



Title	Free-Standing Nanometer-Thick Covalent Organic Framework Films for Separating CO ₂ and N ₂
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Supporting Information

Free-standing Nanometer-Thick Covalent Organic Framework Films for Separating CO₂ and N₂

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Definition and calculation of "ideal selectivity" and "separation factor"

When the pure CO₂ or N₂ was permeated through the membrane, the permeance of each gas at each measurement point was calculated as follows (Eq. (1))

$$P = \frac{V}{A\Delta pRT} \left(\frac{dP}{dt} \right) \quad (1)$$

where V is the volume of the measurement room (15.3 cm³), A is the membrane area (1.33 cm²), Δp is the transmembrane pressure, R is the gas constant (8.31 J K⁻¹ mol⁻¹), T is the absolute temperature (at the ambient condition) and dP/dt is the pressure increase per unit time in the measuring room.

The ideal selectivity of the pure gases was calculated as follows (Eq. (2))

$$\text{Ideal selectivity} = \frac{P_{\text{CO}_2}}{P_{\text{N}_2}} \quad (2)$$

where P_{CO_2} and P_{N_2} are the permeance of CO₂ and N₂, respectively.

When the CO₂-N₂ mixture was permeated through the membrane, the CO₂/N₂ separation factor α was calculated as follows (Eq. (3))

$$\alpha = \frac{y_{\text{CO}_2}/y_{\text{N}_2}}{x_{\text{CO}_2}/x_{\text{N}_2}} \quad (3)$$

where $y_{\text{CO}_2}/y_{\text{N}_2}$ and $x_{\text{CO}_2}/x_{\text{N}_2}$ are the ratios of the molar fraction in the permeate and feed sides, respectively.

Details of model analysis

1 Gas permeation model of the COF films

The mechanism of gas sorption in a glassy polymer is explained by a dual site sorption model.¹

In this model, the Henry sorption (C_D) is the main mechanism of sorption into the matrix component, while Langmuir sorption (C_H) governs the sorption into the microvoid region. The gas concentration in the polymer membrane (C) is described as their sum

$$C = C_D + C_H = k_D p + \frac{C'_H b p}{1 + b p} \quad (4)$$

where k_D is Henry's law constant, p is the feed gas pressure, C'_H is the Langmuir capacity of the glassy polymer, and b is the Langmuir affinity constant.

The gas solubility coefficient (S) is written as the following equation:

$$S = \frac{C}{p} = k_D + \frac{C'_H b}{1 + b p} \quad (5)$$

2 Partial immobilization model

When a gas diffuses in a polymer membrane, we consider both the Henry and Langmuir diffusion mechanisms.

It was assumed that the gas species, which are trapped in the Langmuir site, can be relatively mobile in the glassy polymer (partial immobilization).

We then estimated that the concentration of a gas in the polymer membrane is described by eq. (4), Fick's first law is eq. (6):

$$J = -D_D \frac{\partial C_D}{\partial x} - D_H \frac{\partial C_H}{\partial x} = -D_D \left(\frac{1 + \frac{FK}{(1+bp)^2}}{1 + \frac{K}{(1+bp)^2}} \right) \frac{\partial C}{\partial x} \quad (6)$$

where J is the flux of the gas species, D_D and D_H are the diffusion coefficient under the Henry and Langmuir modes, respectively, F is the ratio of D_D and D_H (D_D/D_H), and K is equal to $C'_H b/k_D$.

By using eq. (6), Fick's second law is eq. (7):

$$\frac{\partial C}{\partial t} = \frac{\partial J}{\partial x} = \frac{\partial}{\partial x} \left(-D_D \left(\frac{1 + \frac{FK}{(1+bp)^2}}{1 + \frac{K}{(1+bp)^2}} \right) \frac{\partial C}{\partial x} \right) \quad (7)$$

Since the gas permeability (P), gas diffusion coefficient (D) and gas solubility coefficient (S) of the polymer membrane have the relationship of $P = DS$ (solution-diffusion mechanism), the average permeability (P_a) of the membrane is eq. (8)

$$P_a = DS = -D_D \left(\frac{1 + \frac{FK}{1+bp}}{1 + \frac{K}{1+bp}} \right) S = k_D D_D \left(1 + \frac{FK}{1+bp} \right) \quad (8)$$

3 Numerical analysis of gas permeation through the COF films

Generally, the dual mode sorption model parameters (C'_H , b , and k_D) can be obtained by using a non-linear curve fitting for the experimental gas sorption isotherms using eq. (4). However, the amount of gases absorbed in the COF film prepared by the alternating deposition cannot be experimentally measured

because its thickness is extremely thin. We determined the parameters by numerically solving eq. (7) by the finite differential method and adjusting its solution to the experimental permeation curve. An analysis program was built by the python 3.7.1 environment. Eq. (7) was numerically solved using the Crank-Nicolson method along with the Gauss-Seidel method. The appropriate parameters were calculated by minimizing the residual sum of squares of the numerical solution and experimental data. Algorithms for searching the minimum value used the differential-evolution method, which can search for the global minimum of a system.

4 DFT calculation

The interaction energy between the COF and the gas molecules was calculated by the density functional theory (DFT). The calculations were performed using the Gaussian 16W package. To consider weak interactions between the atoms, the D3 dispersion correction reported by Grimme is included in the DFT calculations (DFT-D).² Basis sets of the 6-31 G (d)³ and B3LYP^{4, 5} functional were used for the structure optimization. The total energies of the optimized structures were calculated using the basis sets of the 6-311G(d) and B3LYP functional. The basis set superposition error was corrected using the counterpoise method.⁶

The interaction energies between the COF and the gas molecules(ΔE) were calculated using the following equation (Eq.(4)).

$$\Delta E = E_{\text{COF+gas}} - (E_{\text{COF}} + E_{\text{gas}})$$

where $E_{\text{COF}+\text{gas}}$ is the total energy of the COF with gas molecules at a binding site, and E_{COF} and E_{gas} are the energies of the COF and the gas molecules, respectively.

Reference in Supporting Information

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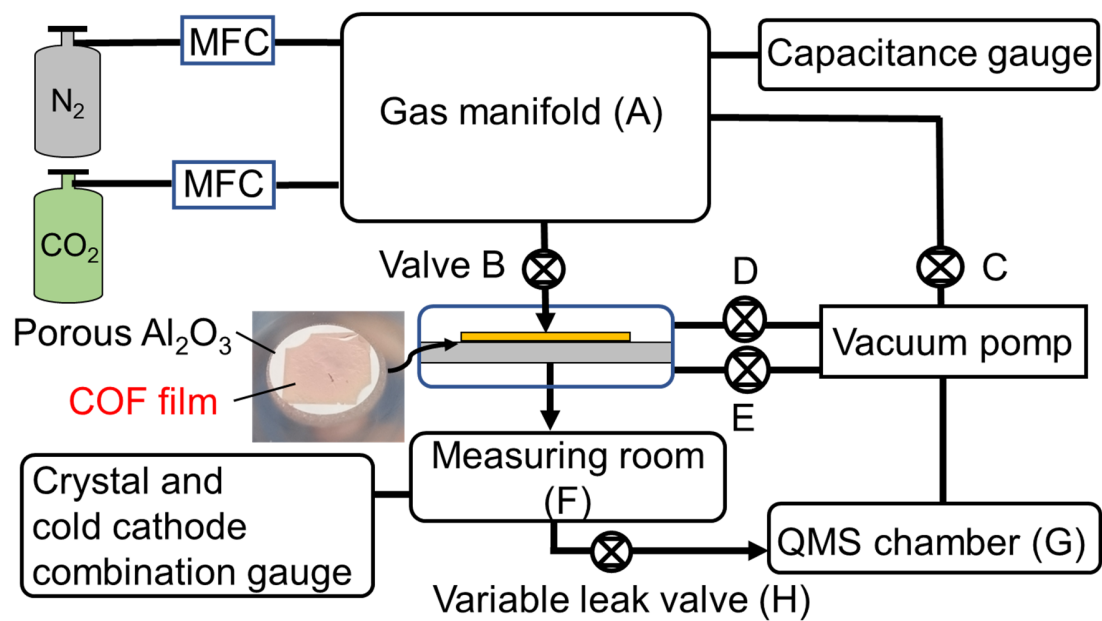


Figure S1. Schematic illustration of the apparatus for the gas permeation experiments.

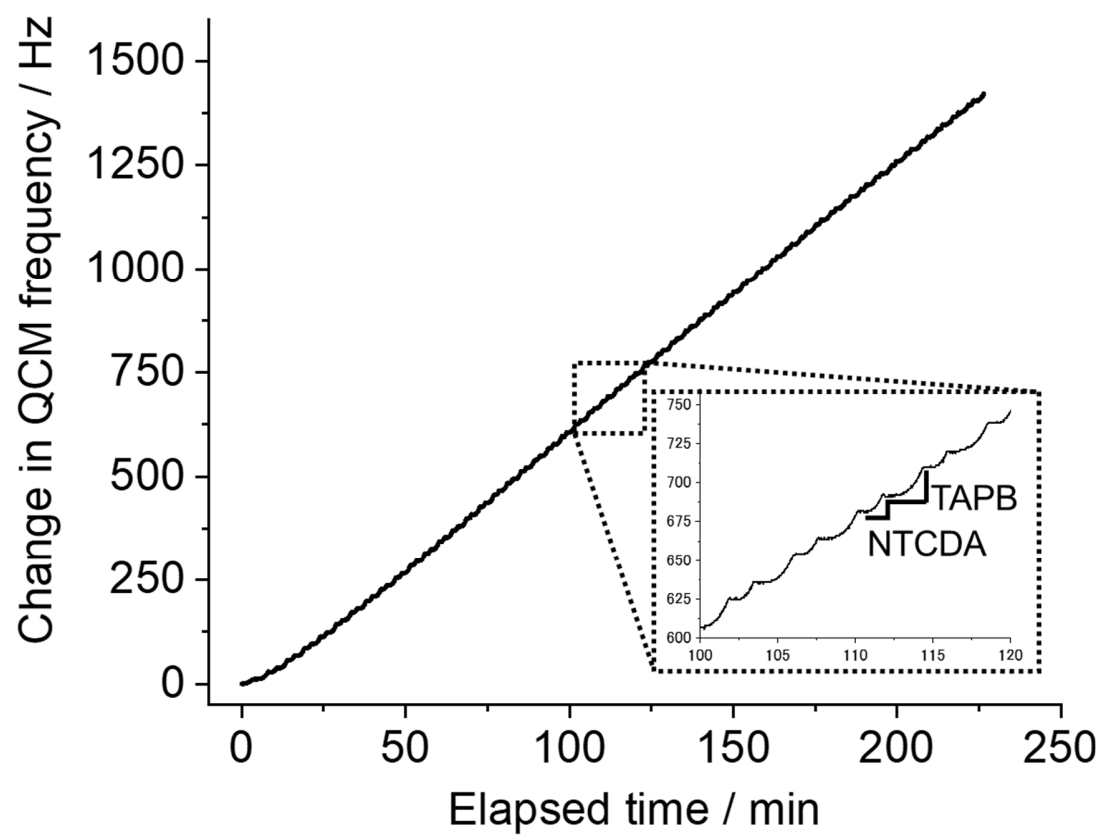


Figure S2: Decrease in the QCM frequency, which corresponds to the deposited amount of TAPB and NTCDA, occurred in a stepwise manner as shown in Fig. S2.

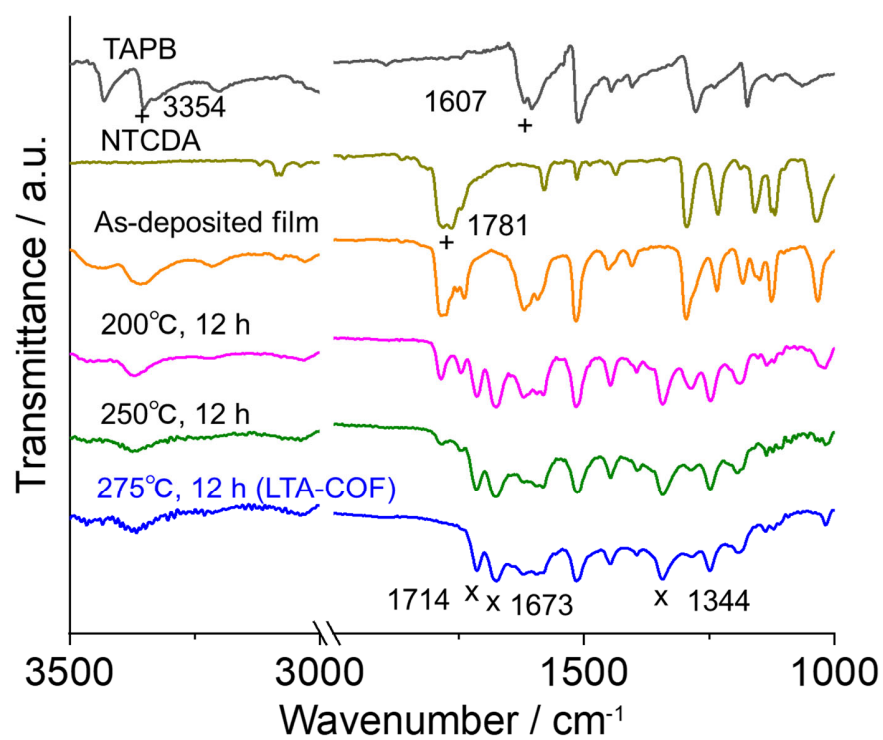


Figure S3: FTIR spectrum of precursors, as-deposited film (deposition ratio of TAPB : NTCDA = 1 : 2.5) and as-deposited film annealed at various temperatures for 12 h.

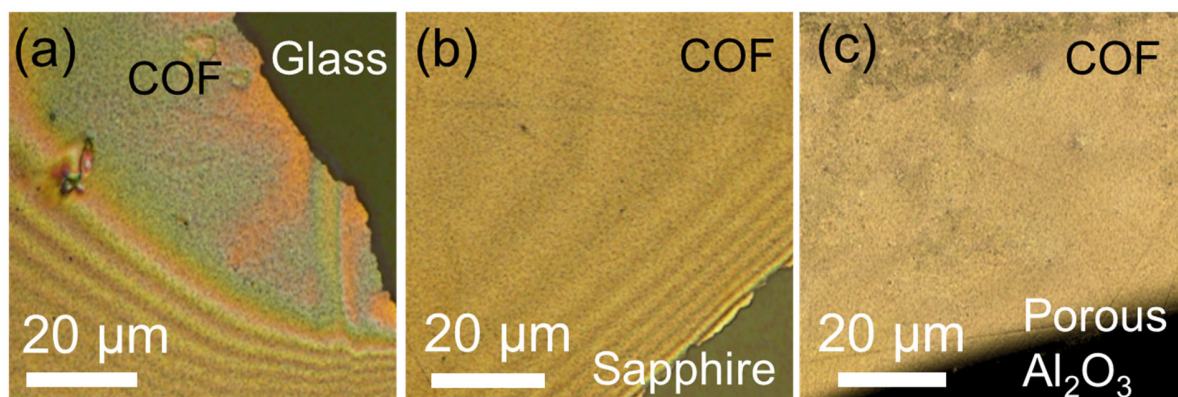


Figure S4: Laser microscope images of the film lifted out and transferred to different substrates from the water surface. Free-standing COF films placed on (a) a glass substrate, (b) a sapphire substrate, and (c) a porous Al₂O₃ support.

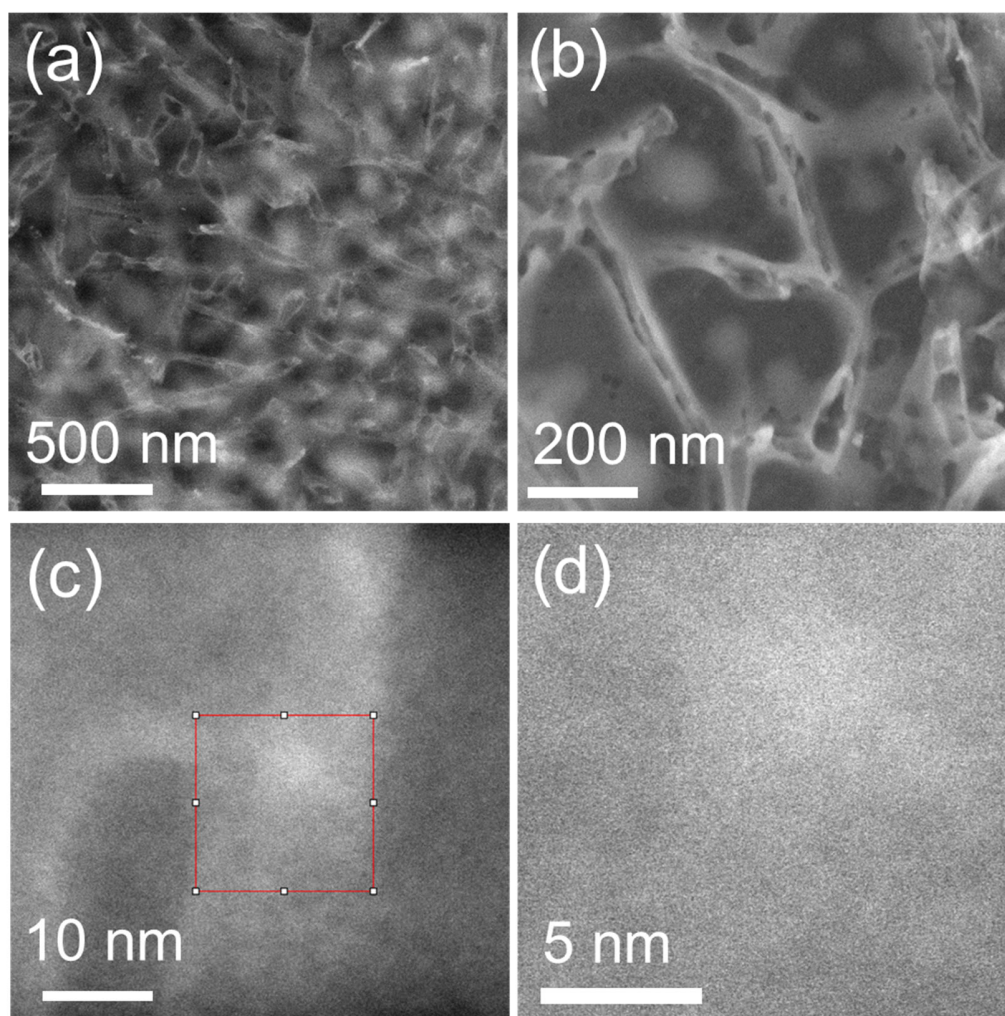


Figure S5: Examination of the LTA-COF film by STEM

(a), (b) Overall structure of the LTA-COF film

(c), (d) Further magnified images. (d) shows the red area of (c).

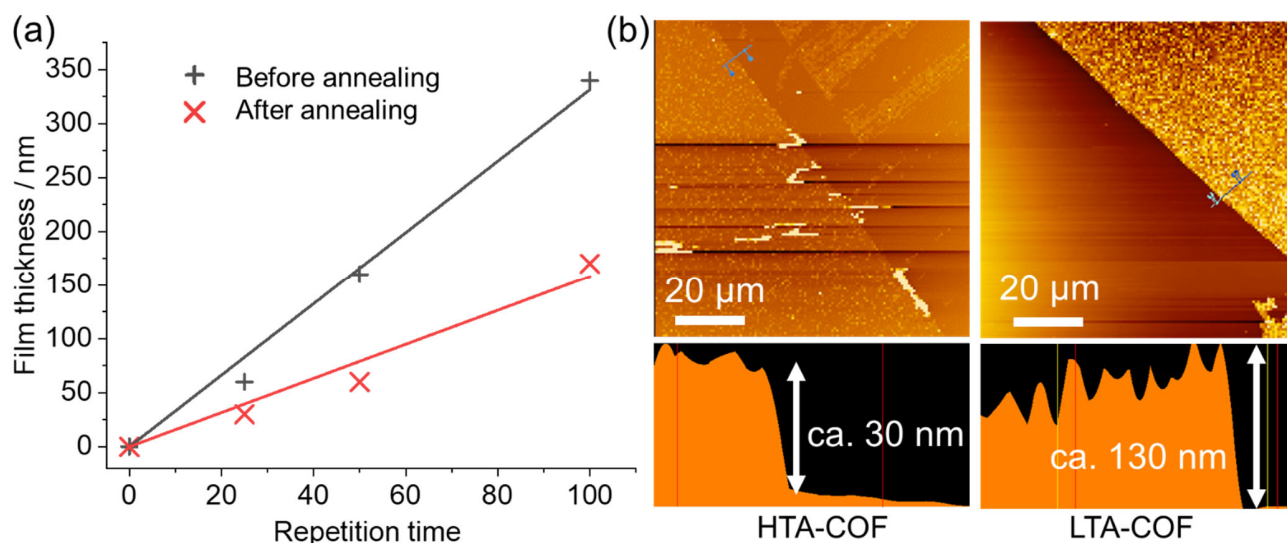


Figure S6: (a) The film thickness of the HTA-COF film for various repetition times (0-100). Black marks of “+” and red marks of “x” denote the film thickness of before and after annealing, respectively. The black and red lines are linear regression lines of each data set. (b) AFM measurement at the scraped edges of the HTA-COF and LTA-COF films (different repetition times) grown on SiO_2/Si wafers.

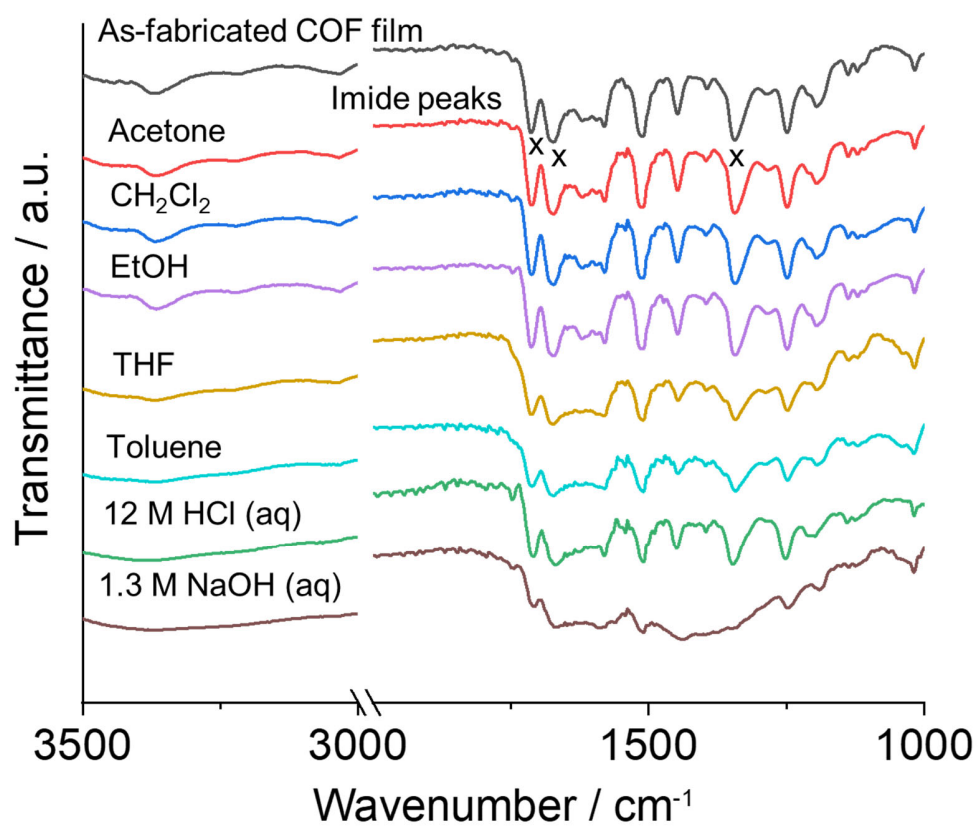


Figure S7: FTIR spectrum of the HTA-COF films before and after immersing in various solvents for 24 hours.

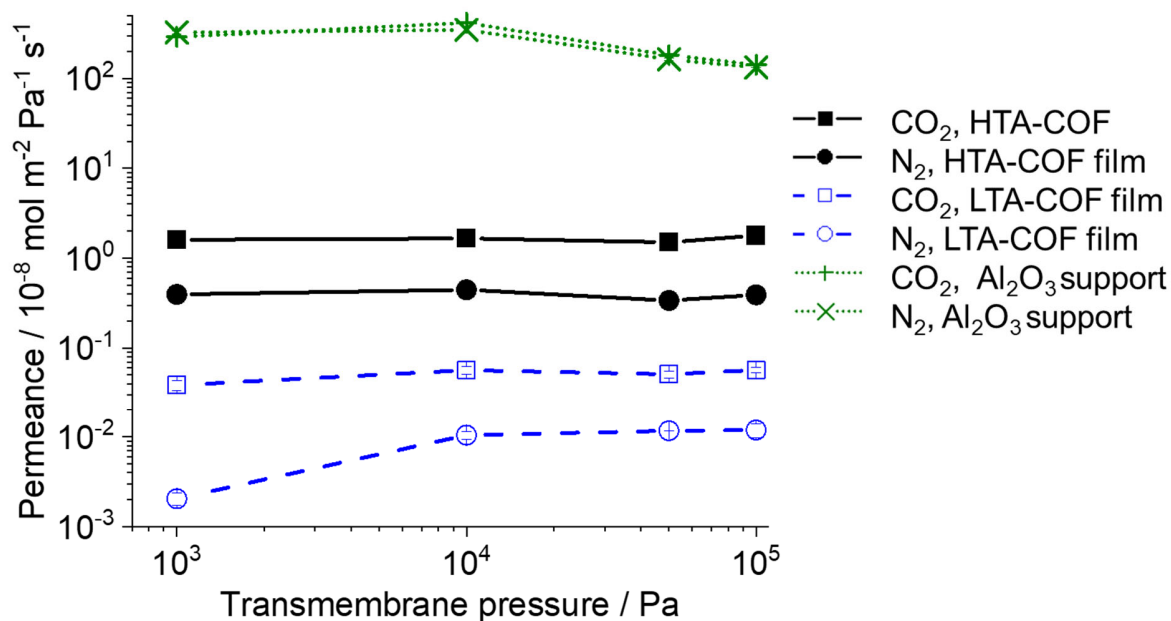


Figure S8: CO₂ and N₂ gas permeances of the HTA-COF films, LTA-COF films and a Al₂O₃ support at the transmembrane pressures of 10³-10⁵ Pa.

Note: CO₂ and N₂ permeances of the Al₂O₃ support were sufficiently greater than that of the HTA- and LTA- COF film. These results indicated that the porous Al₂O₃ support did not prevent CO₂ and N₂ from permeating through the membrane.

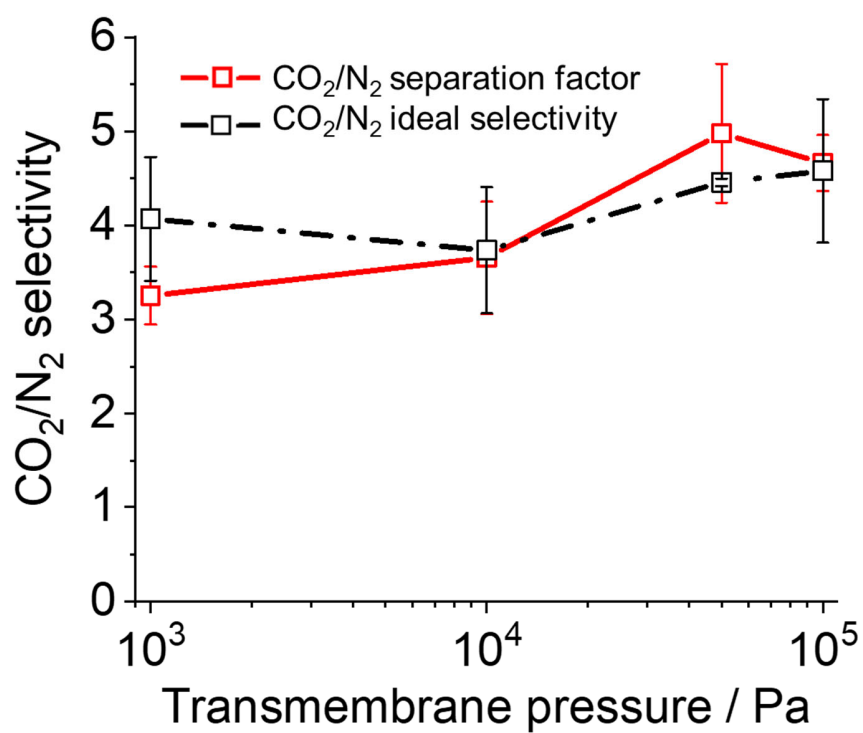


Figure S9: Pressure dependence of the CO₂/N₂ separation factor and CO₂/N₂ ideal selectivity for the HTA-COF film.