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Effect of retarders on flow and strength development of alkali-activated fly ash/blast furnace slag composite

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Abstract

Geopolymer concrete presents a major problem regarding its practical application, in that the geopolymer paste has very short setting time. Previous studies have shown that the addition of blast furnace slag to geopolymer paste considerably shortens the setting time. Based on these findings, in the present study, setting retarders were used to lengthen the setting time of the geopolymer paste. The objective of the present study was to identify the effect of a setting retarder on the fluidity and compressive strength of alkali-activated fly ash/blast furnace slag-based materials. It was shown that, by adding a chelator as a retarder, the setting time can be prolonged. However, the setting time was found to be dependent on the type of chelator. Similarly, the compressive strength development of the geopolymer was also found to be dependent on the type of chelator. It was clarified that the concentration of calcium and aluminum in solution during hardening changes with the addition of a chelator, and it was shown that there is a correlation between the concentrations of calcium and aluminum and the setting time.

Keywords:

Geopolymer, Fly ash, Blast furnace slag, Compressive strength, Setting time, Retarder, Chelator

1. Introduction

Cementitious materials such as concrete are widely used in many fields including reinforced-concrete buildings, roads, dams, and bridges. The main component of concrete is cement. However, the process whereby cement is produced is a major source of CO₂, a recognized greenhouse gas and a contributor to global warming. Therefore, to reduce CO₂ emissions, there is a necessity to reduce cement consumption. It has been reported that around 13.5 trillion tons of CO₂ are produced by global cement production every year, which accounts for about 7% of all greenhouse-gas emissions [1]. To reduce the CO₂ emissions of the cement industry, therefore, blended cement is nowadays being widely used. In this product, the cement is partially replaced by by-products such as blast furnace slag and/or fly ash. However, the cement production process remains a major source of CO₂ emissions. As mentioned above, the ultimate goal would be the development of a cement-free material and, to this end, geopolymer concrete has been attracting considerable attention. Geopolymers, first developed by Davidovits [2], are alkali aluminosilicate binders formed by the alkali silicate activation of aluminosilicate binders [3]. Geopolymers exhibit comparable or superior mechanical properties to those of Portland cement [4-6]. It is also well known that geopolymers possess excellent fire resistance (relative to organic materials) and acid resistance [7,8]. Although geopolymers have been studied for application as fire-resistant polymers, they have also been studied for use as construction materials [9]. However, when a geopolymer is to be used as a construction material, it is important to be aware of its physical properties, including its compressive strength and workability.

Previous studies have found that geopolymers have a high compressive strength but poor workability compared to cement-based concrete. Most previous studies focused on these two factors. Apha et al. studied the effect of a naphthalene-based superplasticizer (NSP) on the compressive strength and workability of a lignite bottom-ash geopolymer [10]. They concluded that NSP was not effective in a geopolymer system activated with NaOH and sodium silicate solutions because, at an NSP/ash ratio of more than 0.09, the strength of the mortar decreased to 40 MPa even though the workability of the mortar was improved. Behzad et al. studied the effects of different plasticizers (SPs) and activator combinations on the workability and strength of a fly-ash-based geopolymer [11]. They concluded that the effect of different SPs on the workability and strength of the fly-ash-based geopolymer is directly dependent on the types of the activator and SPs. A naphthalene-based SP was effective in the case of a sample activated only by a NaOH solution. Polycarboxylate-based SP was effective in the case of a sample activated by a multi-compound activator (NaSiO₃/NaOH = 2.5). Chindaprasirt et al. studied the workability and strength of a coarse high-calcium fly-ash geopolymer with extra water or a SP [12]. They mentioned that the strengths of mortars with extra water were consistently higher than those of mortars with the SP. The reduction in the strength of the mortar with SP in comparison to those of mortar with extra water were found to be dependent on the sodium silicate to NaOH ratio. Hardjito et al. studied the effect of adding a commercially available naphthalene-based high-range water-reducing admixture [13]. They concluded that the addition of the high-range water-reducing

admixture improved the workability of the fresh concrete, but it had very little effect on the compressive strength in amounts up to approximately 2% of the amount of fly ash. The aims of these studies were to attain both high strength and good workability. To this end, the flow value was evaluated as an indicator of the workability. Many studies addressed the compressive strength and flow values when using a SP. In contrast, very few studies evaluated the setting time, which is as important as the workability [14,15,16,17,18].

Against this background, the present study focused on the setting time, with chelators being used as setting retarders. The effect of the chelators on the compressive strength and setting time were evaluated for geopolymers based on blast furnace slag and/or fly ash, and activated by a potassium silicate solution.

2. Experimental

2.1 Sample preparation

The materials used in this study are listed in Table 1. Fly ash (FA) and blast furnace slag (BFS) were used as the aluminosilicate precursors while potassium silicate (PS) was used as the alkali solution. The chemical compositions of these are listed in Table 2. As chelators (CA), HIDS ($C_8H_7NO_9 \cdot 4Na$), EDTA-4Na ($C_{10}H_{12}N_2Na_4O_8 \cdot 4H_2O$), and GLDA ($C_9H_9NNa_4O_8$) were used, as listed in Table 3. Three types of CA with different chelating values were selected, as listed in Table 3. The HIDS was produced by Nippon Shokubai [19]. The chelators bind to a metal ion by coordination with a plurality of coordination sites to form a complex and collect the metal ion. Therefore, it is thought that structure formation can be delayed.

The mixing proportions for the specimens are listed in Table 4. CA (in solid content) was added at a ratio of 4.0 wt% with respect to the amount of alkali activated filler (AF), after which the chelating values were compared. The powders were first mixed for 30 s, after which an activator was added and then mixed for a further 10 min. After mixing, the samples were put in molds measuring $40 \times 40 \times 160 \text{ mm}^3$. After curing for 1 day at $20 \text{ }^\circ\text{C}$, the samples were demolded and then allowed to cure at $20 \text{ }^\circ\text{C}$ in a sealed container (to prevent drying) until the desired degree of aging had been attained.

2.2 Experimental method

In the present study, the slump flow value, electrical resistivity, and concentration of the solution was measured for the fresh geopolymer pastes. The compressive strength, degree of reaction of BFS and FA (as determined by SEM observations), and an elemental analysis by EDX were conducted on the hardened geopolymer paste.

(1) Slump flow test

The slump flow value was determined as specified in JASS15M-103 (shown in Figure 1, using a cylindrical sample measuring $\varnothing 50 \times 50 \text{ mm}$). The slump flow value was measured at 0, 30, 60, 90, 120, 150, and 180 min after mixing, as shown in Figure 2.

(2) Measurement of electrical resistivity

To measure the electrical resistivity, an impedance analyzer (HIOKI IM3570) was used. The size of the electrode plates used for the measurements was $30 \times 30 \text{ mm}^2$. These were embedded in the specimen, 30 mm apart, when the sample was cast. The

measurements were performed with an applied voltage of 0.1 V, a frequency of 4Hz–5 MHz, at room temperature (20 °C). The electrical resistivity was determined by calculating the impedance by assuming that the geopolymers are composed of a circuit with a resistor and capacitor in parallel. The electrical resistivity was measured at 0, 30, 60, 90, 120, 150, and 180 min after mixing.

(3) Measurement of ion concentration in solution

The Ca, K, Si, and Al concentrations in solution were measured by using ICP. The solutions used for the measurements were extracted by centrifugation from the samples at 30, 60, and 90 min after mixing.

(4) Compressive strength test

The samples used for the measurements were cut down to $40 \times 40 \times 40 \text{ mm}^3$. The compressive strength was calculated from the maximum stress divided by the area of the sample surface.

(5) Determination of degree of reaction of FA and BFS from backscattered electron (BSE) image

The samples used for the observations were cut down to $5 \times 5 \times 5 \text{ mm}^3$, and were freeze-dried to stop the reaction. The dried specimens were immersed in epoxy resin and, once the epoxy hardened, the surfaces were polished using SiC paper and diamond paste to give a flat surface. The amounts of unreacted blast furnace slag and fly ash were detected, allowing the degree of reaction of the blast furnace slag and fly ash, as well as the amount of reaction product, to be calculated. SEM observations were performed with an applied voltage of 15 keV, a working distance of 17 mm, a magnification of 500, and a pixel size of $0.32 \mu\text{m}$. Element analysis was conducted with energy dispersive X-ray analysis (EDX). The points were set close to the unreacted blast furnace slag or fly ash, allowing the CaO/SiO_2 , $\text{Al}_2\text{O}_3/\text{SiO}_2$, and $(\text{CaO}+\text{K}_2\text{O})/\text{SiO}_2$ values to be calculated. The conditions were the same as those used for the SEM observations. The references used to determine the concentration were wollastonite (CaSiO_3) and orthoclase (KAlSi_3O_8). In the present study, the target elements were Ca, Si, Al, and K. Twenty images were analyzed using a threshold to acquire the fraction of unreacted blast furnace slag (Figure 3), and grids (24×32) were set as shown in Figure 4 to acquire the fraction of unreacted fly ash by using a point-counting method [20]. Based on Delesse theory, the degree of reaction (R_{FA} or R_{BFS}) and the amount of reacted product (V_p) were calculated using the following formulas and assuming no shrinkage of the specimens [21].

$$R_{\text{BFS}} = \frac{V_{\text{BFS}}^i - V_{\text{BFS}}^u}{V_{\text{BFS}}^i} \quad (1)$$

$$R_{\text{FA}} = \frac{V_{\text{FA}}^i - V_{\text{FA}}^u}{V_{\text{FA}}^i} \quad (2)$$

$$V_p = 1 - V_{\text{BFS}}^u - V_{\text{FA}}^u \quad (3)$$

where V_{BFS}^i is the initial volume of BFS, V_{FA}^i is the initial volume of FA, V_{BFS}^u is the volume of unreacted BFS at the time of measurement, and V_{FA}^u is the volume of unreacted FA at the time of measurement.

3. Results

(1) Slump flow test

Figure 5 shows the results of the slump flow test. A flow value of '100' indicates that the flow value could not be measured because the sample hardened. The time required for the samples with HIDS and GLDA-4Na to set was 2.5 times longer than that required for the 'NONE' sample. The time required for the sample with EDTA-4Na to set was 1.5 times longer than that required for the 'NONE' sample. The time required for each sample to set was retarded by the presence of a chelator. Specifically, HIDS and GLDA-4Na were both able to retard the setting time but had little effect on the slump flow value.

(2) Electrical resistivity

Figure 6 shows the measured values of electrical resistivity. The normalized electrical resistivity was calculated by dividing the values at the time of the measurement by the value at 0 h, for each sample. The electrical resistivity was found to increase over time. The electrical resistivity of the samples with HIDS and GLDA-4Na were higher than that of the 'NONE' sample. This is probably because the ion concentration in the solution is low.

(3) Concentration in solution

The results obtained for the concentration in solution are shown in Figures 7–10. The Ca and Al concentrations of each sample increased over time. The Ca and Al concentrations of EDTA-4Na were equal to or greater than that of the 'NONE' sample. The Ca and Al concentrations in solution with HIDS were the lowest. The Si and K concentrations remained the same regardless of whether a chelator is used or the amount of time that is allowed to elapse.

(4) Compressive strength

Figure 11 shows the results obtained for the compressive strength. The compressive strength was found to increase over time. The compressive strengths of the samples with EDTA-4Na and GLDA-4Na after aging for 28 days were 15 MPa less than that of the 'NONE' sample. However, the compressive strength of the sample mixed with HIDS was the same as that of the 'NONE' sample. It was shown that HIDS did not inhibit the reaction.

(5) Degree of reaction of BFS and FA, and amount of reacted product as determined from BSE image

Figures 12 to 14 show the degrees of reaction obtained for blast furnace slag (BFS) and fly ash (FA), as well as the amount of reacted product. The degree of reaction of BFS (Figure 12) with EDTA and GLDA-4Na is lower than that of the 'NONE' specimen. That is, the reaction may be inhibited by the presence of these chelators. However, the degree of reaction of FA (Figure 13) was almost the same and increased with the curing period. Therefore, it was shown that the effect of the chelating agent on the reaction was minimal. The amount of reacted product (Figure 14) for all the specimens remained the same regardless of the presence or absence of a chelator. There is very little difference in the range which can be observed with an electron microscope.

(6) Element analysis by EDX

Figures 15–17 show the results of the element analysis of reacted product as performed by EDX. The CaO/SiO_2 and $(\text{CaO}+\text{K}_2\text{O})/\text{SiO}_2$ molar ratios (Figure 15 and 16) decreased with the curing time. It is thought that the amount of SiO_2 increased as a result of the progress of the fly ash reaction. Furthermore, the $\text{Al}_2\text{O}_3/\text{SiO}_2$ molar ratio (Figure 17) increased with the curing time except in the case of the HIDS sample. The molar ratios in the HIDS sample were higher than those of the other samples. This shows that the reaction in the HIDS sample is accelerating.

4. Discussion

4.1 Effect of chelator on fluidity

Figures 18–21 show the relationships between the normalized slump flow and the concentration of the solution. Normalized flow values, obtained by dividing the slump flow values by the slump values at 0.5 h, are shown. The slump flow values were found to decrease with the Ca and Al concentrations in the solution. The relationship between the Si and K concentration and slump flow values were not clear. Therefore, it is likely that the Ca and Al affect the slump flow value and setting time. In the sample mixed with HIDS, the setting time became longer because the concentrations of Al and Ca were low. It was reported that HIDS form stable water-soluble complexes with various metal ions over a wide pH range, with the chelating ability of Fe^{3+} in an alkaline solution being particularly high [19,22]. Therefore, it is thought that HIDS forms a complex of calcium or aluminum.

Figures 22–25 show the relationships between the electrical resistivity and concentration in the solution. The normalized electric resistivity obtained by dividing the measured values by the values at 0.5 h is shown. The electrical resistivity was found to decrease as the Ca and Al concentrations increased. In contrast, there is no clear relationship between the Si and K concentrations and the electrical resistivity. This also indicates that the Ca and Al concentrations greatly influence the structure formation.

4.2 Effect of chelator on compressive strength

Figure 26 shows the relationship between the compressive strength and density. The compressive strength was found to be proportional to the density. Therefore, the density has considerable influence on the compressive strength, given that the density is proportional to the amount of air trapped in the specimen. Therefore, it is thought that some chelators generate air in high alkali conditions.

Figures 27 and 28 show the relationship between degree of reaction of BFS and FA and the compressive strength. Figure 29 shows the relationship between the amount of reacted product and the compressive strength. The compressive strength was found to increase with the degree of reaction. In the same way, the compressive strength increased with the amount of reacted product. It can be concluded that the compressive strength increases as space is filled with the reacted product. It has been pointed out that the formation of C-A-S-H contributes to the strength development in a slag–FA system [14,23].

Figures 30–33 show the relationship between the element composition (as determined

by EDX-element analysis) and the compressive strength. There is no clear relationship between the element composition and the compressive strength. These results show that the air content (density) and the degree of reaction influence the strength development. It has been shown that the strength development can be controlled by using an appropriate chelator.

5. Conclusion

The effect of adding chelators as a setting retarder to blast furnace slag and a fly ash-based geopolymer paste was shown to be as follows:

(1) The chelators prolonged the setting time of the geopolymer paste, but the degree of prolongation depends on the type of the chelator that is used. HIDS was shown to be most effective.

(2) It was shown that the strength development also varies depending on the type of chelators.

(3) The concentrations of Ca and Al changed over time with the addition of a chelator, while these are also related to the setting time.

Therefore, the setting time was improved by adding a chelator to a geopolymer paste based on blast furnace slag and fly ash. This is extremely relevant to the practical application of geopolymers in engineering.

Acknowledgement

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Table1 Materials used in this study

		Material	Physical character
AF: Activated Filler	BFS	Blast furnace slag	Density: 2.91g/cm ³ Specific Surface Area: 3830cm ² /g
	FA	Fly ash	Density :2.33g/cm ³ Specific Surface Area :3740cm ² /g
Activator	PS	Potassium silicate solution	Density: 1.58 g/cm ³ , Concentration 51.0 wt%

Table2 Chemical composition of the materials

	Chemical composition (%)											
	SiO ₂	TiO ₂	Al ₂ O ₃	Fe ₂ O ₃	MnO	MgO	CaO	Na ₂ O	K ₂ O	P ₂ O ₅	Cl	S
BFS	33.90	0.50	14.61	1.03	-	6.04	43.28	0.23	0.25	-	-	-
FA	61.7	1.23	24.0	6.1	0.08	1.11	2.57	0.82	1.51	0.78	-	0.04
PS	29.1	-	-	-	-	-	-	-	21.9	-	-	-

Table3 Chelator used in this study

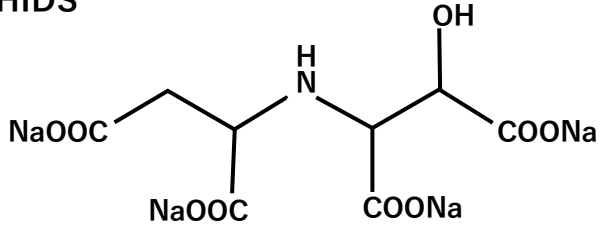
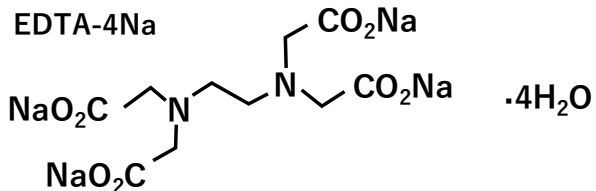
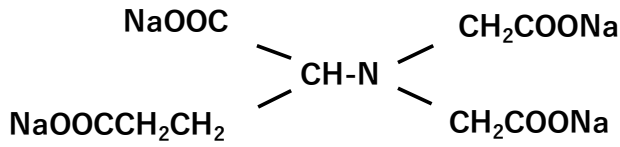
		Material	Physical properties
Chelator (CA)	HIDS	3-hydroxy-2,2'-iminodisuccinic acid tetra sodium($C_8H_7NO_9 \cdot 4Na$)	Molecular weight: 353.1 Chelating value: 300mg- $CaCO_3/g$ Solid content: 50wt%
		HIDS 	
	EDTA-4Na	Tetra sodium ethylene diamine tetra acetate($C_{10}H_{12}N_2Na_4O_8 \cdot 4H_2O$)	Molecular weight: 452 Chelating value: 221mg- $CaCO_3/g$ Solid content: 100wt%
		EDTA-4Na 	
	GLDA-4Na	Tetra sodium L-glutamic acid diacetate($C_9H_9NNa_4O_8$)	Molecular weight: 351 Chelating value: 115mg- $CaCO_3/g$ Solid content: 40wt%
		GLDA-4Na 	

Table 4 Mix proportions

	Curing condition	Age	BFS/AF wt%	FA/AF wt%	PS/AF wt%	W/AF wt%	CA(solid content)/AF wt%
NONE	20°C -Sealed	3,7,28-day	20	80	60	6.0	4.0
HIDS							
EDTA-4Na							
GLDA-4Na							

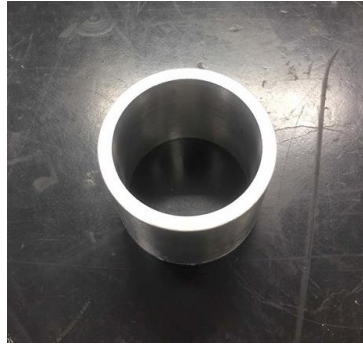


Figure1 JASS15M-103



Figure 2 Slump flow test

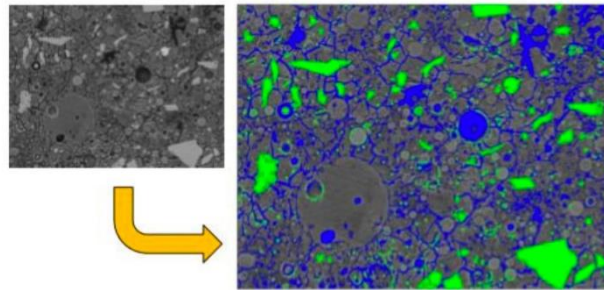


Figure 3 Image applied “threshold” on image J

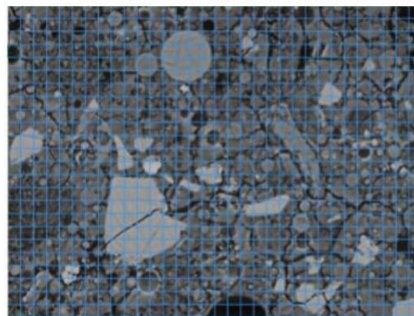


Figure 4 Image set grids for point counting method

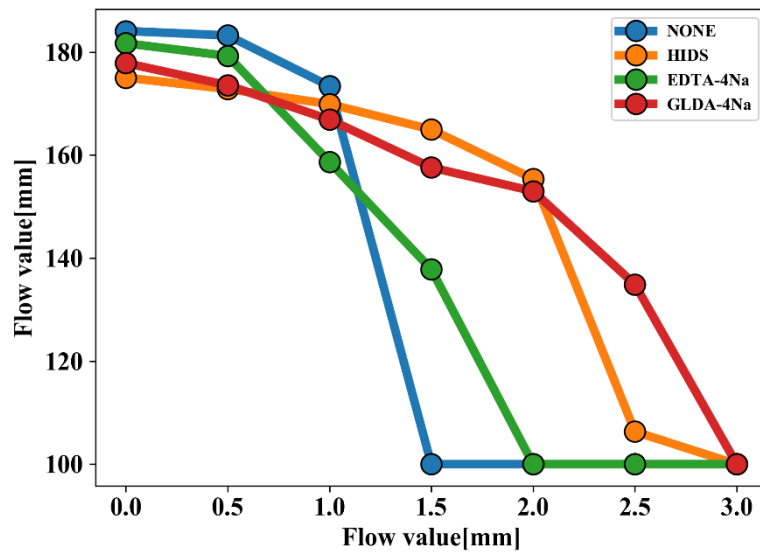


Figure 5 Change of slump flow value with time

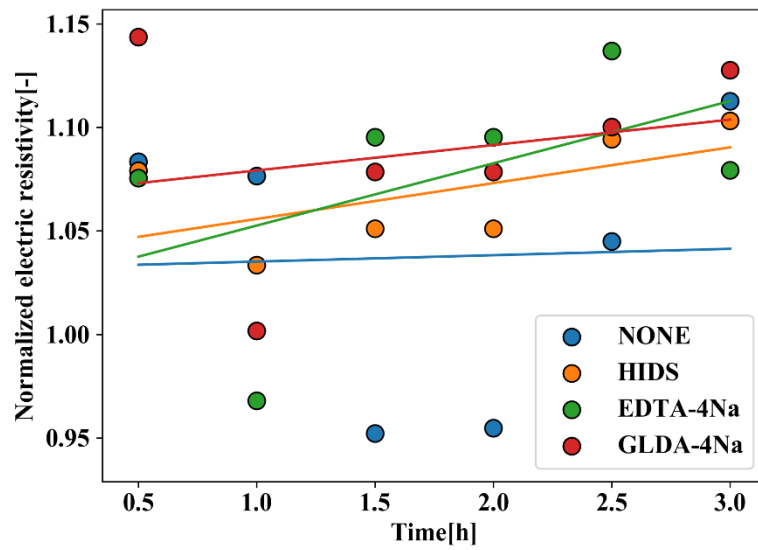


Figure 6 Change of electric resistivity with time

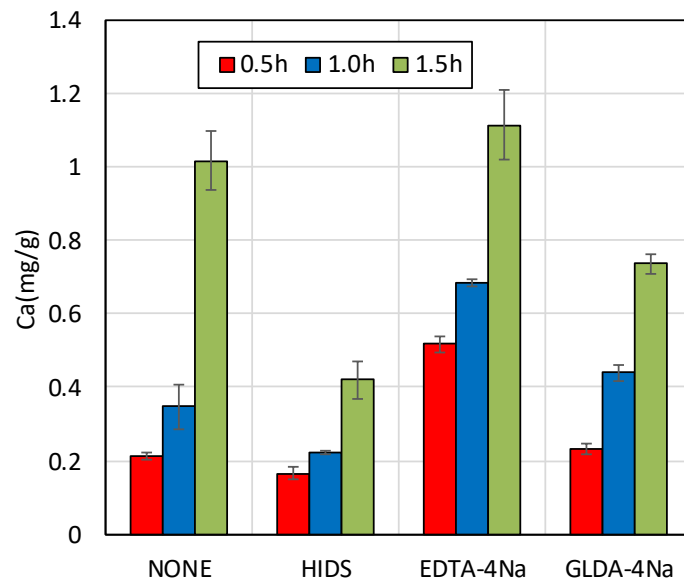


Figure 7 Concentration of Ca in solution

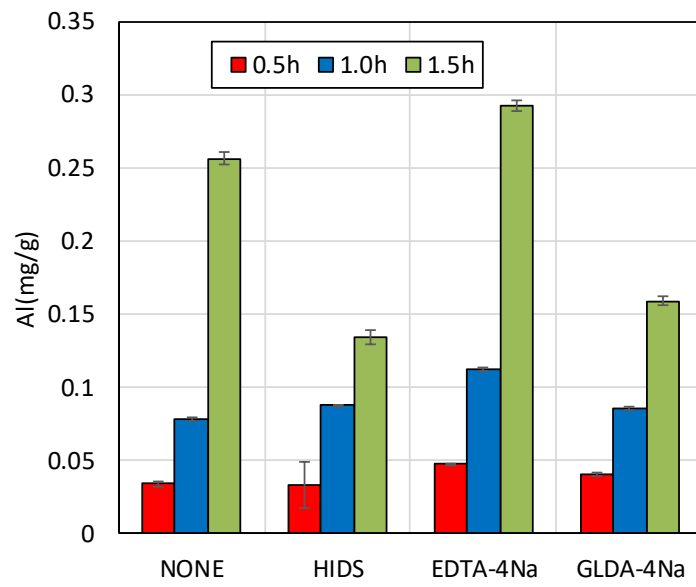


Figure 8 Concentration of Al in solution

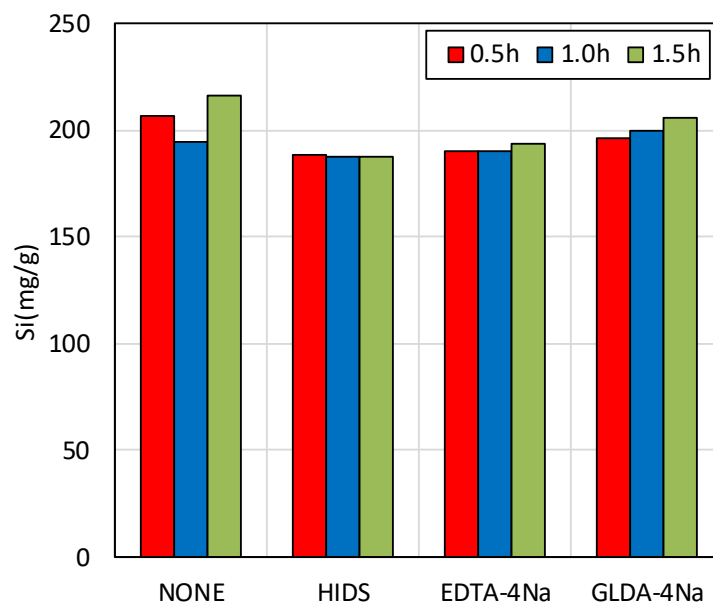


Figure 9 Concentration of Si in solution

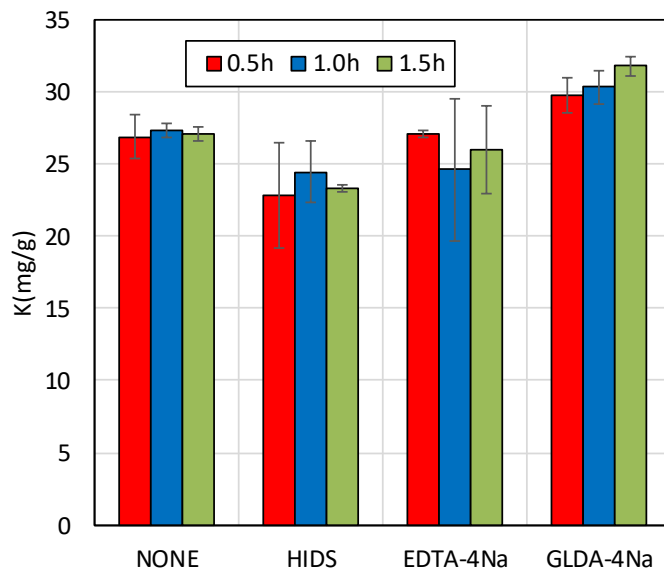


Figure 10 Concentration of K in solution

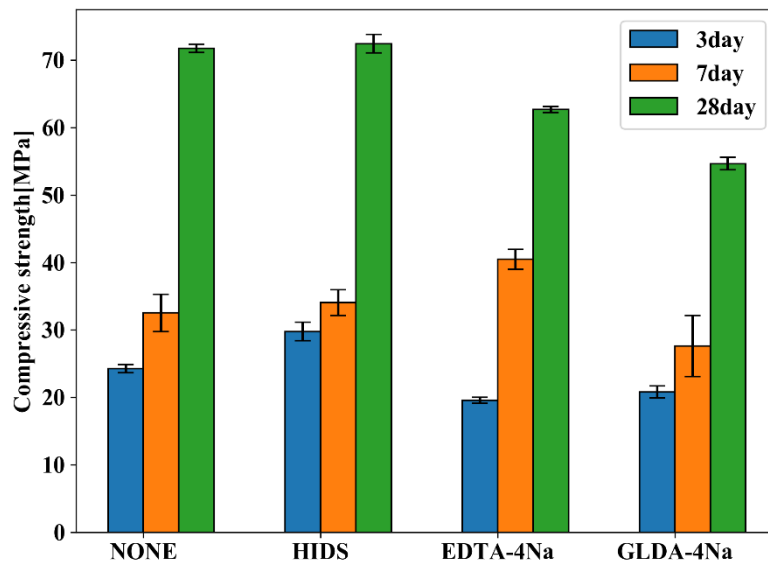


Figure 11 Compressive strength

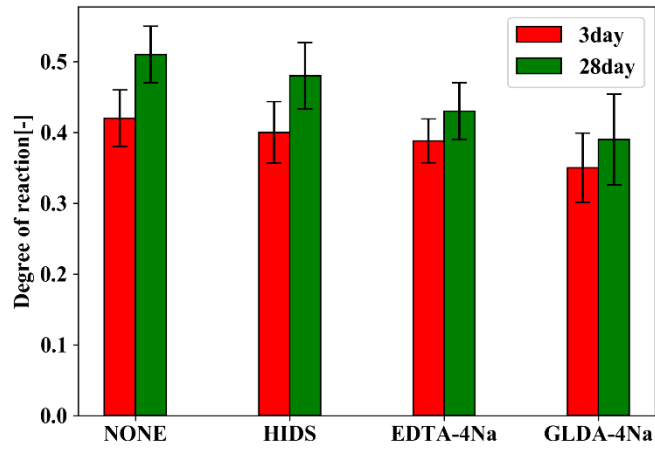


Figure 12 Degree of reaction of blast furnace slag

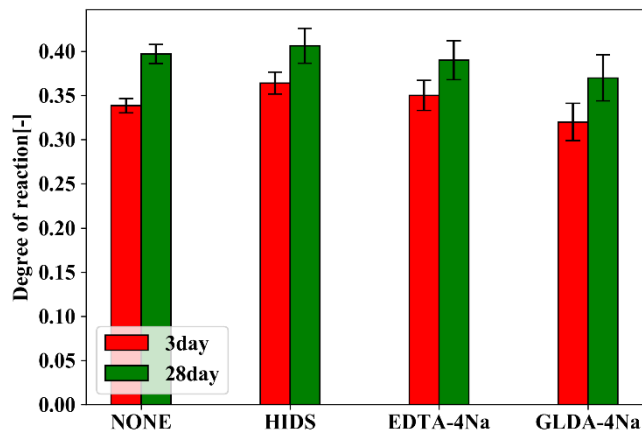


Figure 13 Degree of reaction of fly ash

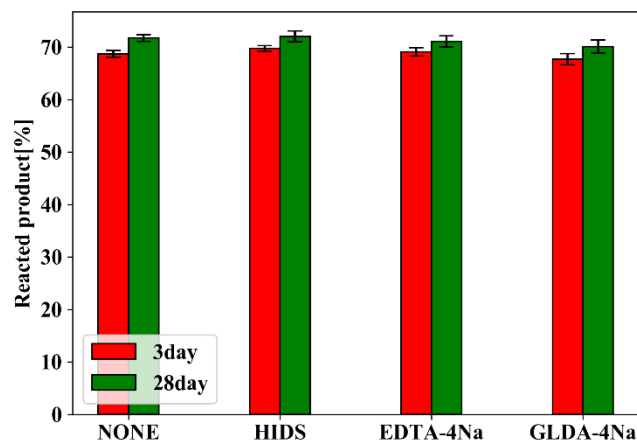


Figure 14 The amount of reacted product

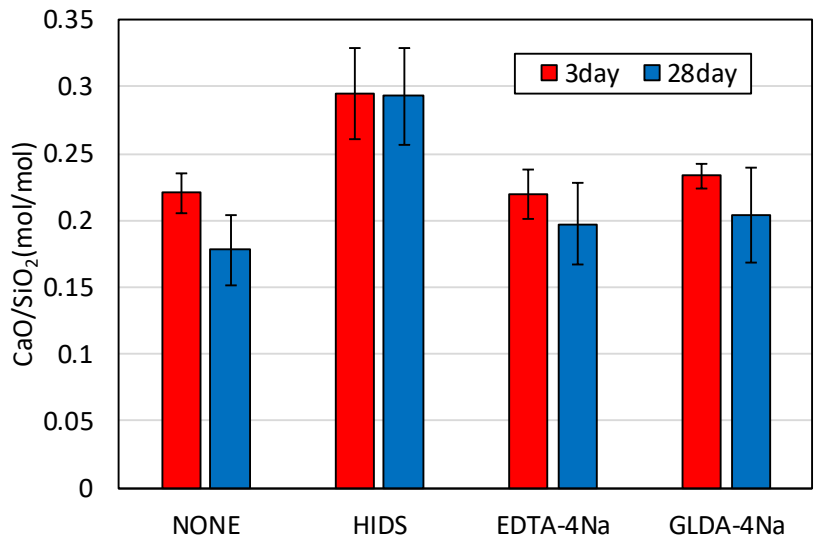


Figure 15 Result of EDX analysis of CaO/SiO₂

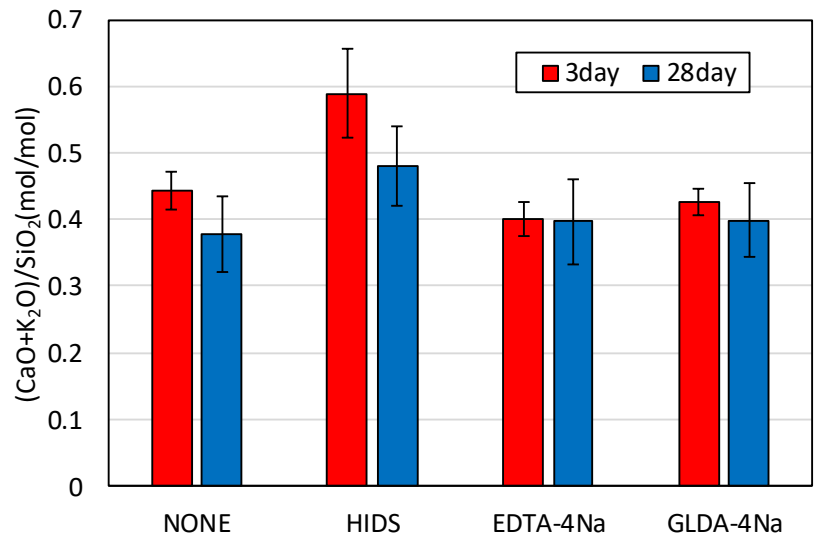


Figure 16 Result of EDX analysis of (CaO+K₂O)/SiO₂

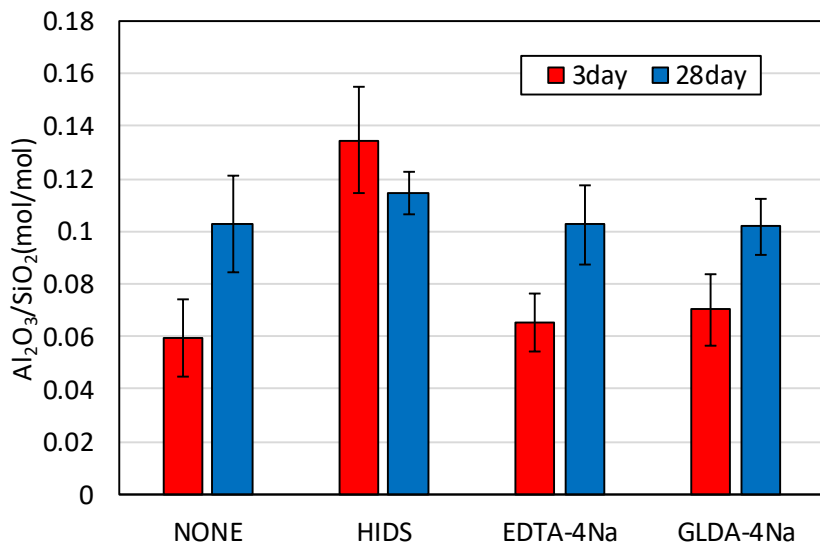


Figure 17 Result of EDX analysis of Al₂O₃/SiO₂

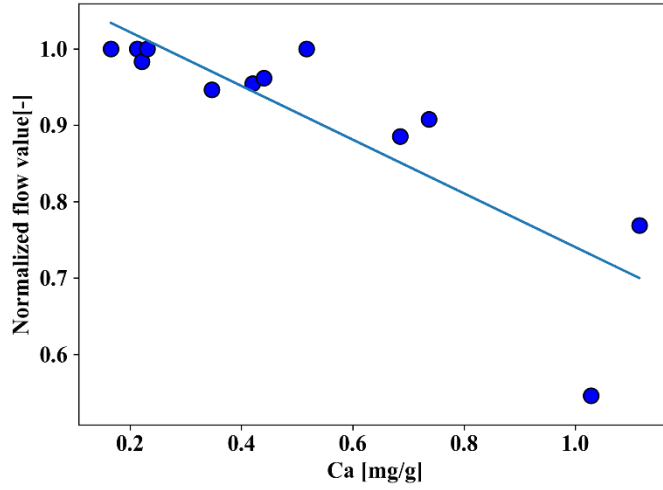


Figure18 Relationship between Ca concentration and normalized slump flow value

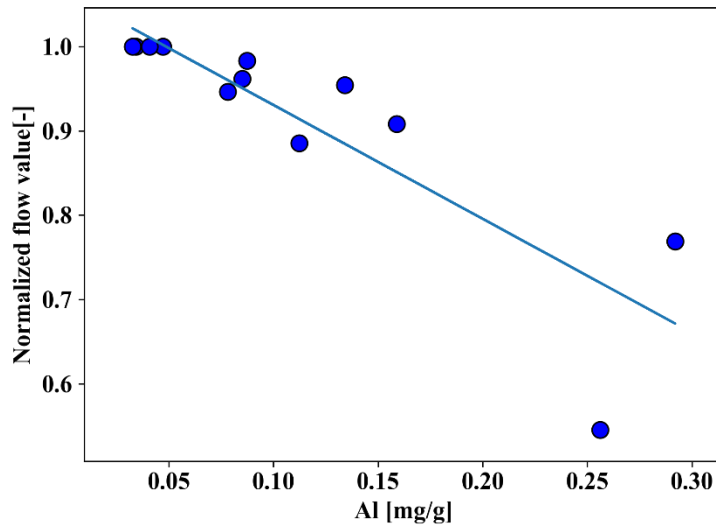


Figure 19 Relationship between Al concentration and normalized slump flow value

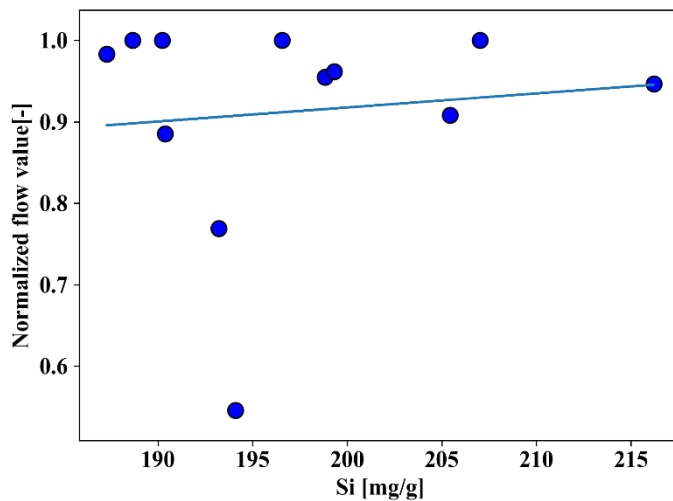


Figure 20 Relationship between Si concentration and normalized slump flow value

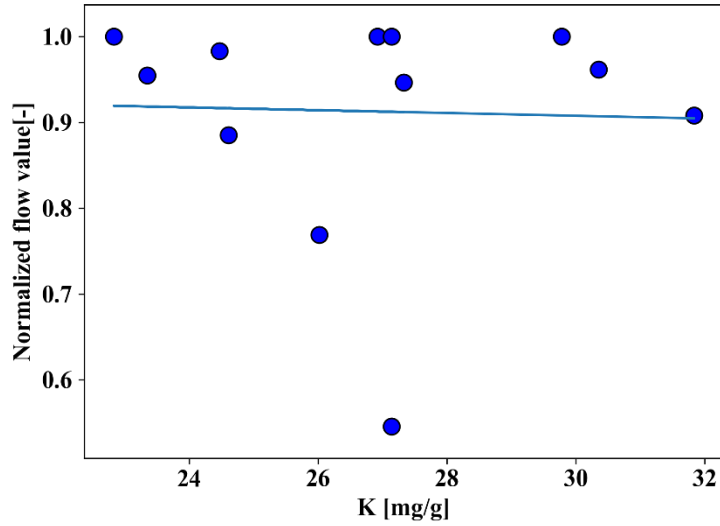


Figure 21 Relationship between K concentration and normalized slump flow value

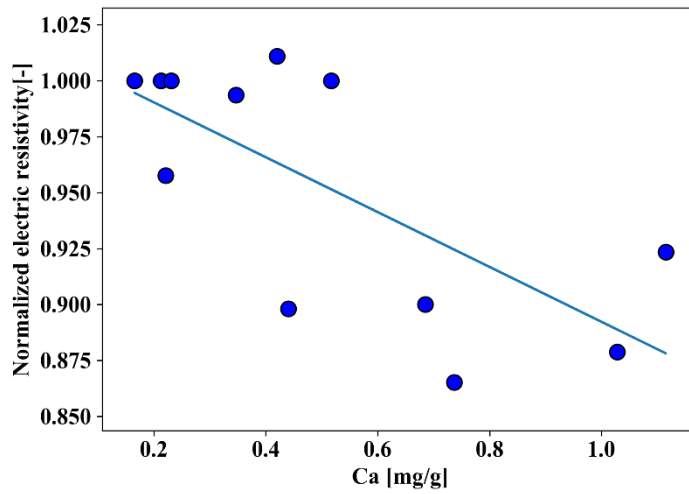


Figure22 Relationship between Ca concentration and normalized electric resistivity

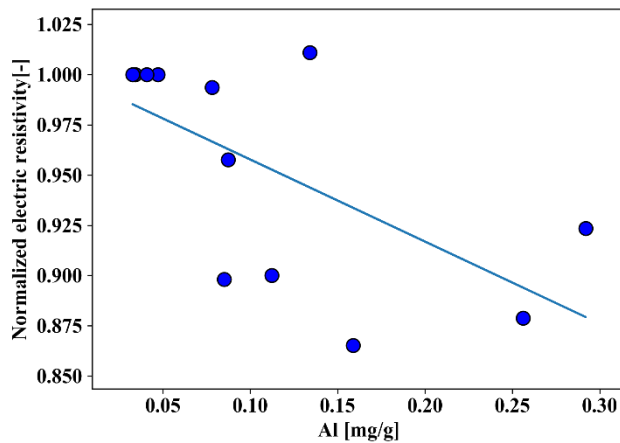


Figure23 Relationship between Al concentration and normalized electric resistivity

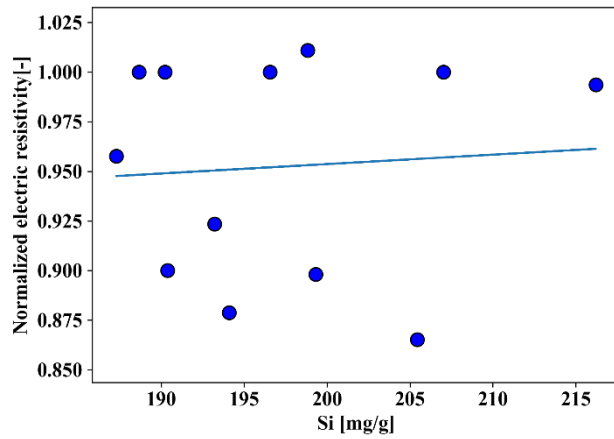


Figure 24 Relationship between Si concentration and normalized electric resistivity

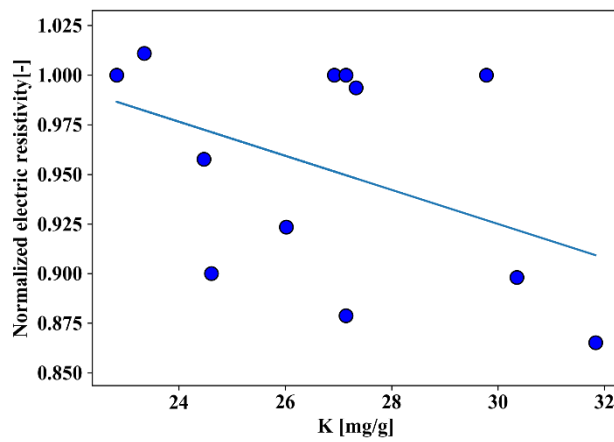


Figure 25 Relationship between K concentration and normalized electric resistivity

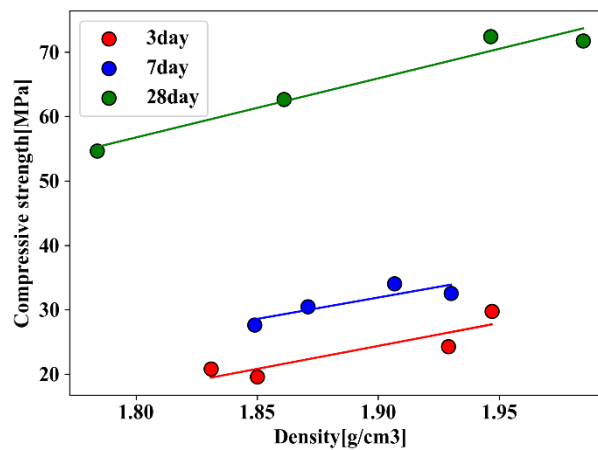


Figure 26 Relationship between density and compressive strength

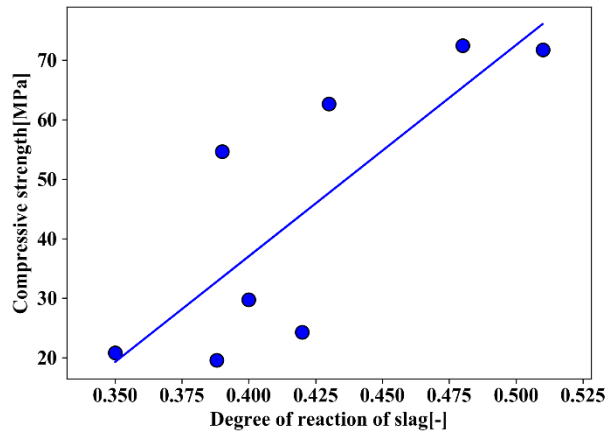


Figure 27 Relationship between degree of reaction of slag and compressive strength

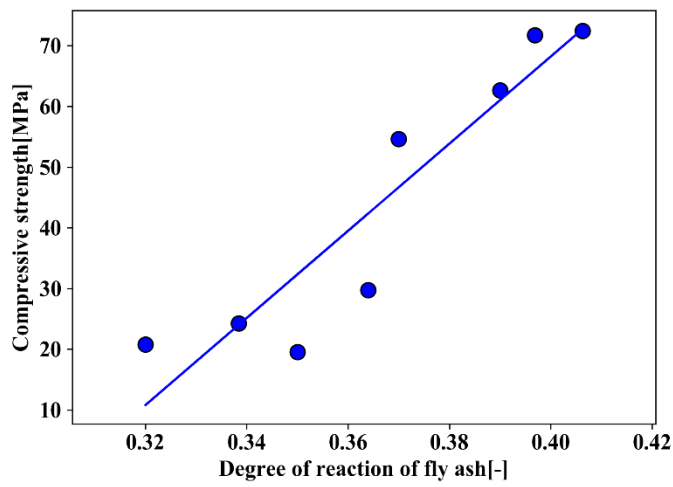


Figure 28 Relationship between degree of reaction of fly ash and compressive strength

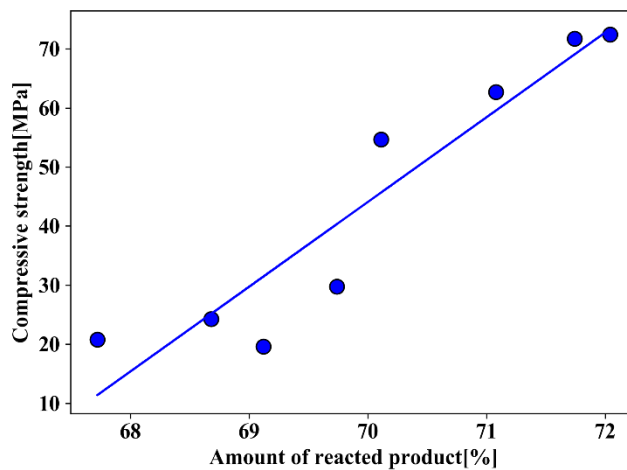
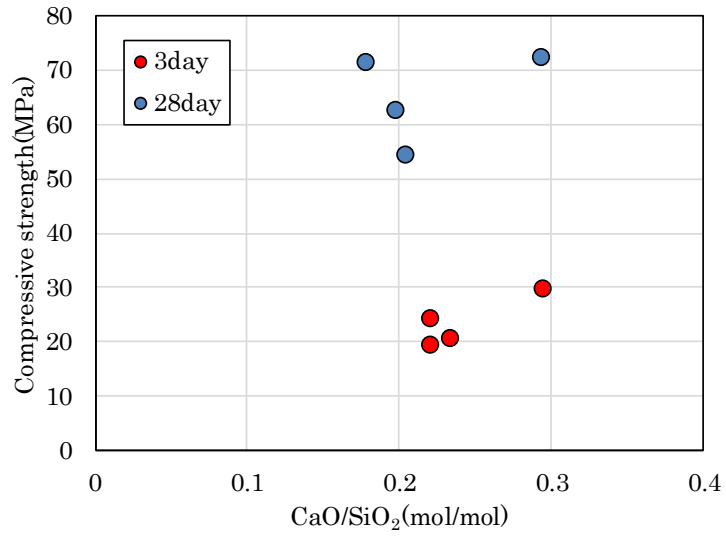


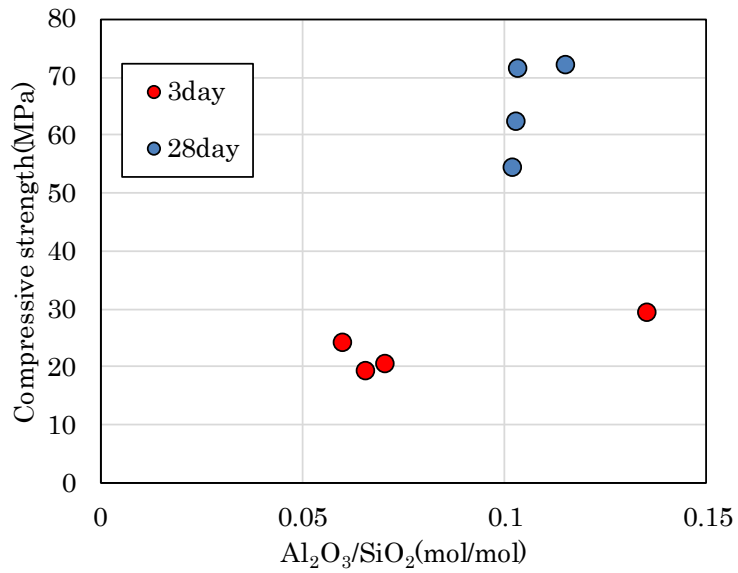
Figure 29 Relationship between amount of reacted product and compressive strength



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Figure 30 Relationship between CaO/SiO₂ and compressive strength

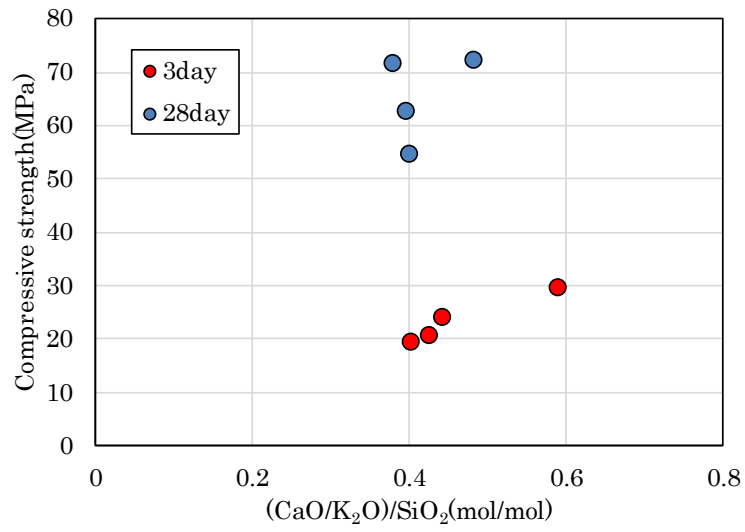


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Figure 31 Relationship between Al₂O₃/SiO₂ and compressive strength

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Figure 32 Relationship between (CaO+K₂O)/SiO₂ and compressive strength