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# Determination of Source Parameters of Deep Earthquakes around Japan from Long-period Rayleigh Waves

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## Abstract

Source parameters of fifteen deep and intermediate earthquakes which occurred in and around Japan are determined. Focal mechanisms are obtained from first-motion data. The long-period Rayleigh waves recorded by IDA network are used for the determination of source process time  $\tau$  and seismic moment  $M_0$ . It is found that  $M_0$  is proportional to  $\tau^3$ . Broad-band body wave magnitude and  $\log M_0$  is linearly related. This relationship suggests that the apparent stress of deep and intermediate shocks is nearly constant for a wide range of depth.

## 1. Introduction

Systematic researches of the source process of deep and intermediate earthquakes (hereafter we collectively call them "deep earthquakes", unless otherwise mentioned) were not numerous, because of infrequent occurrence of deep events. The relationship among the source parameters such as seismic moment, source process time and magnitude was studied by a few investigators (Abe, 1982; Vassiliou and Kanamori, 1982). For most of the previous studies of deep events, body waves were used (e.g., Mikumo, 1971; Wyss and Molnar, 1972; Chung and Kanamori, 1980; Sasatani, 1980). A few studies employed long-period surface waves (Abe, 1972; Furumoto and Fukao, 1976; Osada and Abe, 1981). A weak excitation of fundamental mode surface waves by deep shocks has been a major reason of this small number of surface wave analyses of deep events. However, long-period surface waves represent the overall feature of earthquakes. Furthermore, surface wave analysis of deep events makes it possible to compare source parameters between deep and shallow earthquakes on a common basis, since surface wave analyses have been exten-

sively made for shallow events (e.g., Kanamori and Given, 1982).

In this paper source process times and seismic moments of deep shocks are determined from long-period Rayleigh waves recorded by IDA (International Deployment of Accelerographs) network (Agnew et al., 1976). Because of the long-period characteristics of IDA instruments, it is possible to analyze surface waves of deep events.

## 2. Earthquakes and mechanisms

Six deep ( $h > 300$  km) and nine intermediate ( $70 \leq h \leq 300$  km) earthquakes which occurred in and around Japan from 1977 to 1981 are selected. Figure 1 and Table 1 show their epicenters. All the events with magnitude  $M$  above 6.5 in JMA scale are included. Since  $M$  is not given by JMA for event No. 2, we adopt the value given by Utsu (1982). The long-period Rayleigh waves of events  $M \geq 6.5$  are recorded with adequate signal-to-noise ratio by IDA network. Origin times (GMT), epicenters and depths in Table 1 are given by NEIS. The depth of event No. 9 is 69 km in Table 1. Because JMA gives 70 km for this event, it is included in this study.

Fault plane solutions are determined from the first-motion data given in ISC, EDR and JMA bulletins. Since the first-motions of deep events are clear

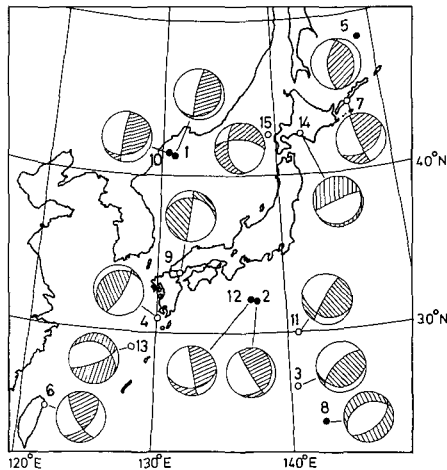


Fig. 1 Locations and mechanisms of earthquakes used. The epicenters for intermediate and deep events are shown by open and solid circles, respectively. Focal mechanisms are shown in equal-area projection of the lower hemisphere. Hatched area represents compressional quadrant.

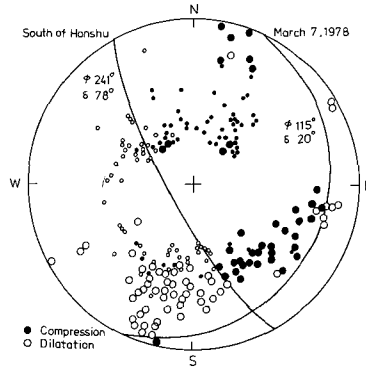


Fig. 2 Equal-area projection of the lower hemisphere for the first-motion data of the Honshu event (No. 2). The open and solid circles represent compression and dilatation, respectively. The large symbols are the readings from long-period seismograms, and the small symbols are from short-period seismograms.  $\phi$  and  $\delta$  denote dip direction and dip angle, respectively.

without contaminations of free-surface phases, bulletin reports are reliable. Furthermore, for deep events around Japan, the dense distribution of JMA stations enables us to determine two nodal planes almost uniquely. An example of the fault plane solutions is shown in Fig. 2 for the Honshu event (No. 2 of Table 1 and Fig. 1). 207 readings from bulletins are plotted. Two nodal planes are determined very well. The nodal plane solutions thus determined are given in Table 1. In the table  $\phi$  and  $\delta$  correspond to dip direction (measured clockwise from the north) and dip angle, respectively.

### 3. Surface wave analysis

Rayleigh wave seismograms recorded by IDA network are windowed between group velocities of 3.4 and 4.0 km/s. These values are not fixed but changed by up to 0.2 km/s according to visual inspections. This windowing separates fundamental Rayleigh waves from higher modes which are often excited by deep events. The seismograms thus windowed are Fourier transformed. All the phases R1-R5 are examined and as many phases as possible are analyzed.

First we determine source process time. For shallow earthquakes Kanamori and Given (1981) used an empirical relation between magnitude and source process time to correct the source finiteness. However, such an empirical relation is presently unknown for deep shocks. In this study source process time for individual shock is determined directly from surface wave spectra.

Trios of phases (e.g., R2, R3 and R4) observed at one station are used to cancel the propagation effect and the directional source phases (Furumoto and Nakanishi, 1983; Nakanishi and Kanamori, 1982). Averaging over many stations, we obtain the source process time  $\tau$ .  $\tau$  is determined at the period where the scatter is minimum for each event. This period ranges from 244 to 301 s in this study. The values of  $\tau$  are given in Table 1 with standard deviations. Table 1 shows that standard errors of  $\tau$  reach 20 s. Considering the fact that the sampling interval of IDA data used in this study is 20 s, we assume a step function point source (i.e.  $\tau=0$  s) when the measured  $\tau$  is less than 10 s.

Next we determine seismic moment using a method similar to that used by Kanamori and Given (1981). They determine the fault parameters and the seismic moment simultaneously using the moment tensor inversion while we obtain the fault parameters from first-motion data in this study. The basic equation is given by

$$AM_0 = Vr \quad (1)$$

where

$$A = s_R S_R^{(1)} + p_R P_R^{(1)} + iq_R Q_R^{(1)}. \quad (2)$$

$s_R$ ,  $p_R$  and  $q_R$  are determined from fault plane geometry and station azimuth (Kanamori and Stewart, 1976).  $P_R^{(1)}$ ,  $Q_R^{(1)}$  and  $S_R^{(1)}$  are Rayleigh wave excitation functions calculated for a given Earth model.  $M_0$  is the scalar seismic moment.  $Vr$  is the Fourier transform of the observed seismograms corrected for geometrical spreading, propagation, source process time and polar phase shifts. Expression of  $Vr$  is given by Kanamori and Given (1981). For the propagation corrections, the values of  $Q$ , group velocities and phase velocities compiled by Dziewonski and Anderson (1981) are used in this study. Excitation functions are calculated for the Earth model 5.08 M (Kanamori, 1970). We determine  $M_0$  for each phase (R1 to R5) at all the stations. We average the values from all the phases and the stations to obtain a value of  $M_0$  for a given period. In Eq. (1), a step function point source is assumed. For large events the corrections for the source finiteness and the finite rise time are necessary. Since the details of the rupture mode are unknown, we assume that the overall source finiteness effect is given by

$$\frac{\sin(\pi\tau/T)}{(\pi\tau/T)} \exp(-i\pi\tau/T), \quad (3)$$

where  $T$  is the wave period and  $\tau$  is the source process time which has already been determined. The left hand side of Eq. (1) must be multiplied by Eq. (3) to correct the finiteness.

The amplitude and phase of  $Vr$  at a period of 256 s for the Honshu event

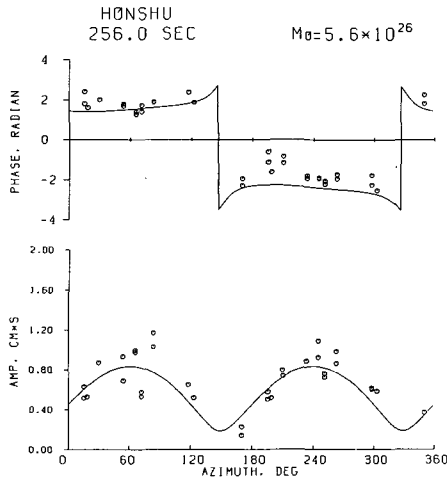


Fig. 3 Amplitude and phase spectra at a period of 256 s for event No. 2 as a function of azimuth. The azimuth is measured clockwise from the north. Two measurements at the same azimuth are obtained from multiple phases such as R2 and R4.

(No. 2) are shown in Fig. 3 as a function of azimuth. Figure 3 also shows the synthetic spectra (l.h.s. of Eq. (1)) of  $M_0 = 5.6 \times 10^{26}$  dyne  $\cdot$  cm corrected for the finiteness. Although the phase spectrum is not necessary for the determination of  $M_0$ , comparison of synthetic and observed radiation patterns makes it possible to check the agreement of the surface wave mechanism and the mechanism determined by first-motion data. Systematic deviations of the observed spectra from the synthetic radiation patterns for a particular azimuth indicate the existence of lateral heterogeneity of the phase velocity and  $Q$  structure. These discrepancies cannot be reduced as long as we use a laterally homogeneous Earth model for the propagation corrections.

Analyses are made at four different periods. They are, 150, 197, 256 and 300 s. Figure 4 shows the values of  $M_0$  of four events as a function of period. In this period range ( $150 \leq T \leq 300$  s),  $M_0$  is found to be nearly constant. Equation (3) shows that large  $\tau$  relative to  $T$  causes a significant effect of finiteness. For example, the Kunashiri event (No. 7) in Fig. 4 has a source process time of 66 s. If we assume  $\tau = 0$  s, then we underestimate the values of  $M_0$  by 10 to 30%.

For two events (Nos. 3 and 10), some of the fault parameters cannot be determined from the first-motion data alone. We adopt a method similar to that of Weidner and Aki (1973), in which we change the undetermined parameters iteratively. We regard a parameter value as the best fit, when it gives the

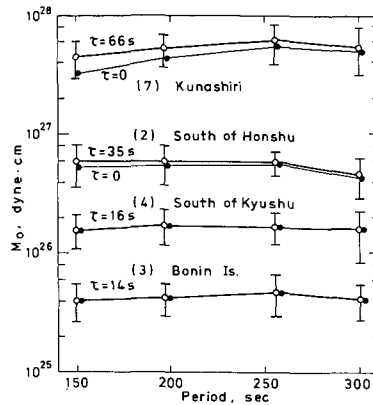


Fig. 4 Seismic moments of four events as a function of period. Open symbols with error bars represent the seismic moments corrected for the finiteness. The uncorrected values are shown by solid symbols.

minimum of RMS residual (observed minus calculated) of amplitude and phase.

#### 4. Seismic moment, source process time and magnitude

The seismic moments and source process times determined in this study are summarized in Table 1 with their standard deviations. The number of trios used for the determination of  $\tau$  is 3 to 15.  $M_0$  is the averaged value over the four periods. For each period, 13 to 37 phases of various stations are used. Standard deviation of  $M_0$  ranges 28 to 67% of  $M_0$ . For some of the events, other investigators independently obtained the seismic moments. Silver and Jordan (1983) obtained the total moment and the characteristic source time for events Nos. 2 and 7. Their values are very similar to our estimates of seismic moment and source process time. On the basis of GDSN (Global Digital Seismic Network) data, Dziewonski et al. (1981) and Dziewonski and Woodhouse (1983) obtained the moment tensor solutions for events Nos. 2, 3, 6, 13, 14 and 15. They mainly used body wave parts of seismograms and obtained almost the same values as our estimates. The differences are less than 30% of  $M_0$  for most of the events.

The relation between source process time and seismic moment is shown in Fig. 5. The source process time of a deep shock which occurred around Japan and determined by Furumoto and Nakanishi (1983) is added to our data. They found that source process times for large deep shocks are roughly constant in a narrow range of seismic moment ( $10^{27}$ – $10^{28}$  dyne  $\cdot$  cm). We extend the range

Table 1 List of earthquakes

| No. | Yr.  | Date<br>(m d) | Time<br>(h m s) | Lat.<br>(°N) | Long.<br>(°E) | Depth<br>(km) | Magnitudes |           |       |       | Mechanism           |                     | $M_0$ $\Delta M_0$<br>( $10^{25}$ dyn·cm) |    | $\tau$ $\Delta\tau$<br>(sec) |     | $\sigma_a$<br>(bar) |
|-----|------|---------------|-----------------|--------------|---------------|---------------|------------|-----------|-------|-------|---------------------|---------------------|---|----|------------------------------|-----|---------------------|
|     |      |               |                 |              |               |               | $m_1$      | $M_{JMA}$ | $m_B$ | $m_W$ | ( $\phi$ $\delta$ ) | ( $\phi$ $\delta$ ) |   |    |                              |     |                     |
| 1   | 1977 | 3 9           | 14 27 53.6      | 41.61        | 130.88        | 528           | 5.9        | 7.2       | 6.7   | 6.8   | 143 17 287 76       | 25                  | 8.1                                       | 0  | 0                            | 30  |                     |
| 2   | 1978 | 3 7           | 2 48 47.6       | 32.01        | 137.61        | 439           | 6.9        | 7.6       | 6.9   | 6.9   | 115 20 241 78       | 56                  | 18  | 35 | 12                           | 46  |                     |
| 3   | 1978 | 3 15          | 22 4 40.1       | 26.42        | 140.56        | 263           | 6.1        | 6.7       | 6.7   | 6.5   | 166 22 320 70       | 4.2                 | 1.6                                       | 14 | 19                           | 191 |                     |
| 4   | 1978 | 5 23          | 7 50 28.2       | 31.06        | 130.14        | 161           | 6.3        | 6.7       | 6.5   | 6.7   | 123 74 323 17       | 16                  | 6.0                                       | 16 | 12                           | 16  |                     |
| 5   | 1978 | 6 21          | 11 10 38.2      | 48.31        | 148.61        | 377           | 5.9        | 6.7       | 6.4   | 6.5   | 65 30 268 62        | 5.4                 | 2.8                                       | 23 | 18                           | 29  |                     |
| 6   | 1978 | 9 2           | 1 57 33.4       | 24.90        | 121.99        | 109           | 6.1        | 6.5       | 6.4   | 6.5   | 135 50 241 72       | 4.4                 | 2.9                                       | 0  | 0                            | 36  |                     |
| 7   | 1978 | 12 6          | 14 2 1.0        | 44.59        | 146.58        | 91            | 6.7        | 7.7       | 7.5   | 7.3   | 147 41 245 83       | 534                 | 215                                       | 66 | 3                            | 126 |                     |
| 8   | 1979 | 5 18          | 20 18 1.1       | 24.13        | 142.40        | 567           | 5.8        | 6.6       | 6.6   | 6.5   | 134 49 329 42       | 6.0                 | 1.7                                       | 0  | 0                            | 69  |                     |
| 9   | 1979 | 7 13          | 8 10 11.7       | 33.84        | 131.80        | 69            | 5.9        | 6.1       | 6.2   | 6.4   | 8 24 98 90          | 3.0                 | 1.4                                       | 0  | 0                            | 15  |                     |
| 10  | 1979 | 8 16          | 21 31 26.3      | 41.81        | 130.79        | 588           | 6.1        | 6.8       | 6.7   | 6.7   | 161 28 275 78       | 17                  | 6.4                                       | 29 | 19                           | 48  |                     |
| 11  | 1979 | 12 11         | 17 26 16.8      | 28.88        | 140.70        | 110           | 6.1        | 6.7       | 6.7   | 6.7   | 192 30 300 80       | 18                  | 12  | 36 | 21                           | 38  |                     |
| 12  | 1980 | 4 22          | 5 34 13.8       | 32.11        | 137.57        | 394           | 5.7        | 6.6       | 6.6   | 6.6   | 80 90 170 35        | 7.0                 | 2.3                                       | 12 | 15                           | 69  |                     |
| 13  | 1981 | 1 2           | 15 39 47.3      | 29.24        | 128.14        | 242           | 6.1        | 6.7       | 6.9   | 6.9   | 35 31 162 70        | 38                  | 16  | 31 | 14                           | 58  |                     |
| 14  | 1981 | 1 23          | 4 58 31.5       | 42.52        | 142.12        | 116           | 6.3        | 7.1       | 6.8   | 6.8   | 148 10 337 80       | 26                  | 14  | 31 | 7                            | 53  |                     |
| 15  | 1981 | 5 8           | 23 34 44.9      | 42.66        | 139.13        | 200           | 6.0        | 6.4       | 6.4   | 6.5   | 7 60 250 52         | 6.0                 | 2.0                                       | 0  | 0                            | 23  |                     |



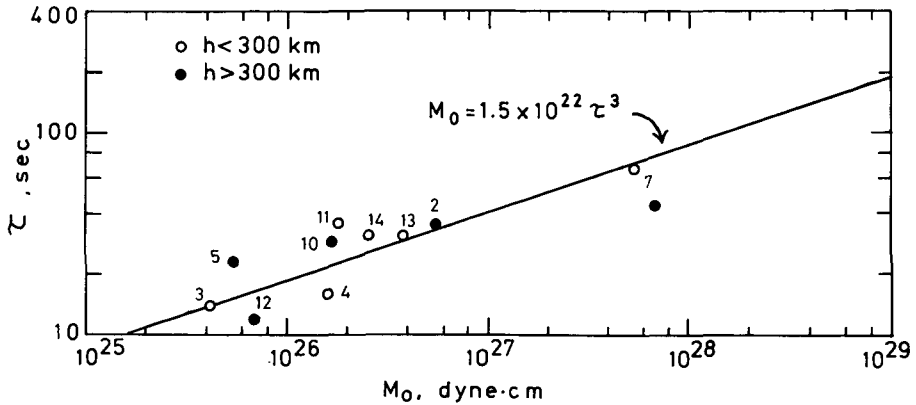


Fig. 5 The relation between seismic moment and source process time. Open and solid symbols represent intermediate and deep earthquakes, respectively. The numbers attached to symbols correspond to the event number in Table 1. A deep earthquake studied by Furumoto and Nakanishi (1983) is added. Equation (4) in the text is also shown by a solid line.

down to  $10^{25}$  dyne · cm. Figure 5 shows a tendency that smaller shocks have shorter source process times. Assuming a slope of 1/3 from the figure, we fit a straight line to these data in a least-squares sense, that is

$$M_0 = 1.5 \times 10^{22} \tau^3. \quad (4)$$

This relation is shown by a solid line in Fig. 5. Equation (4) is very close to the relation for low angle thrust earthquakes along trenches obtained by Furumoto and Nakanishi (1983).

Four kinds of magnitudes are listed in Table 1.  $m_1$  is the body wave magnitude given by NEIS. Since it is determined from short-period (usually 1 s) P waves, we call it  $m_1$  instead of  $m_0$  in this paper.  $m_1$  represents the size of an earthquake at its beginning (Kanamori, 1983).  $M_{JMA}$  is magnitude given by JMA. This scale is based on relatively long-period ( $T \leq 5$  s) waves. Since  $M_{JMA}$  is assigned to only Japanese events, it is impossible to compare with other data. To overcome these inconveniences, we employed the broad-band body wave magnitude  $m_b$ , which is determined from amplitudes and periods of body waves on various types of seismograms (e.g., Abe and Kanamori, 1979). In this study the amplitudes and periods of P, PP and S waves recorded at Pasadena are mainly used. Long-period ( $T \geq 3$  s) reports in EDR are supplementarily used. The average period of body waves ranges 2 to 11 s. These periods are long enough to represent the overall size of earthquakes. The values of  $m_b$  and  $M_0$  are plotted in Fig. 6. Although the data are not equally distributed, a linear relation between  $m_b$  and  $\log M_0$  is seen in this figure. A similar plot was given

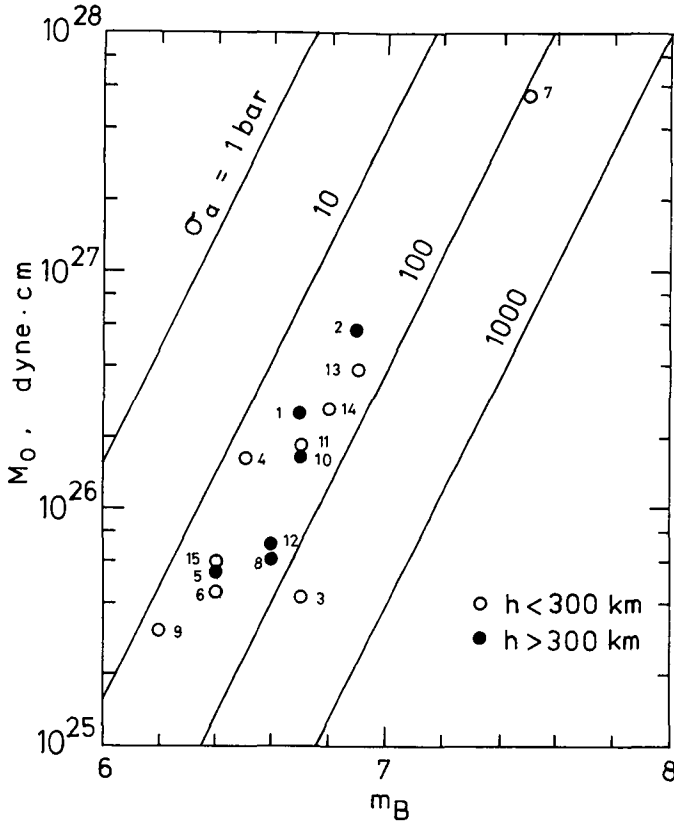


Fig. 6 The relation between body wave magnitude and seismic moment. Open and solid symbols represent intermediate and deep earthquakes, respectively. The numbers attached to symbols correspond to the event number in Table 1. The straight lines represent constant apparent stress.

by Abe (1982) for a different set of worldwide data. On the basis of this linear relationship between  $m_B$  and  $\log M_0$ , Kanamori (1983) introduced a moment magnitude scale  $m_w$  for deep events. The values of  $m_w$  that are calculated from  $M_0$  are listed in Table 1. Since the comparison of  $m_B$  and  $m_w$  is essentially the same as of  $m_B$  and  $\log M_0$ ,  $m_B$  and  $m_w$  agree very well (Table 1).

## 5. Discussion

For low angle thrust earthquakes along trenches, Furumoto and Nakanishi (1983) obtained a formula similar to Eq. (4). Assuming a constant stress drop and rupture velocity, they derived a scaling relation based on that formula. On

the other hand, it is suggested that stress drop increases with increasing depth for deep earthquakes (Mikumo, 1971 ; Sasatani, 1980). If this is the case, the scaling relation cannot be applied to deep earthquakes.

The relation between  $m_B$  and  $M_0$  is discussed by Abe (1982). Combining the Gutenberg-Richter's magnitude-energy relation and the definition of the apparent stress  $\sigma_a$ , he obtained

$$\log M_0 = 2.4 m_B + 5.8 - \log (\sigma_a / \mu), \quad (5)$$

where  $\mu$  is the rigidity near the source. Equation (5) means that  $m_B$  and  $\log M_0$  are linearly related if the apparent stress is constant. Assuming  $\mu = 9 \times 10^{11}$  dyne/cm<sup>2</sup> as the average for the depth range considered here, the relations for  $\sigma_a = 1, 10, 100$  and 1000 bar are shown in Fig. 6. It is seen in this figure that most of the earthquakes have  $\sigma_a$  between 10 and 100 bar. Each value of  $\sigma_a$  is summarized in Table 1 and the average is 56 bar. If we change  $\mu$  as a function of depth, we have similar values of  $\sigma_a$ . Figure 6 suggests that the apparent stress is nearly constant over a wide range of depth. Abe (1982) obtained the same result from the worldwide data, which were obtained by various methods and types of waves. In this study the region is limited to Japan and its vicinity, and seismic moments and magnitudes are determined by the same method for all the events. In spite of the differences in region and analysis method, the constant apparent stress is obtained for both data-sets, Abe (1982) and this study.

## 6. Conclusion

The seismic moment  $M_0$  and the source process time  $\tau$  of 15 deep earthquakes ( $6.2 \leq m_B \leq 7.5$ ) which occurred in and around Japan are determined from the analysis of surface waves recorded by IDA network. It is found that  $M_0$  is proportional to  $\tau^3$ . A linear relationship between  $\log M_0$  and  $m_B$  suggests the apparent stress is nearly constant over a wide range of depth.

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The computations were made at the Hokkaido University Computing Center.

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