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## Supporting Information

# Structure Frustration Enables Thermal History-Dependent Responsive Behavior in Self-Healing Hydrogels

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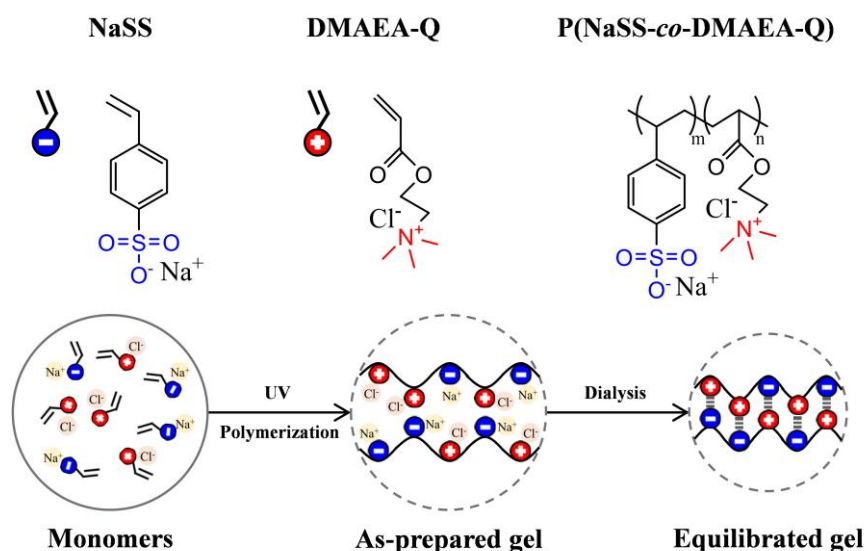
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## 1. Supporting results

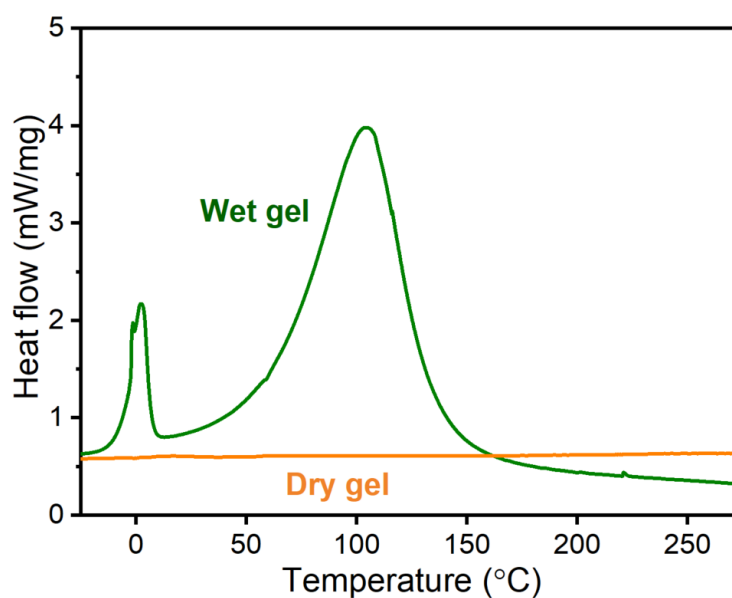
### 1) Chemical structure of the monomers and of the hydrogels

A recent work<sup>1</sup> studied the reactivity ratios of NaSS ( $r_1 = 1.26$ ) and DMAEA-Q ( $r_2 = 0.58$ ) in water and analyzed the instantaneous number-average sequence length of the NaSS monomer,  $N_{\text{NaSS}}$ , and DMAEA-Q monomer,  $N_{\text{DMAEA-Q}}$ , with the total monomer conversion  $p$  according to the Mayo–Lewis theory. At total monomer conversion  $p = 0$ , the determination of  $N_{\text{NaSS}}$  is 2.4 and  $N_{\text{DMAEA-Q}}$  is 1.5. This can be understood that, as an average of the incorporation to the growing polymer chains, a sequence of three NaSS molecules follows by two DMAEA-Q molecules. At  $p = 0.7$ , then  $N_{\text{NaSS}} = 1.4$  and  $N_{\text{DMAEA-Q}} = 2.7$ , a sequence of one NaSS molecule would follow by three DMAEA-Q molecules. At higher conversion ( $p > 0.9$ ), the polymer chains will grow with a block sequence of DMAEA-Q molecules. So, NaSS rich segments formed at the beginning of polymerization and DMAEA-Q-rich segments formed at the end of polymerization.



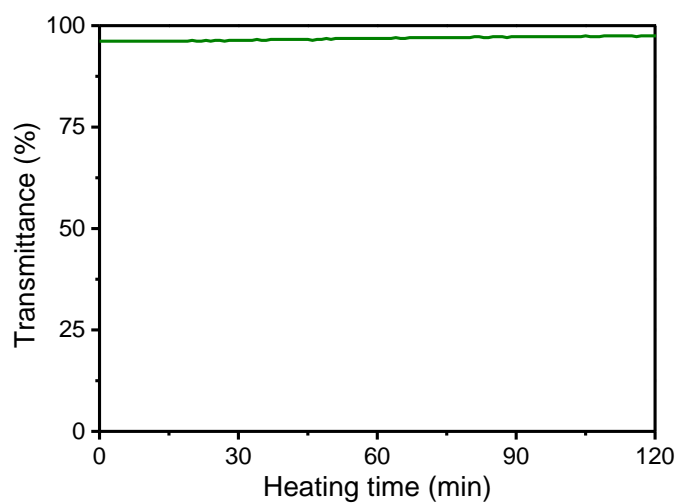
**Fig. S1.** Schematic illustration of the chemical structure of the monomers NaSS and DMAEA-Q, and the P(NaSS-co-DMAEA-Q) hydrogel.

## 2) Structure analysis

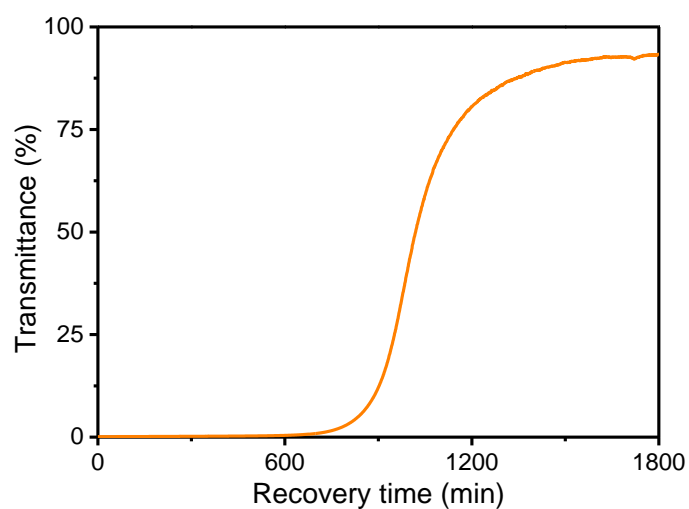


**Fig. S2.** Differential scanning calorimetry (DSC) scanning for dry and wet P(NaSS-co-DMAEA-Q) samples performed at a heating rate of 10 °C/min from -50 °C to 275 °C. The two peaks (around 0 °C and 100 °C) in the DSC curve of wet sample are assigned to the melting point and boiling point of water in the polymer, respectively. No thermal melting peak from the ion complex structures appears in DSC curves either for the hydrogels or for the dried sample. This result indicates that the PA gel is amorphous with no crystalline structure.

### 3) Transmittance change of the PA gel during heating and recovery

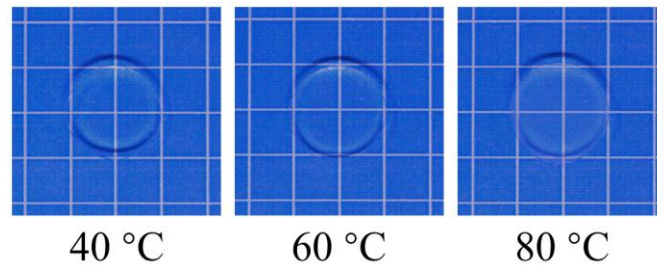


**Fig. S3.** Transmittance of the gel during heating at  $T_L = 80\text{ }^\circ\text{C}$  for  $t_L = 2\text{ h}$ .



**Fig. S4.** Transmittance of the gel during recovery at  $T_F = 25\text{ }^\circ\text{C}$ . The turbid gel was obtained by quenching the gel to  $25\text{ }^\circ\text{C}$  after heating at  $T_L = 80\text{ }^\circ\text{C}$  for  $t_L = 2\text{ h}$ .

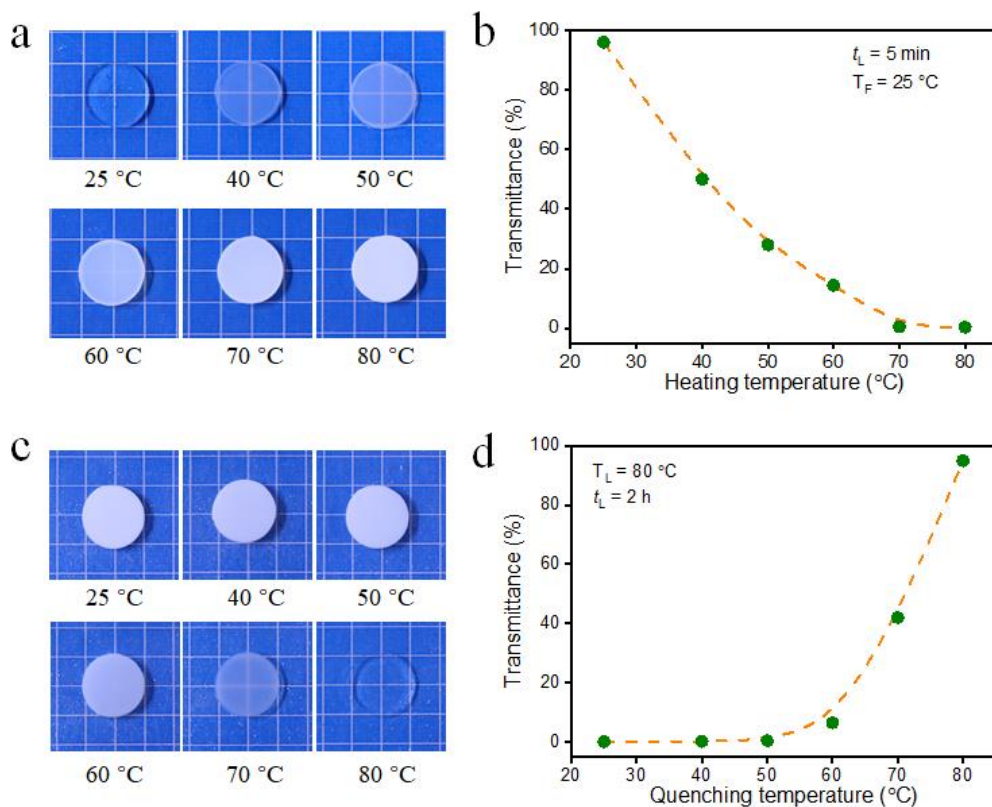
#### 4) Small size change during thermal response



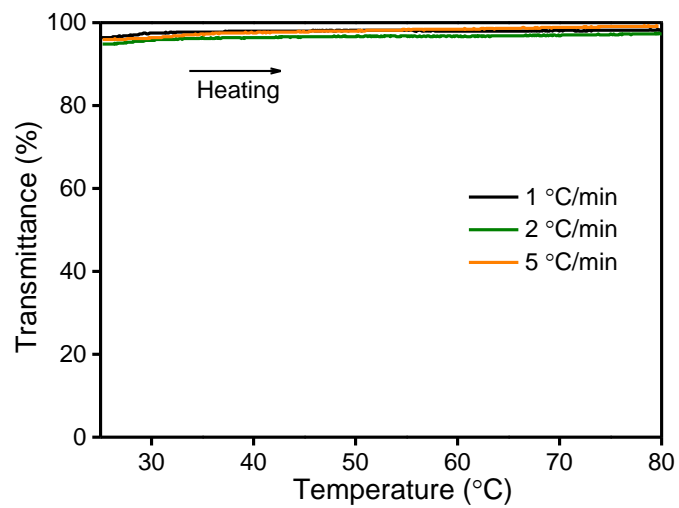
**Fig. S5.** Optical images of a PA gel at different heating temperatures for  $T_L = 2$  h.

Background lattices, 5 mm.

5) Effect of heating temperature and cooling temperatures on transmittance of PA gels at cooling



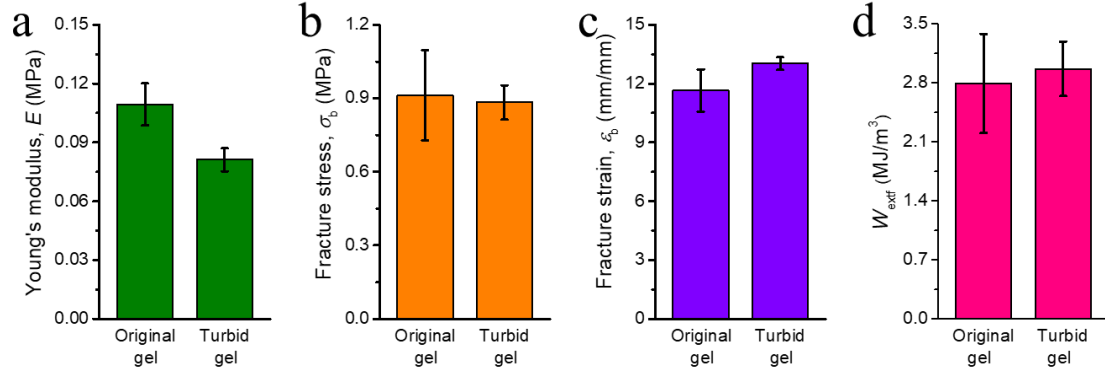
**Fig. S6.** Tunable transparency of PA gels at cooling by tuning  $T_L$  and  $T_F$ . (a) Optical images and (b) transmittance change of PA gels with different heating temperatures  $T_L$  for fixed  $t_L = 5$  min and  $T_F = 25$  °C. (c) Optical images and (d) transmittance change of PA gels with different  $T_F$  for fixed  $T_L = 80$  °C and  $t_L = 5$  min. The optical images were taken after cooling the temperature to  $T_F$  for 1 min. The temperatures in (a) and (c) are  $T_L$  and  $T_F$ , respectively. Background lattices, 5 mm.



**Fig. S7.** Transmittance of the original gel during heating from 25 to 80 °C with different heating rates.



## 6) Comparison of mechanical performances of turbid and original gels



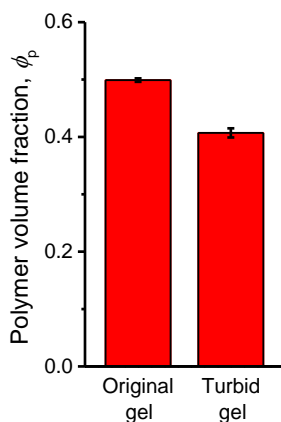
**Fig. S8.** Tensile behavior of original gel and turbid gel. (a) Young's modulus  $E$ , (b) fracture stress  $\sigma_b$ , (c) fracture strain  $\epsilon_b$ , and (d) work of extension at fracture  $W_{\text{extf}}$ , calculated from the tensile stress-strain curves.

Fig. S8 exhibits the Young's modulus  $E$ , fracture stress  $\sigma_b$ , fracture strain  $\epsilon_b$ , and work of extension at fracture  $W_{\text{extf}}$ , calculated from the uniaxial tensile stress-strain curves of the original gel and the turbid gel at 25 °C (Fig. 6b, main text). As the total water contents ( $W_T$ 's) of the turbid gel ( $55.0\% \pm 0.8\%$ ) and the original gel ( $45.7\% \pm 0.3\%$ ) are different<sup>2</sup>, we calculated their polymer volume fractions ( $\phi_p$ ) to remove this effect.  $\phi_p$  of the gels is calculated by the equation

$$\phi_p^{-1} = 1 + [W_T / (1 - W_T)] / (\rho_p / \rho_w),$$

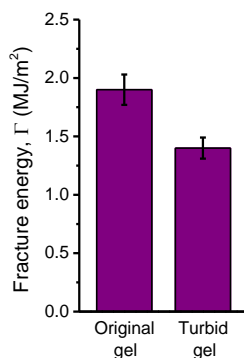
where  $\rho_p = 1.19$  and  $\rho_w = 0.98 \text{ g/cm}^3$  are the densities of PA and water at room temperature, respectively.<sup>3</sup>  $\phi_p$  of the original gel and turbid gel are 0.50 and 0.41, respectively (Fig. S9). By assuming the polymer density changes of the original gel and the turbid gel are homogeneous,  $E$ ,  $\sigma_b$ , and  $\epsilon_b$  are related to  $\phi_p$ :  $E = E^N \phi_p$ ,  $\sigma_b = \sigma_b^N \phi_p^{2/3}$ , and  $\lambda_b = \lambda_b^N \phi_p^{1/3}$ , where  $E^N$ ,  $\sigma_b^N$ , and  $\lambda_b^N$  are the values at the virtual

reference state ( $\phi_p = 1$ ).<sup>4</sup> Here,  $\lambda_b = \varepsilon_b + 1$  is the fracture stretch ratio.  $E^N$ ,  $\sigma_b^N$ , and  $\varepsilon_b^N$  of the original gel and the turbid gel are almost the same (Figs. 6c-e, main text).



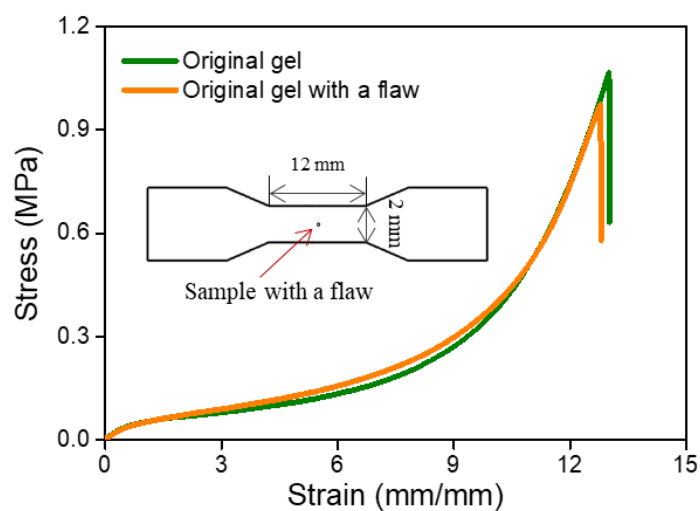
**Fig. S9.** Polymer volume fractions of original gel and turbid gel.

Single-edge notch test was performed to evaluate the toughness of the original gel and the turbid gel.<sup>5</sup> The toughness represented by fracture energy  $\Gamma$  is estimated and shown in Fig. S10. Similarly, fracture energy  $\Gamma$  of the turbid and original gels at the virtual reference state ( $\phi_p = 1$ ) is obtained by  $\Gamma = \Gamma^N \phi_p^{2/3}$ .  $\Gamma^N$  are about  $2.5 \pm 0.2$  kJ/m<sup>2</sup> for the turbid gel and  $3.0 \pm 0.2$  kJ/m<sup>2</sup> for the original gel (Fig. 6g, main text), respectively, which are nearly the same. Therefore, all the mechanical tests in this work suggest that the mechanical performance of PA gels can keep almost unchanged before and after thermal treatment.



**Fig. S10.** Fracture energy  $\Gamma$  of original gel and turbid gel.

## 7) Comparison of uniaxial tensile behavior of the original gels with and without a flaw



**Fig. S11.** Comparison of the uniaxial tensile behavior of the original gels with and without a flaw. Inset shows a dumbbell shape sample with a 0.25 mm diameter flaw in the center of the sample. The gels with and without a flaw show nearly the same tensile behavior, indicates that the PA gel is flaw insensitive up to a size of submillimeter. This explains why the turbid gel containing water aggregations with a size of several micrometers has similar mechanical performance to the original gel.

## **2. Supporting movie**

**Movie S1. Movie to show the autonomic disappearance of the recorded temporary information on the surface of PA gels.** A letter “L” is initially written on the surface of the gel; after 30 s, “S” is written, and L nearly disappears at this time; then, “W” is written after waiting another 30 s, and S almost disappears; finally, W also disappears, and the PA gel turns to transparent as before.

### 3. Supporting references

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