/j.minpro.2004.12.001>
- 313 4. Hori K, Tsunekawa M, Hiroyoshi N, Ito M (2009) Optimum water pulsation of jig separation for  
314 crushed plastic particles. *Int J Miner Process* 92:103-108.  
315 <https://doi.org/10.1016/j.minpro.2009.01.001>

- 316 5. Hori K, Tsunekawa M, Ueda M, Hiroyoshi N, Ito M, Okada H (2009) Development of a new  
317 gravity separator for plastics -a Hybrid-jig-. Mater Trans 50:2884-2847.  
318 <https://doi.org/10.2320/matertrans.M-M2009825>
- 319 6. Ito M, Tsunekawa M, Ishida E, Kawai K, Takahashi T, Abe N, Hiroyoshi N (2010) Reverse jig  
320 separation of shredded floating plastic - separation of polypropylene and high density  
321 polyethylene. Int J Miner Process 97:96-99. <https://doi.org/10.1016/j.minpro.2010.08.007>
- 322 7. Kuwayama Y, Ito M, Hiroyoshi N, Tsunekawa M (2011) Jig separation of crushed automobile  
323 shredded residue and its evaluation by float and sink analysis. J Mater Cycles Waste Manag  
324 13:240–246. <https://doi.org/10.1007/s10163-011-0008-y>
- 325 8. Tsunekawa M, Kobayashi R, Hori K, Okada H, Abe N, Hiroyoshi N, Ito M (2012) Newly  
326 developed discharge device for jig separation of plastics to recover higher grade bottom layer  
327 product. Int J Miner Process 114-117:27–29. <https://doi.org/10.1016/j.minpro.2012.09.003>
- 328 9. Phengsaart T, Ito M, Hamaya N, Tabelin CB, Hiroyoshi N (2018) Improvement of jig efficiency  
329 by shape separation, and a novel method to estimate the separation efficiency of metal wires in  
330 crushed electronic wastes using bending behavior and “entanglement factor”. Miner Eng  
331 129:54-62. <https://doi.org/10.1016/j.mineng.2018.09.015>
- 332 10. Pita F, Castilho A (2016) Influence of shape and size of the particles on jigging separation of  
333 plastics mixture. Waste Manage 48:89-94. <https://doi.org/10.1016/j.wasman.2015.10.034>
- 334 11. Ferrara G, Bevilacqua P, Lorenzi L, Zanin M (2000) The influence of particle shape on the

- 335 dynamic dense medium separation of plastics. *Int J Miner Process* 59:225-235.
- 336 [https://doi.org/10.1016/S0301-7516\(99\)00078-2](https://doi.org/10.1016/S0301-7516(99)00078-2)
- 337 12. Pongstabodee S, Kunachitpimol B, Damronglerd S (2008) Combination of three-stage sink-float  
338 method and selective flotation technique for separation of mixed post-consumer plastic waste.  
339 *Waste Manage* 28:475-483. <https://doi.org/10.1016/j.wasman.2007.03.005>
- 340 13. Richard GM, Mario M, Javier T, Susana T (2011) Optimization of the recovery of plastics for  
341 recycling by density media separation cyclones. *Resour Conserv Recycl* 55: 472-482.  
342 <https://doi.org/10.1016/j.resconrec.2010.12.010>
- 343 14. Dodbiba G, Shibayama A, Sadaki J, Fujita T (2003) Combination of triboelectrostatic separation  
344 and air tabling for sorting plastics from a multicomponent plastic mixture. *Mater Trans*  
345 44:2427-2435. <https://doi.org/10.2320/matertrans.44.2427>
- 346 15. Dodbiba G, Sadaki J, Okaya K, Shibayama A, Fujita T (2005) The use of air tabling and  
347 triboelectric separation for separating a mixture of three plastics. *Miner Eng* 18:1350-1360.  
348 <https://doi.org/10.1016/j.mineng.2005.02.015>
- 349 16. Gente V, Marca FL, Lucci F, Massacci P (2003) Electrical separation of plastics coming from  
350 special waste. *Waste Manage* 23:951-958. [https://doi.org/10.1016/S0956-053X\(03\)00088-6](https://doi.org/10.1016/S0956-053X(03)00088-6)
- 351 17. Shent H, Pugh RJ, Forssberg E (1999) A review of plastics waste recycling and the flotation of  
352 plastics. *Resour Conserv Recycl* 25:85-109. [https://doi.org/10.1016/S0921-3449\(98\)00017-2](https://doi.org/10.1016/S0921-3449(98)00017-2)
- 353 18. Fraunholz N (2004) Separation of waste plastics by froth flotation—a review, part I. *Miner Eng*



- 354 17:261-268. <https://doi.org/10.1016/j.mineng.2003.10.028>
- 355 19. Wang C, Wang H, Fu J, Liu Y (2015) Flotation separation of waste plastics for recycling—A  
356 review. *Waste Manage* 41:28–38. <https://doi.org/10.1016/j.wasman.2015.03.027>
- 357 20. Güney A, Özdilek C, Kangal MO, Burat F (2015) Flotation characterization of PET and PVC in  
358 the presence of different plasticizers *Separation and Purification Technology*. 151:47-56  
359 <https://doi.org/10.1016/j.seppur.2015.07.027>
- 360 21. Burat F, Güney A, Kangal MO (2009) Selective separation of virgin and post-consumer  
361 polymers (PET and PVC) by flotation method. *Waste Manage* 29:1807-1813.  
362 <https://doi.org/10.1016/j.wasman.2008.12.018>
- 363 22. Shibata J, Matsumoto S, Yamamoto H, Lusaka E, Pradip (1996) Flotation separation of plastics  
364 using selective depressants. *Int J Miner Process* 48:127-134.  
365 [https://doi.org/10.1016/S0301-7516\(96\)00021-X](https://doi.org/10.1016/S0301-7516(96)00021-X)
- 366 23. Marques GA, Tenório JAS (2000) Use of froth flotation to separate PVC/PET mixtures. *Waste*  
367 *Manage* 20: 265-269. [https://doi.org/10.1016/S0956-053X\(99\)00333-5](https://doi.org/10.1016/S0956-053X(99)00333-5)
- 368 24. Saisinchai S (2013) Separation of PVC from PET/PVC mixtures using flotation by calcium  
369 lignosulfonate depressant. *Eng J* 18:45-54. <https://doi.org/10.4186/ej.2014.18.1.45>
- 370 25. Wang H, Wang C, Fu J, Gu G (2014) Flotability and flotation separation of polymer materials  
371 modulated by wetting agents. *Waste Manage.* 34:309-315  
372 <https://doi.org/10.1016/j.wasman.2013.11.007>

- 373 26. Pita F, Castilho A (2017) Separation of plastics by froth flotation. The role of size, shape and  
374 density of the particles. *Waste Manage* 60:91-99. <https://doi.org/10.1016/j.wasman.2016.07.041>
- 375 27. Takoungsakdakun T, Pongstabodee S Separation of mixed post-consumer PET–POM–PVC  
376 plastic waste using selective flotation. *Sep Purif Technol* 54:248-252.  
377 <https://doi.org/10.1016/j.seppur.2006.09.011>
- 378 28. Dodbiba G, Haruki N, Shibayama A, Miyazaki T, Fujita T (2002) Combination of sink–float  
379 separation and flotation technique for purification of shredded PET-bottle from PE or PP flakes.  
380 *Int J Miner Process* 65:11-29. [https://doi.org/10.1016/S0301-7516\(01\)00056-4](https://doi.org/10.1016/S0301-7516(01)00056-4)
- 381 29. Jeon S, Ito M, Tabelin CB, Pongsumrankul R, Kitajima N, Hiroyoshi N (2018) Gold recovery  
382 from shredder light fraction of E-waste recycling plant by flotation-ammonium thiosulfate  
383 leaching. *Waste Manage* 77:195–202. <https://doi.org/10.1016/j.wasman.2018.04.039>
- 384 30. Wills BA, Napier-Munn TJ (2006) *Mineral Processing Technology*, seventh ed. Pergamon press,  
385 Oxford
- 386 31. Brozek M, Surowiak A (2007) Effect of particle shape on jig separation efficiency. *Physicochem*  
387 *Probl Mi* 41:397-413
- 388 32. Beunder EM (2000) Influence of shape on particle behaviour in recycling techniques.  
389 Dissertation, Delft University of Technology
- 390 33. Boylu F, Cinku K, Cetinel T, Karakas F, Guven O, Karaagaclioglu IE, Celik MS (2015) Effect of  
391 coal moisture on the treatment of a lignitic coal through a semi-pilot-scale pneumatic

392 stratification jig. Int J Coal Prep Util 35:143-153.  
393 <https://doi.org/10.1080/19392699.2015.1005743>

394 34. Butt HJ, Graf K, Kappl M (2003) Physics and Chemistry of Interfaces, first ed., Wiley-VCH  
395 Verlag GmbH & Co. KGaA, Weinheim

396 35. Firouzi M, Nguyen AV, Hashemabadi SH (2011) The effect of microhydrodynamics on  
397 bubble-particle collision interaction. Miner Eng 24:973-986.  
398 <https://doi.org/10.1016/j.mineng.2011.04.005>

399 36. Zhao Y, Li YP, Huang J, Liu J, Wang WK (2015) Rebound and attachment involving single  
400 bubble and particle in the separation of plastics by froth flotation. Sep Purif Technol  
401 144:123-132. <https://doi.org/10.1016/j.seppur.2015.02.016>