



Title	Molecular dynamics study of evaporation induced by locally heated argon liquid
Author(s)	Tabe, Hirofumi; Hiramatsu, Kiryu; Kobayashi, Kazumichi; Fujii, Hiroyuki; Watanabe, Masao; Totani, Tsuyoshi
Citation	Applied Thermal Engineering, 212, 118472 <a href="https://doi.org/10.1016/j.applthermaleng.2022.118472">https://doi.org/10.1016/j.applthermaleng.2022.118472</a>
Issue Date	2022-07-25
Doc URL	<a href="http://hdl.handle.net/2115/85099">http://hdl.handle.net/2115/85099</a>
Rights	© 2022 The Author(s). Published by Elsevier Ltd.
Rights(URL)	<a href="https://creativecommons.org/licenses/by/4.0/">https://creativecommons.org/licenses/by/4.0/</a>
Type	article
File Information	1-s2.0-S1359431122004264-main.pdf



[Instructions for use](#)



## Research paper

## Molecular dynamics study of evaporation induced by locally heated argon liquid

Hirofumi Tabe, Kiryu Hiramatsu, Kazumichi Kobayashi\*, Hiroyuki Fujii, Masao Watanabe, Tsuyoshi Totani

Faculty of Engineering, Hokkaido University, Kita 13, Nishi 8, Kita-ku, Sapporo, Hokkaido, 060-8628, Japan

## ARTICLE INFO

## Keywords:

Evaporation  
Molecular dynamics  
Kinetic boundary condition  
Non-equilibrium

## ABSTRACT

In this study, we conducted molecular dynamics simulations of the evaporation of locally heated argon liquid to construct the kinetic boundary condition (KBC) for the evaporation. The KBC denotes the boundary condition of the Boltzmann equation, and the mass, momentum, and heat fluxes through the interface can be determined by solving the Boltzmann equation with the KBC. From the results, we established a method for constructing the KBC for the evaporation of locally heated argon liquid. Furthermore, we found that the velocity distribution of the KBC immediately after liquid heating becomes anisotropic, which means that the normal and tangential temperatures composed of outgoing molecules from the liquid phase to the gas phase take different values when the liquid interface is heated momentarily. From the present study, we can elucidate the mechanism of the occurrence of net evaporation mass flux due to the locally heated liquid film, e.g., the spot heating by infrared radiation.

## 1. Introduction

Recently, a new drying system has attracted attention from the drying industry. This drying system uses an infrared wavelength-selective emitter [1]. For example, for drying water, this emitter irradiates infrared radiation with a peak emissivity coincident with the O–H stretching absorption band. The irradiation of the emitter induces the O–H stretching vibration of water molecules located on a liquid surface, as shown in Fig. 1. Ashihara reported that the O–H stretching vibration energy is transferred to intermolecular vibrations, such as vibrational motions [2]. Through interactions with other molecules, some molecules gain sufficient kinetic energy to overcome the potential energy binding them in place. In this sense, such molecules have a high translational temperature, referred to as excitation. As a result, these molecules fly out of the liquid surface, i.e., evaporate. Therefore, this emitter allows the system to dry at a low temperature in furnace, which prevents flammable solvents from being ignited and reduces the heat damage generated in a solute by a high temperature. The effectiveness of this device has been confirmed as shown in [1,3,4]. In Refs. [1,3], a wavelength-selective emitter with the metamaterial structure of a metal–insulator–metal, i.e., the MIM emitter, was developed to decrease large heat losses. In these studies, it was shown that the drying rate of 2-propanol when using the MIM emitter was 2.1 times higher than that achieved with a conventional wavelength-selective emitter. Moreover, in Ref. [4], it was shown that wrinkles formed in polymer

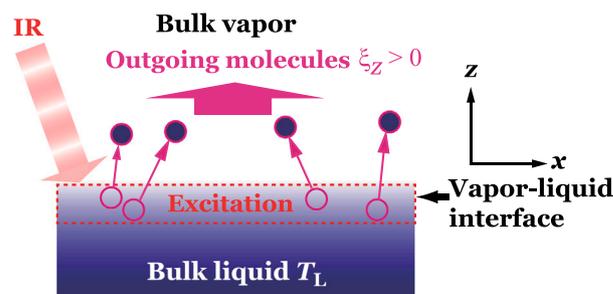


Fig. 1. Schematic of evaporation molecules induced by liquid surface excitation.

films during drying by hot-air flow but not during drying by infrared irradiation, and the detailed mechanism was discussed. However, a detailed analysis of drying efficiency based on molecular theory is required because this drying system induced by infrared radiation is considered as strong non-equilibrium evaporation in which a part of the liquid phase is instantaneously heated.

For this purpose, molecular gas dynamics analysis [5–7] is essential because the essence of evaporation and condensation phenomena is due to the non-equilibrium of molecular groups at the gas–liquid interface.

\* Corresponding author.

E-mail address: [kobakazu@eng.hokudai.ac.jp](mailto:kobakazu@eng.hokudai.ac.jp) (K. Kobayashi).

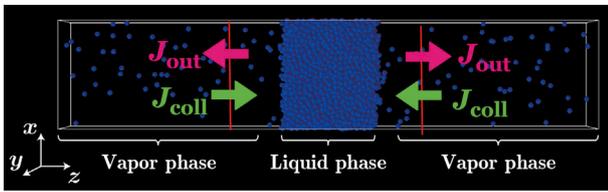


Fig. 2. Snapshot of MD simulation.

The velocity distribution function (VDF) of gas molecules is used in molecular gas dynamics analysis, where the governing equation of the VDF is the Boltzmann equation. Hence, the analysis of the Boltzmann equation is capable of treating non-equilibrium phenomena, such as evaporation and condensation. To solve the Boltzmann equation, a boundary condition called the kinetic boundary condition (KBC) is required at the vapor–liquid interface. The KBC is composed of molecules moving from the liquid phase to the vapor phase. The generalized form of the KBC [8–10] is written as

$$f_{\text{out}} = \frac{\rho_{\text{out}}}{(2\pi R)^{3/2} T_n \sqrt{T_n}} \exp\left(-\frac{\xi_x^2 + \xi_y^2}{2RT_n} - \frac{\xi_z^2}{2RT_t}\right), \text{ for } \xi_z > 0, \quad (1)$$

where  $f_{\text{out}}$  is the VDF of the outgoing molecules from the liquid phase to the vapor phase.  $f_{\text{out}}$  is the KBC of the vapor–liquid interface.  $R = k/m$  is the gas constant, where  $k$  is the Boltzmann constant and  $m$  is the mass of a molecule;  $\xi_x, \xi_y, \xi_z$  are the molecular velocities of  $x, y,$  and  $z$  directions;  $\rho_{\text{out}}$  is the vapor density; and  $T_n$  and  $T_t$  are the temperatures normal and tangential to the vapor–liquid interface, respectively.  $\rho_{\text{out}}, T_n,$  and  $T_t$  are also composed of outgoing molecules with a positive  $\xi_z$  velocity, as shown in Fig. 1. For example,  $T_t \neq T_n = T_0$  has been observed in a strong condensation case [8,11], where  $T_0$  is the temperature of the bulk liquid. In previous studies,  $T_t = T_n = T_0$  holds in a steady evaporation [10,12–16]. However, whether such a relationship holds in evaporation caused by a local temperature increase is unknown.

In this study, we conduct molecular dynamics (MD) simulations of the evaporation process owing to the instantaneous increase in the liquid surface temperature to modify the infrared irradiation. First, argon was targeted because it is monatomic and therefore easy to treat in MD simulations. MD is a useful tool for investigating evaporation and condensation phenomena, and various insights have been obtained from equilibrium and non-equilibrium MD calculations for single-component [17–21] and multi-component [22–25] systems using this method. However, no studies have investigated the details of molecular groups in evaporation phenomena caused by instantaneous heating at the gas–liquid interface. Therefore, our main objective is to construct the KBC for the evaporation of locally heated argon liquid using MD simulations; that is, we must identify three values: (i) the tangential temperature at the interface  $T_t$ , (ii) the normal temperature at the interface  $T_n$ , and (iii) the vapor density of outgoing molecules  $\rho_{\text{out}}$  immediately after excitation. In this study, we also propose a method for determining the KBC for the evaporation of locally heated argon liquid using MD simulations.

## 2. Molecular dynamics simulation

### 2.1. Equilibrium simulation

In this section, we describe a method for equilibrium MD simulations for argon. A system of 6000 argon molecules was considered in a simulation cell with dimensions  $L_x \times L_y \times L_z$  at a temperature  $T_0 = 85$  K, where  $L_x = 7.0$  nm,  $L_y = 7.0$  nm, and  $L_z = 35$  nm (see Fig. 2). We chose this temperature because it is close to the triple point temperature. Several studies on KBC have also been conducted using this temperature, e.g., see Refs. [8,12–14]. A vapor–liquid equilibrium

was realized between the triple point (83.8 K) and the critical point (150.7 K) [12]. The liquid phase was formed at the center of the  $z$ -direction. Periodic boundary conditions were applied in all three directions of the simulation cell. As an intermolecular pair potential for argon, we employed the 12-6 Lennard-Jones potential:

$$\phi(r) = 4\epsilon \left[ \left(\frac{\sigma}{r}\right)^{12} - \left(\frac{\sigma}{r}\right)^6 \right], \quad (2)$$

where  $r$  is the distance between two interacting particles, the particle diameter  $\sigma$  is 3.405 Å, and the potential depth  $\epsilon/k$  is 119.8 K ( $k$  is the Boltzmann constant). In general, because intermolecular interactions become weaker as the distance between two molecules increases, the cut-off radius was set as  $r_c = 1.5$  nm ( $4.4\sigma$ ) because it has been shown that  $r_c > 4.0\sigma$  leads to simulation results similar to those achieved when  $r_c = \infty$  [26–28]. Equations of motion were solved by using the leap–frog method.

Newton’s equations of motion for the 6000 molecules in the system were integrated using the leap–frog method with a time step of 5 fs. We performed the equilibrium simulation for 200 ns and sampled the configuration of molecules (the positions and the molecular velocities of each molecule) at each time step. This yielded the number of samples  $N_s = 40,000,000$ .

In MD simulations, an averaged density can be calculated as

$$\rho = \frac{1}{N_s \Delta V} \sum_{N_s} \sum_{i \in \Delta V} m^i, \quad (3)$$

where  $\Delta V$  is a volume element in the physical space and  $m^i$  is the mass of the  $i$ th molecule ( $m^i = m$  in this study).  $\sum_{i \in \Delta V}$  is the summation of the masses of the molecules contained in  $\Delta V$ .

The mass flux  $J$  was also calculated by counting the number of molecules passing through per unit area per unit time [13,29]. These values are defined as follows:

$$J = \frac{mN}{S \Delta t}, \quad (4)$$

where  $N$  is the number of sample molecules for each trajectory stated above, and  $S$  is the cross-section of the system. The equilibrium simulation produced the following averaged quantities: bulk vapor density  $\rho_v$ ; bulk liquid density  $\rho_\ell$ ; mass flux of outgoing molecules from the liquid phase to the vapor phase  $J_{\text{out}}$ , which is composed of the molecules of  $f_{\text{out}}$ ; and mass flux of molecules colliding onto the liquid phase  $J_{\text{coll}}$ , which is composed of the molecules of  $f_{\text{coll}}$ , where  $f_{\text{coll}}$  is the VDF with a negative velocity  $\xi_z < 0$  at the right-hand side vapor–liquid interface in Fig. 2 (For the left-hand side interface,  $J_{\text{out}}$  is composed of the molecules having negative  $\xi_z$ , and  $J_{\text{coll}}$  is composed of the molecules having positive  $\xi_z$ ). The net mass flux  $\dot{m}$  can be defined as follows:

$$\dot{m} = J_{\text{out}} - J_{\text{coll}}. \quad (5)$$

In the case of an equilibrium,  $J_{\text{out}} = J_{\text{coll}}$ , which leads to  $\dot{m} = 0$ . In the case of net evaporation,  $\dot{m}$  takes positive values because  $J_{\text{out}} > J_{\text{coll}}$ .

The spatial density distribution near the transition layer is shown in Fig. 3. In order to determine the approximate location of the center of the transition layer and its thickness, which is known to be asymmetric in practice [30,31], the following equation was used to estimate the thickness [29].

$$\rho(z) = \frac{\rho_v + \rho_\ell}{2} + \frac{\rho_v - \rho_\ell}{2} \tanh\left(\frac{z - Z_m}{0.455\delta}\right), \quad (6)$$

where  $Z_m$  is the center of the transition layer and  $\delta$  is the 10–90 thickness. In an equilibrium state at temperature  $T_0$ , the vapor density  $\rho_v$  becomes  $\rho_v^*$ , where  $\rho_v^*$  denotes the saturated vapor density at  $T_0$ , and  $\rho_\ell$  becomes  $\rho_\ell^*$ , where  $\rho_\ell^*$  denotes the liquid density in the equilibrium state at  $T_0$ . The values of  $Z_m$  and  $\delta$  were determined by the nonlinear least-squares method using the density distribution. The value of saturated vapor density is 4.86 kg/m<sup>3</sup> and the value of liquid density is 1388.44 kg/m<sup>3</sup> in this simulations. We confirmed that these values are in agreement with those of previous studies (i.e., Refs. [8,29]). A

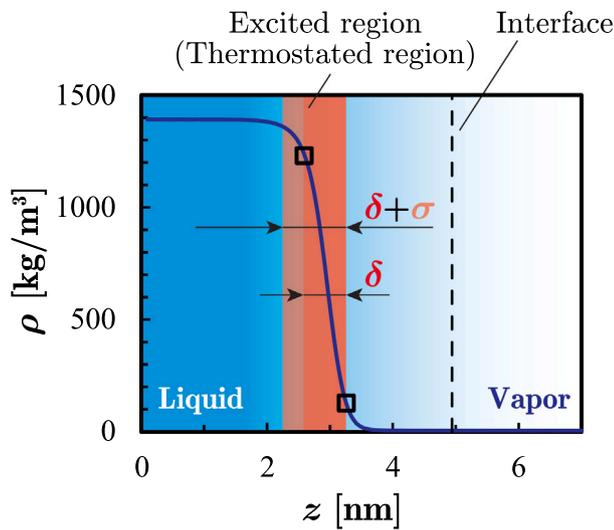


Fig. 3. Schematic of excited region at liquid surface, (a)  $\delta + \sigma$  and (b)  $\delta$ . The density profile is represented by Eq. (6). The squares indicate the edges of the transition layer. The dotted line indicates the interface position for imposing the KBC.

previous study demonstrated that for vapor–liquid equilibrium systems of Ar molecules, vapor can be treated as an ideal gas at temperatures below 100 K [8]. Therefore, the vapor in the initial state can be considered as an ideal gas in this study.

The position to impose the KBC is defined as  $z = Z_m + 3\delta$ . At this position, the influence of the intermolecular potential force composed of liquid molecules becomes sufficiently small to be ignored. This is why Eq. (1) does not include the effect of the liquid potential. The validity of this position has been discussed in our previous studies [13,29,32].

## 2.2. Excitation (thermostatting)

This section describes how to excite the liquid surface to simulate infrared irradiation drying. Essentially, there are two factors that lead to more evaporation: (i) higher excitation temperature, and (ii) a thicker excited region. Now, we explain the excited region and the method for exciting the liquid surface. Because it is difficult to know the detailed information of excitation experimentally, we investigate the evaporation process by changing the excited region and excitation temperature based on MD simulations.

In this study, we used two types of excited regions (see Fig. 3). Here, we consider that many molecules in the first layer at the liquid surface are excited, and we performed MD simulations for the following two cases. The difference is the thickness of the excited region. One is the 10–90 thickness  $\delta$  (8.85 Å) + the argon diameter  $\sigma$  (3.405 Å). The other is the 10–90 thickness  $\delta$ . The vapor-side edge of the excited region for each case coincides with the edge of the transition layer, as shown in Fig. 3.

To excite the region, we increased the molecular velocities of the argon molecules contained in these regions using velocity scaling [33]. In velocity scaling, the  $j$  component of the molecular velocity of the  $i$ th molecule  $\xi_j^i$  is transformed to  $\xi_j^{i'}$  through the following rule:

$$\xi_j^{i'} = \sqrt{\frac{T_{\text{exc}}}{T}} \xi_j^i \quad (j = x, y, z), \quad (7)$$

where  $T_{\text{exc}}$  is the target temperature and  $T$  is the temperature immediately before excitation. This corresponds to thermostatting the molecules in a certain region, which we call excitation in this study. Thus, we can instantly increase the temperature of the excited region to the target temperature  $T_{\text{exc}}$ . Hereafter, we refer to the target temperature  $T_{\text{exc}}$  as the excitation temperature.

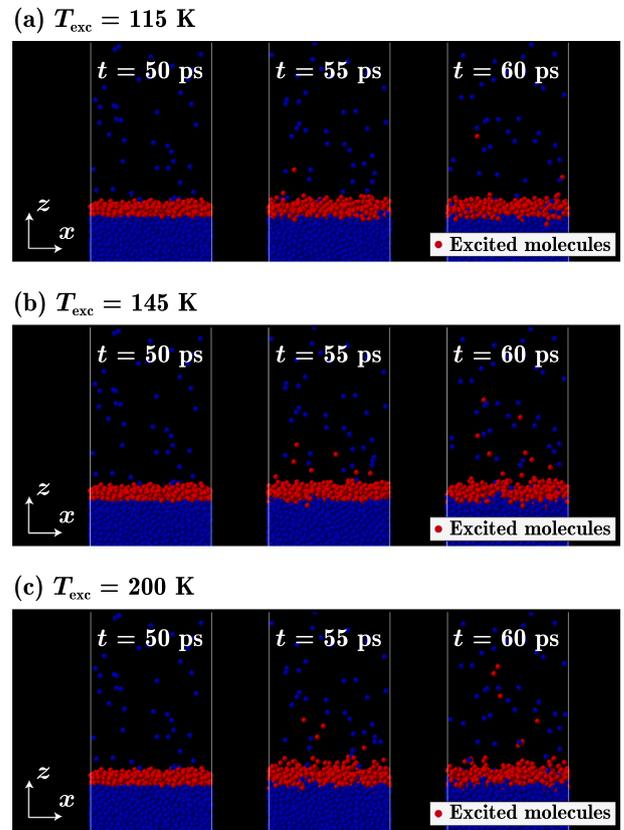


Fig. 4. Snapshots of MD simulation at the moment of excitation when  $T_{\text{exc}} = 115$  K, 145 K, and 200 K in the case of  $\delta + \sigma$ . Red molecules indicate excited molecules. Excitation is started at  $t = 50$  ps.

Here, we chose several excitation temperatures:  $T_{\text{exc}} = 95, 100, 105, 115, 130, 145,$  and  $200$  K. An excitation temperature of  $T_{\text{exc}} = 200$  K is still high, considering that the critical temperature of argon is 150.7 K.

## 3. Results

### 3.1. Net evaporation mass flux $\dot{m}$

We present the results of this study. MD simulations for excitation evaporation using 1000 initial conditions obtained by equilibrium simulations were conducted, and the averages of the 1000 MD simulations are reflected in the following results. We focus on the results of the excitation temperature  $T_{\text{exc}} = 115$  K, 145 K, and 200 K. Snapshots of the MD simulation at the time of excitation in the  $T_{\text{exc}} = 115$  K, 145 K, and 200 K cases are shown in Fig. 4. The red molecules denote the excitation molecules in the case of  $\delta + \sigma$ . When the time is  $t = 50$  ps, the molecules in the excited region are excited in accordance with Eq. (7). It can then be seen that the excited molecules interact with other molecules and fly toward the vapor region, i.e., evaporation occurs due to excitation.

Fig. 5 shows the temporal evolutions of  $J_{\text{out}}$  and  $J_{\text{coll}}$  for  $T_{\text{exc}} = 115$  K, 145 K, and 200 K, respectively. The dotted line in each figure is  $J_{\text{out}}^*$  or  $J_{\text{coll}}^*$ , where  $J_{\text{out}}^*$  and  $J_{\text{coll}}^*$  are the outgoing and colliding molecular mass fluxes at the equilibrium state, respectively. We can easily obtain  $J_{\text{out}}^* = J_{\text{coll}}^* = \rho_v^* \sqrt{RT_0/2\pi}$  from Eq. (1) in the equilibrium state ( $\rho_{\text{out}} = \rho_v^*$  and  $T_n = T_i = T_0$ ). From Figs. 5(a), (b) and (c), we can observe that  $J_{\text{out}}$  becomes larger than  $J_{\text{out}}^*$ , which leads to the evaporation of liquid molecules due to excitation for the cases of  $\delta + \sigma$  and  $\delta$ . As the excited region becomes thicker, the evaporation mass flux increases.

The peak times of  $J_{\text{out}}$  are shifted to the right from  $t = 50$  ps because excited molecules take time to reach the interface as shown

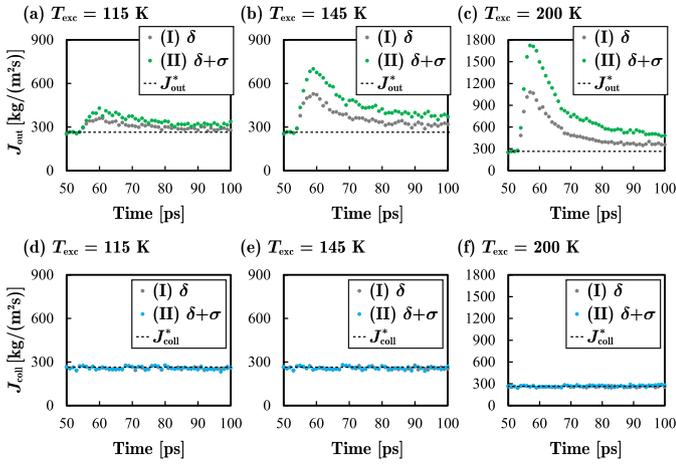


Fig. 5. Temporal evolutions of  $J_{\text{out}}$  and  $J_{\text{coll}}$ . (a) and (d);  $T_{\text{exc}} = 115$  K, (b) and (e);  $T_{\text{exc}} = 145$  K, (c) and (f);  $T_{\text{exc}} = 200$  K.

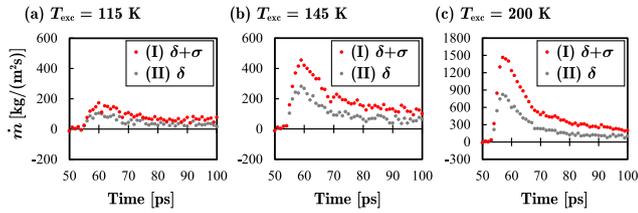


Fig. 6. Temporal evolutions of net evaporation mass flux  $\dot{m}$ . (a)  $T_{\text{exc}} = 115$  K, (b)  $T_{\text{exc}} = 145$  K, and (c)  $T_{\text{exc}} = 200$  K.

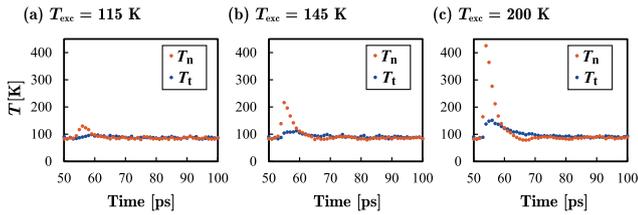


Fig. 7. Temporal evolutions of tangential temperature  $T_t$  and normal temperature  $T_n$ . The blue circles represent  $T_t$  and the orange circles represent  $T_n$ . (a)  $T_{\text{exc}} = 115$  K, (b)  $T_{\text{exc}} = 145$  K, and (c)  $T_{\text{exc}} = 200$  K.

in Figs. 5(a), (b), and (c). We can estimate the time for molecules to travel from the center of the excited region to the interface,  $\Delta t_f$ , by using the most probable speed of vapor molecules,  $v_p = \sqrt{2RT_{\text{exc}}}$ . When the excited region is  $\delta$ , the times are  $\Delta t_f = 9.19$  ps,  $\Delta t_f = 8.18$  ps, and  $\Delta t_f = 6.97$  ps for 115 K, 145 K, and 200 K, respectively; when the region is  $\delta + \sigma$ , the times are  $\Delta t_f = 9.96$  ps,  $\Delta t_f = 8.87$  ps, and  $\Delta t_f = 7.55$  ps. According to these results, the  $\Delta t_f$  values in both cases are almost the same at each peak time, as shown in Figs. 5(a), (b), and (c).

However, as shown in Figs. 5(d), (e), and (f), the values of  $J_{\text{coll}}$  are constant,  $J_{\text{coll}} = J_{\text{coll}}^*$ . These results indicate that the excited molecules do not interact with the molecules colliding from the vapor phase to the liquid phase, and that net evaporation occurs in the present MD simulations.

The temporal changes in the net evaporation mass flux  $\dot{m}$  in the evaporation simulation for  $T_{\text{exc}} = 115$  K, 145 K, and 200 K are plotted in Fig. 6 obtained from Eq. (5). After  $t = 50$  ps,  $\dot{m}$  increases in both cases due to excitation. The peak of  $\dot{m}$  becomes higher as the value of  $T_{\text{exc}}$  increases. Evaporation continues after 100 ps, after which the system returns to equilibrium.

Although there is a difference in the amount of evaporation, we will discuss the above results of  $\delta + \sigma$  in the following, as it was confirmed

that there is no difference in evaporation tendency between the excited regions  $\delta$  and  $\delta + \sigma$ .

### 3.2. Velocity distribution at the interface

In this section, we discuss the velocity distribution function of the outgoing molecules at the interface, namely, the kinetic boundary condition.

First, we focus on the tangential temperature  $T_t$  and the normal temperature  $T_n$  to make use of the KBC form in Eq. (1). These temperatures are obtained by the following equations:

$$\frac{1}{2}kT_t = \sum_{N_s} \frac{1}{2}m \frac{\xi_x^2 + \xi_y^2}{2N_s}, \quad (8)$$

$$\frac{1}{2}kT_n = \sum_{N_s} \frac{1}{2}m \frac{\xi_z^2}{N_s}, \quad (9)$$

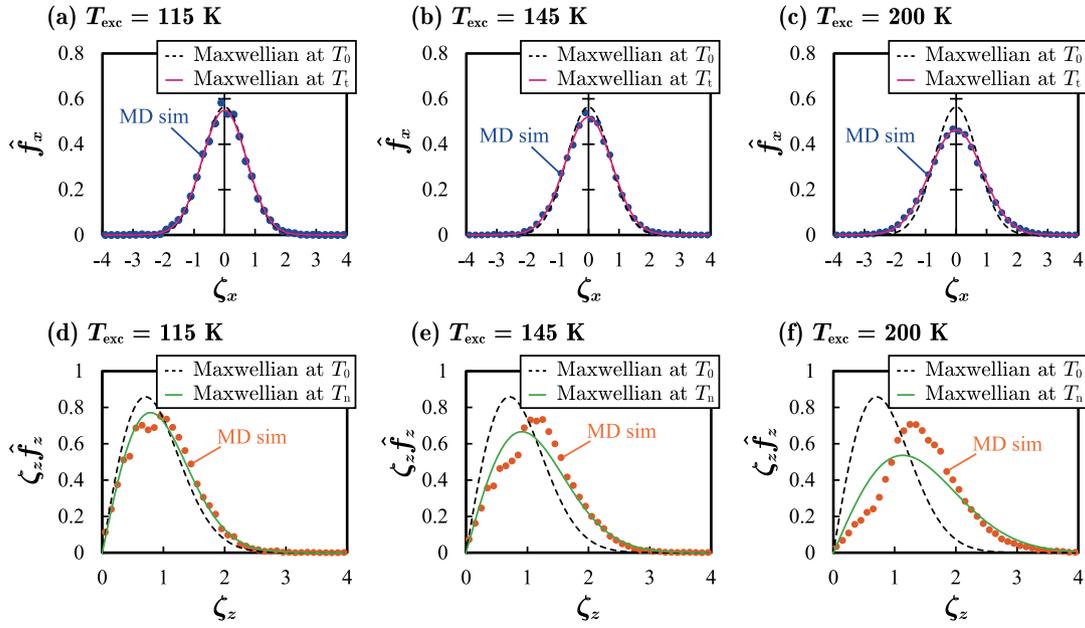
where the above equations are for molecules outgoing from liquid to vapor, e.g., in Fig. 1, the equation consists of molecules with positive velocities  $\xi_z$ . Fig. 7 shows the temporal evolutions of  $T_t$  and  $T_n$  for each excitation temperature and the excited region  $\delta + \sigma$ . In the case of  $T_{\text{exc}} = 115$  K,  $T_n$  is greater than  $T_0$  for  $52 \text{ ps} \leq t \leq 60 \text{ ps}$ , whereas  $T_t$  remains approximately 85 K. In contrast, in the cases of  $T_{\text{exc}} = 145$  K and 200 K,  $T_n$  has a higher peak and  $T_t$  has a small peak after a short delay. These temperature differences lead to the anisotropy of the VDF at the vapor–liquid interface.

Here, we take the time average of  $T_t$  and  $T_n$  for  $52 \text{ ps} \leq t \leq 60 \text{ ps}$  to treat the pulsate changes in the temperatures. Using these temperatures, we construct the KBC, given by Eq. (1), for each excitation temperature.

Fig. 8 shows the velocity distribution function of  $\hat{f}_{\text{out}} = \hat{f}_x \hat{f}_y \hat{f}_z$ , where  $\hat{\cdot}$  denotes the normalization, and  $\hat{f}_j$  ( $j = x, y, z$ ) denotes the normalized VDF for the  $j$ -component, where  $\hat{f}_x = \hat{f}_y$  in this study. We plot the time-averaged velocity distributions for  $52 \text{ ps} \leq t \leq 60 \text{ ps}$  of the outgoing molecules at the interface, which were obtained by the MD simulations. The time-averaged velocity distributions for Figs. 8(a) and (d)  $T_{\text{exc}} = 115$  K, Figs. 8(b) and (e)  $T_{\text{exc}} = 145$  K, and Figs. 8(c) and (f)  $T_{\text{exc}} = 200$  K are made up of 8920, 13,234, and 30,706 molecules, respectively. Here, because the KBCs and time-averaged velocity distributions are normalized, their velocity distribution functions indicate the probability of existence of the molecule. The abscissa  $\zeta_j = \xi_j / \sqrt{2RT_0}$  is the  $j$  component of the normalized molecular velocity, where  $T_0 = 85$  K.

As shown in Fig. 8(a), the velocity distribution for the tangential direction  $\hat{f}_x$  agrees with a solid curve, the normalized Maxwellian  $\sqrt{T_0/(T_t\pi)} \exp(-\zeta_x^2 T_0/T_t)$  with  $T_t = 89.6$  K for  $T_{\text{exc}} = 115$  K. For the cases of  $T_{\text{exc}} = 145$  K and 200 K in Figs. 8(b) and (c),  $\hat{f}_x$  also agrees with a normalized Maxwellian with  $T_t = 100.3$  K and 126.5 K. We can say that the outgoing molecules have a velocity distribution in the tangential direction at  $T_0 = 85$  K in the case of low excitation temperature because  $T_t$  is nearly equal to  $T_0$ .

From Fig. 8(d), the velocity distribution function for the normal direction  $\hat{f}_z$  can be almost fitted by the normalized Maxwellian  $2T_0/T_n \zeta_z \exp(-\zeta_z^2 T_0/T_n)$  with  $T_n = 105.3$  K for  $T_{\text{exc}} = 115$  K. The value of  $T_n = 105.3$  K is much larger than the tangential temperature  $T_t = 89.6$  K (see Fig. 8(a)). In the cases of  $T_{\text{exc}} = 145$  K and 200 K (Figs. 8(e) and (f)),  $\hat{f}_z$  is slightly different from the normalized Maxwellian with  $T_n = 141.1$  K or 217.5 K. The values of  $T_n$  are also larger than the tangential temperatures  $T_t = 100.3$  K and 126.5 K. We confirm that the normal temperature takes the approximate value of the excitation temperature. For the VDF in the normal direction, an almost Maxwell distribution with an excitation temperature is observed in the MD simulation of a heated ultra-thin liquid layer [34]. Our results agree with the previous MD simulation except for the extremely high excitation temperature having the deviation from the Maxwellian, as shown in Fig. 8(f).



**Fig. 8.** Normalized velocity distribution at the interface. (a)  $\hat{f}_x$ ,  $T_{\text{exc}} = 115$  K ( $T_t = 89.6$  K,  $T_0 = 85$  K); (b)  $\hat{f}_x$ ,  $T_{\text{exc}} = 145$  K ( $T_t = 100.3$  K,  $T_0 = 85$  K); (c)  $\hat{f}_x$ ,  $T_{\text{exc}} = 200$  K ( $T_t = 126.5$  K,  $T_0 = 85$  K); (d)  $\hat{f}_z$ ,  $T_{\text{exc}} = 115$  K ( $T_n = 105.3$  K,  $T_0 = 85$  K); (e)  $\hat{f}_z$ ,  $T_{\text{exc}} = 145$  K ( $T_n = 141.1$  K,  $T_0 = 85$  K); (f)  $\hat{f}_z$ ,  $T_{\text{exc}} = 200$  K ( $T_n = 217.5$  K,  $T_0 = 85$  K).

The anisotropy of VDF at the KBC is thought that by increasing the temperature of the liquid, the molecules with fast positive velocity in the  $z$ -direction, i.e., the normal direction to the interface from the liquid phase to the vapor phase, will evaporate and pass through the interface position near the density transition layer where the VDF is measured. In previous studies, it was shown that the molecules having fast positive velocity in the normal direction can evaporate, that is, the evaporation probability increases with the increase in the normal direction velocity [29,35,36]. On the other hand, the molecules with slow positive velocities in the  $z$ -direction are less likely to evaporate and will take longer to pass through the interface where the VDF is measured. In addition, the molecules with slow positive velocities have more time to interfere with the liquid phase, so they tend to lose the effect of warming the liquid film. This effect would result in a smaller number of molecules with low  $z$ -direction velocity being measured, compared to molecules with relatively high  $z$ -direction velocity in the VDF. The detailed mechanism of the deviation will be a focus of our future work.

### 3.3. Excitation temperature dependence of $T_t$ , $T_n$ , and $\rho_{\text{out}}$

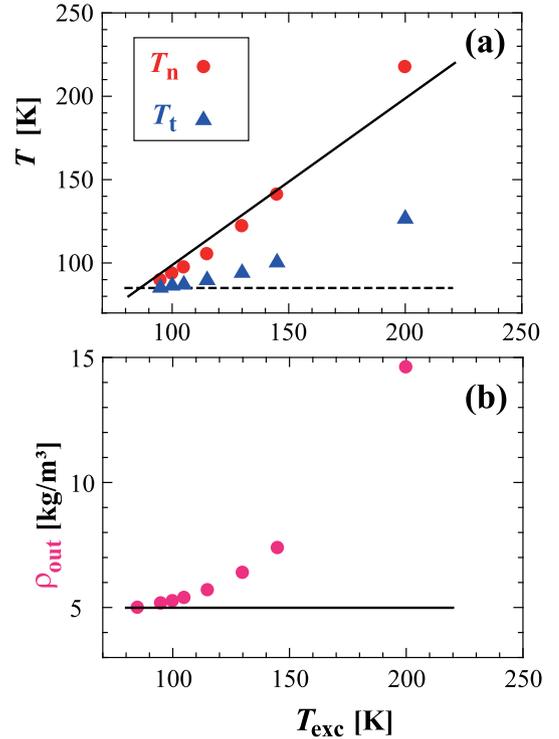
Fig. 9 shows  $T_t$ ,  $T_n$ , and  $\rho_{\text{out}}$  as functions of  $T_{\text{exc}}$ . These values are the time-averaged values for  $52 \text{ ps} \leq t \leq 60 \text{ ps}$ , which show the values immediately after the excitation of the liquid surface. We can obtain the vapor density of outgoing molecules  $\rho_{\text{out}}$ .  $f_{\text{out}}$ ,  $\rho_{\text{out}}$ , and  $J_{\text{out}}$  have the following relation:

$$J_{\text{out}} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_0^{\infty} \xi_z f_{\text{out}} d\xi_z d\xi_x d\xi_y = \rho_{\text{out}} \sqrt{\frac{RT_n}{2\pi}}. \quad (10)$$

From the above equation, we can obtain the following equation for  $\rho_{\text{out}}$  and calculate its value using  $J_{\text{out}}$  and  $T_n$ :

$$\rho_{\text{out}} = \frac{J_{\text{out}}}{\sqrt{RT_n/2\pi}}. \quad (11)$$

Note that the error in this procedure increases as the excitation temperature increases, because the deviation from the Maxwellian at  $T_n$  becomes larger when the excitation temperature is higher. Fig. 9(a) shows  $T_t$  and  $T_n$ . The solid line denotes  $T_n = T_{\text{exc}}$ , and the dotted line in Fig. 9(a) denotes  $T_0 = 85$  K. As shown in Fig. 9(a),  $T_n$  increases



**Fig. 9.** (a)  $T_n$  and  $T_t$  composed of evaporating molecules as a function of  $T_{\text{exc}}$ ; (b)  $\rho_{\text{out}}$  composed of evaporation molecules as a function of  $T_{\text{exc}}$ .

with  $T_{\text{exc}}$ , and the value  $T_n$  is almost the same as  $T_{\text{exc}}$ , which leads to  $T_n \approx T_{\text{exc}}$ . In contrast, for  $T_t$ , the value is slightly higher than the initial value  $T_0$  in the case of high excitation temperature. However, for low excitation temperature (approximately  $T_{\text{exc}} < 100$  K),  $T_t \approx T_0$ .

Fig. 9(b) shows  $\rho_{\text{out}}$ . The solid line denotes the saturated vapor density at  $T_0$ . As shown in the figure, the value of  $\rho_{\text{out}}$  increases with an increase in  $T_{\text{exc}}$ . However, when  $T_{\text{exc}}$  takes a small value, we can assume that  $\rho_{\text{out}} \approx \rho_v^*(T_0)$ .

We now obtain all three values: (i) the tangential temperature at the interface  $T_t$ , (ii) the normal temperature at the interface  $T_n$ , and (iii) the vapor density of outgoing molecules  $\rho_{out}$ . In addition, we confirm that the outgoing molecules almost leave the interface with the KBC form of Eq. (1). Therefore, KBC can be constructed using Eq. (1) with these values. From the above discussion, we can rewrite the KBC as

$$f_{out} = \frac{\rho_{out}}{(2\pi R)^{3/2} T_t \sqrt{T_{exc}}} \exp\left(-\frac{\xi_x^2 + \xi_y^2}{2RT_t} - \frac{\xi_z^2}{2RT_{exc}}\right), \quad (12)$$

where  $T_n = T_{exc}$ ,  $\rho_{out}$  and  $T_t$  are functions of  $T_{exc}$ , as shown in Fig. 9. Moreover, we can obtain the colliding mass flux as  $J_{coll} = \rho_v^*(T_0) \sqrt{RT_{exc}/2\pi}$  as shown in Fig. 5. Using  $J_{out}$  and  $J_{coll}$ , the following mass flux can be obtained immediately after excitation:

$$\dot{m} = \rho_{out} \sqrt{\frac{RT_0}{2\pi}} \left( \sqrt{\frac{T_{exc}}{T_0}} - 1 \right). \quad (13)$$

From the above equation, we can estimate the net mass flux  $\dot{m}$  immediately after excitation of the liquid surface in the case of low excitation temperature.

#### 4. Conclusion

In this study, we conducted MD simulations of the evaporation of locally heated argon liquid to construct the kinetic boundary conditions for the evaporation. We also proposed a method for constructing the KBC for the evaporation of locally heated argon liquid. From the results, we found that the velocity distribution of the KBC becomes anisotropic, which means that the tangential and normal temperatures composed of outgoing molecules from the liquid phase to the gas phase take different values when the liquid interface is heated momentarily. The normal temperature  $T_n$  agrees with the excitation temperature  $T_{exc}$  and the tangential temperature  $T_t$  is almost the same as the initial temperature  $T_0$  in the case in which the difference between  $T_{exc}$  and  $T_0$  is not very large.

From this study, we were able to demonstrate the non-equilibrium nature of the evaporation phenomenon induced on the surface of a liquid with an instantaneous temperature increase by studying the behavior of the molecules. As a result, a boundary condition for the Boltzmann equation for this problem was proposed. This is a novelty in this research. By using the proposed boundary condition, the evaporation rate of the instantaneously excited interfaces can be obtained through the Boltzmann equation analysis. In future work, we will conduct the evaporation with polyatomic molecules [37], e.g., water molecules, to simulate the actual drying phenomenon. In addition, the evaporation of a multi-component system [32,38–41] is an important topic. It has been found that the composition of molecules at the liquid or gas–liquid interface is important for multi-component evaporation [42]. Examining the composition of such interfaces and the detailed behavior of evaporated molecules are two of our future research themes.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### Acknowledgments

This work was supported by JSPS, Japan KAKENHI Grant Number JP 19H02074 to T.T., 20K04277 to K.K., and f3 Engineering Education and Research Center, Faculty of Engineering, Hokkaido University to K.K., and JST, PRESTO, Japan Grant Number JPMJPR21O3, Japan to K.K.

#### References

- [1] T. Totani, A. Sakurai, T.D. Dao, T. Nagao, Y. Kondo, Application of the wavelength selective emitter with the metamaterial of a metal-insulator-metal to an infrared ray drying furnace, in: International Heat Transfer Conference Digital Library, Begel House Inc. 2018.
- [2] S. Ashihara, Time-resolved observation of molecular dynamics in liquid water by mid-infrared nonlinear spectroscopy (in Japanese), *Kougaku* 40 (8) (2011) 409–414.
- [3] T. Totani, A. Sakurai, T. Nagao, Y. Kondo, Increase of drying rate by wavelength-selective emitter with metamaterial structures in infrared ray drying, in: Extended Abstracts of the Second Pacific Rim Thermal Engineering Conference, 2019.
- [4] T. Kinnan, Y. Kondo, M. Aoki, S. Inasawa, How do drying methods affect quality of films? Drying of polymer solutions under hot-air flow or infrared heating with comparable evaporation rates, *Dry. Technol.* (2020) 1–12.
- [5] G.A. Bird, *Molecular Gas Dynamics and the Direct Simulation of Gas Flows*, Clarendon press Oxford, 1994.
- [6] C. Cercignani, *Rarefied Gas Dynamics: From Basic Concepts to Actual Calculations*, Cambridge University Press, 2000.
- [7] Y. Sone, *Molecular Gas Dynamics*, Birkhäuser, 2007.
- [8] T. Ishiyama, T. Yano, S. Fujikawa, Kinetic boundary condition at a vapor-liquid interface, *Phys. Rev. Lett.* 95 (2005) 084504.
- [9] A. Frezzotti, Boundary conditions at the vapor-liquid interface, *Phys. Fluids* 23 (3) (2011) 030609.
- [10] M. Kon, K. Kobayashi, M. Watanabe, Method of determining kinetic boundary conditions in net evaporation/condensation, *Phys. Fluids* 26 (7) (2014) 072003.
- [11] A. Tokunaga, T. Tsuruta, Nonequilibrium molecular dynamics study on energy accommodation coefficient on condensing liquid surface-molecular boundary conditions for heat and mass transfer, *Phys. Fluids* 32 (11) (2020) 112011.
- [12] T. Ishiyama, T. Yano, S. Fujikawa, Molecular dynamics study of kinetic boundary condition at an interface between argon vapor and its condensed phase, *Phys. Fluids* 16 (8) (2004) 2899–2906.
- [13] K. Kobayashi, K. Hori, M. Kon, K. Sasaki, M. Watanabe, Molecular dynamics study on evaporation and reflection of monatomic molecules to construct kinetic boundary condition in vapor-liquid equilibria, *Heat Mass Trans.* 52 (9) (2016) 1851–1859.
- [14] M. Kon, K. Kobayashi, M. Watanabe, Liquid temperature dependence of kinetic boundary condition at vapor-liquid interface, *Int. J. Heat Mass Trans.* (ISSN: 0017-9310) 99 (2016) 317–326.
- [15] M. Kon, K. Kobayashi, M. Watanabe, Kinetic boundary condition in vapor-liquid two-phase system during unsteady net evaporation/condensation, *Eur. J. Mech. - B/Fluids* (ISSN: 0997-7546) 64 (2017) 81–92, Special Issue on Non-equilibrium Gas Flows.
- [16] V.V. Zhakhovskiy, A.P. Kryukov, V.Y. Levashov, I.N. Shishkova, S.I. Anisimov, Mass and heat transfer between evaporation and condensation surfaces: Atomistic simulation and solution of Boltzmann kinetic equation, *Proc. Natl. Acad. Sci.* 116 (37) (2019) 18209–18217.
- [17] C. Braga, J. Muscatello, G. Lau, E.A. Müller, G. Jackson, Nonequilibrium study of the intrinsic free-energy profile across a liquid-vapour interface, *J. Chem. Phys.* 144 (4) (2016) 044703.
- [18] A. Lofji, J. Vrabc, J. Fischer, Evaporation from a free liquid surface, *Int. J. Heat Mass Trans.* 73 (2014) 303–317.
- [19] M. Heinen, J. Vrabc, Evaporation sampled by stationary molecular dynamics simulation, *J. Chem. Phys.* 151 (4) (2019) 044704.
- [20] Z. Liang, A. Chandra, E. Bird, P. Keblinski, A molecular dynamics study of transient evaporation and condensation, *Int. J. Heat Mass Trans.* (ISSN: 0017-9310) 149 (2020) 119152.
- [21] B. Ma, K. Guye, B. Dogruoz, D. Agonafer, Molecular dynamics simulations of thin-film evaporation: The influence of interfacial thermal resistance on a graphene-coated heated silicon substrate, *Appl. Therm. Eng.* (ISSN: 1359-4311) 195 (2021) 117142.
- [22] V. Baidakov, S. Protsenko, Molecular-dynamics simulation of relaxation processes at liquid–gas interfaces in single-and two-component lennard-jones systems, *Coll. J.* 81 (5) (2019) 491–500.
- [23] V.G. Baidakov, S.P. Protsenko, V.M. Bryukhanov, Relaxation processes at liquid-gas interfaces in one-and two-component lennard-jones systems: Molecular dynamics simulation, *Fluid Ph. Equilib.* 481 (2019) 1–14.
- [24] S. Cai, Q. Li, C. Liu, L. Zhang, Evaporation of Ar/Kr mixtures on platinum surface: a molecular dynamics study, *Phys. Chem. Chem. Phys.* 22 (28) (2020) 16157–16164.
- [25] S. Stephan, D. Schaefer, K. Langenbach, H. Hasse, Mass transfer through vapour-liquid interfaces: A molecular dynamics simulation study, *Mol. Phys.* 119 (3) (2021) e1810798.
- [26] C. Holcomb, P. Clancy, S. Thompson, J. Zollweg, A critical study of simulations of the lennard-jones liquid-vapor interface, *Fluid Ph. Equilib.* 75 (1992) 185–196.
- [27] A. Trokhymchuk, J. Alejandre, Computer simulations of liquid/vapor interface in lennard-jones fluids: Some questions and answers, *J. Chem. Phys.* 111 (18) (1999) 8510–8523.

- [28] H. Yaguchi, T. Yano, S. Fujikawa, Molecular dynamics study of vapor-liquid equilibrium state of an argon nanodroplet and its vapor, *J. Fluid Sci. Tech.* 5 (2) (2010) 180–191.
- [29] H. Tabe, K. Kobayashi, H. Fujii, M. Watanabe, Molecular dynamics study on characteristics of reflection and condensation molecules at vapor-liquid equilibrium state, *PLoS One* 16 (3) (2021) e0248660.
- [30] B.Q. Lu, R. Evans, M. Telo da Gama, The form of the density profile at a liquid-gas interface: Dependence on the intermolecular potential, *Mol. Phys.* 55 (6) (1985) 1319–1338.
- [31] S. Stephan, J. Liu, K. Langenbach, W.G. Chapman, H. Hasse, Vapor- liquid interface of the lennard-jones truncated and shifted fluid: Comparison of molecular simulation, density gradient theory, and density functional theory, *J. Phys. Chem. C* 122 (43) (2018) 24705–24715.
- [32] K. Ohashi, K. Kobayashi, H. Fujii, M. Watanabe, Evaporation coefficient and condensation coefficient of vapor under high gas pressure conditions, *Sci. Rep.* 10 (1) (2020) 1–10.
- [33] M.P. Allen, D.J. Tildesley, *Computer Simulation of Liquids*, Oxford, 1987.
- [34] P. Yi, D. Poulikakos, J. Walther, G. Yadigaroglu, Molecular dynamics simulation of vaporization of an ultra-thin liquid argon layer on a surface, *Int. J. Heat Mass Trans.* (ISSN: 0017-9310) 45 (10) (2002) 2087–2100.
- [35] T. Tsuruta, H. Tanaka, T. Masuoka, Condensation/evaporation coefficient and velocity distributions at liquid-vapor interface, *Int. J. Heat Mass Trans.* 42 (22) (1999) 4107–4116.
- [36] T. Tsuruta, G. Nagayama, Molecular dynamics studies on the condensation coefficient of water, *J. Phys. Chem. B* 108 (5) (2004) 1736–1743.
- [37] S. Busuioc, L. Gibelli, Mean-field kinetic theory approach to langmuir evaporation of polyatomic liquids, *Phys. Fluids* 32 (9) (2020) 093314.
- [38] K. Kobayashi, K. Sasaki, M. Kon, H. Fujii, M. Watanabe, Kinetic boundary conditions for vapor-gas binary mixture, *Microfluid Nanofluid* 21 (3) (2017) 53.
- [39] A. Frezzotti, L. Gibelli, D.A. Lockerby, J.E. Sprittles, Mean-field kinetic theory approach to evaporation of a binary liquid into vacuum, *Phys. Rev. Fluids* 3 (2018) 054001.
- [40] K. Ohashi, K. Kobayashi, H. Fujii, M. Watanabe, Mean-field kinetic theory analysis of vapor flow between evaporating and condensing interfaces in the presence of non-condensable gas molecules, *Phys. Fluids* 33 (12) (2021) 122017.
- [41] H. Tabe, K. Kobayashi, H. Fujii, M. Watanabe, Molecular dynamics simulation of evaporation coefficient of vapor molecules during steady net evaporation in binary mixture system, *Int. J. Heat Mass Trans.* 188 (2022) 122663.
- [42] S. Stephan, H. Hasse, Enrichment at vapour-liquid interfaces of mixtures: establishing a link between nanoscopic and macroscopic properties, *Int. Rev. Phys. Chem.* 39 (3) (2020) 319–349.