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Supplementary Materials for

Role of hierarchy structure on the mechanical adaptation of self-healing hydrogels under cyclic stretching

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Fig. S1. Bicontinuous phase separation structure of s-PA and its deformation under loading characterized by *in-situ* SAXS. (A) The illustration of the specimen used in *in-situ* SAXS tests. The rectangular sample ($L_0 = 7.5 \text{ mm}$, $H_0 = 16 \text{ mm}$, thickness 1.65 mm) was used. The loading strain rate is 1 s⁻¹. (B) Typical 2D SAXS patterns under the uniaxial tensile ($\lambda = 1, 1.75, 7.25$ are taken as examples). We can see from the patterns, with increasing stretch ratio λ , the phase networks become oriented along the stretching direction (schemed in the right figure). (C) 1D scattering profiles I(q) as a function of q at $\lambda = 1.75$ in parallel (//) and perpendicular (\perp) to the stretch direction. Inset shows the sector regions for integrating the 1D scattering intensity. From the position of scattering peaks ($q_{l',max}$ and $q_{\perp,max}$), we obtain the *d*-spacing change in the stretching direction ($d_{l'}$) and perpendicular direction (d_{\perp}), by $d_{l'} = 2\pi/q_{l',max}$ and $d_{\perp} = 2\pi/q_{\perp,max}$, respectively. (D) The $d_{l'}$ and d_{\perp} as a function of λ . The *d*-spacing (d_0) between adjacent soft regions or hard regions in the undeformed gel is $d_0 \approx 100 \text{ nm}$. When the gel is loaded to $\lambda > 1.75$, the $d_{l'}$ exceeds the detecting range. The microscopic deformation is obtained by d_{l'/d_0} and d_{\perp}/d_0 . Inset shows the direction of the macroscopic stretch ratio λ . The orange lines stand for the prediction of affine deformation of the phase networks (for incompressible materials, the affine deformation follows $d_{l'/d_0} = \lambda$ and $d_{\perp}/d_0 = \lambda^{-1/2}$). The data is extracted from ref (49). The d_{\perp}/d_0

prediction of affine deformation of the phase networks (for incompressible materials, the affine deformation follows $d_{ll}/d_0 = \lambda$ and $d_{\perp}/d_0 = \lambda^{-1/2}$). The data is extracted from ref (49). The d_{\perp}/d_0 versus λ curve can be divided into three regimes with the split points λ_{affine} (black arrow) and λ_c (blue arrow). The λ_{affine} ($\lambda_{affine} = 3.06$) is determined by the critical point at which the microscopic deformation of the phase network begins to deviate from the predicted affine deformation. The λ_c ($\lambda_c = 9.2$) is determined by the point at which d_{\perp}/d_0 slightly increases with λ . According to our previous work (51), the percolated hard and soft phase networks deform equally at stretch ratio λ $< \lambda_{affine}$ (regime I), but the hard phase network sustains more stress due to high stiffness. At $\lambda =$ λ_{affine} , damage to the hard phase strands begins to occur as they carry most of the stress, and the contraction of the damaged hard phase strands exerts a large shear stress on the adjacent soft phase strands. The load is transferred to adjacent hard-phase strands via the soft-phase strands (regime II). With increasing λ , more hard phase strands rupture until the shear stress is larger than the strength of the soft phase strands, resulting in the soft phase network rupture at $\lambda = \lambda_c$. The rupture of the soft phase network results in a catastrophic fracture of the whole sample immediately (regime III). Above the $\lambda = \lambda_c$, the d_{\perp}/d_0 increases with λ since the rupture of soft phase strands destroys the ordering of neighboring hard phase strands. Therefore, the λ_{affine} denotes the onset of damage to the hard-phase network, and the λ_c denotes the onset of damage to the soft-phase network.



Fig. S2. Dynamic mechanical behavior of the s-PA gel. Frequency (ω) dependence of the storage modulus *G'*, loss modulus *G''*, and loss factor tan δ . The vertical dotted line indicates the angular frequency at $\omega = 2\pi \dot{\epsilon} (45)$ for the strain rate of cyclic loading $\dot{\epsilon} = 1 \text{ s}^{-1}$. *G'* does not reach the plateau modulus at the high frequency limit, indicating that the lifetime of ionic bonds (τ_s) is short, beyond our observation window ($\tau_s < 10^{-5} \text{ s}$). The data is adopted from ref (47).

Section S1. Cyclic training behaviors of soft materials with or without hierarchical

structure

To illustrate the effect of the hierarchical structure in cyclic training, we subjected two control samples to cyclic loading (stretching): one with very weak phase separation (w-PA gel) and another without phase separation but with good self-healing properties (PPEA elastomer).



Fig. S3. Comparison of fracture behavior in strong (s-PA) and weak (w-PA) phase-separated PA gels under monotonic and cyclic stretching. (A) SAXS result for s-PA and w-PA. s-PA

exhibits a pronounced density contrast (proportional to the modulus contrast) tween its hard and soft phase domains, while w-PA displays a substantially weak density contrast between the two phases. (**B**) Pure shear geometry used for monotonic and cyclic stretching ($L_0 = 50$ mm, and $H_0 =$ 10 mm). (**C**) The stress-stretch (S-S) curve for w-PA gel. (**D**) The S-S curve for s-PA gel. In figure C and D, the black "X" denotes sample fracture under monotonic stretching. The red "X" indicates sample fracture under cyclic stretching condition. The red dots denote the sample capable of enduring $N_{tr} = 10^4$ cycles at λ_{tr} equal to the corresponding λ without fracture. (**E**) Evolution of loading-unloading curves with training cycle (N_{tr}) at $\lambda_{tr} = 8.5$ for s-PA. (**F**) Evolution of loadingunloading curves with training cycle (N_{tr}) at $\lambda_{tr} = 9.1$ for s-PA.



Fig. S4. Dynamic mechanical behavior, SAXS result, and cyclic training behavior of the PPEA elastomer. (A) Chemical structure of ethylene glycol phenyl ether acrylate (PEA) monomer. The PPEA elastomer is crosslinked by 0.1 mol% MBAA in relative to the monomer. (B) Frequency (ω) dependence of the storage modulus *G'*, loss modulus *G''*, and loss factor tan δ . The vertical dotted line indicates the angular frequency at $\omega = 2\pi \dot{\varepsilon}$ for the strain rate of cyclic loading $\dot{\varepsilon} = 0.5$ s⁻¹. (C) SAXS result. The SAXS result shows no phase separation and the WAXS result shows no crystallization in the PPEA elastomer (*55*). These results suggest that no hierarchical structure formed in PPEA elastomer. (D) The S-S curve for PPEA elastomer. The black "X" denotes sample fracture under monotonic stretching. The red "X" indicates sample fracture under cyclic stretching condition. The red dots denote the sample capable of enduring $N_{tr} = 10^4$ cycles at λ_{tr} equal to the corresponding λ without fracture.



Fig. S5. Cyclic training of PPEA elastomer. The same pure shear geometry as Fig. 2A was used for the training. Training was performed at 24 °C with an initial strain rate $\dot{\varepsilon} = 0.5 \text{ s}^{-1}$. (A) Evolution of loading-unloading curves with training cycle (N_{tr}). (B) Loading-unloading curves for a trained gel resting for t_{rest} . (C) W_{ex} as a function of time (red: training, blue: detraining). (D) λ_{res} as a function of time (red: training, blue: detraining). Training at $\lambda_{tr} = 2.1$ for $N_{tr} = 10^4$ cycles is taken as an example. We can observe that the training curves reach the steady state rapidly, and both the W_{ex} and λ_{res} fully recover quickly during detraining. This suggests that the PPEA elastomer does not possess a long-term memory of the training effect.



Fig. S6. Prony series fitting for W_{ex} versus N_{tr} curve of s-PA hydrogel and PPEA elastomer trained at $\lambda_{tr} = 2.1$ and $N_{tr} = 10^4$ cycles. (A) Comparison of the fitting curve by the two-term (n = 2) and three-term (n = 3) Prony series fitting of s-PA hydrogel. (B) Two-term (n = 2) Prony series fitting for PPEA elastomer. The fitting equation is $y = y_0 + \sum_{i=1}^{n} A_i e^{-x/t_i}$, where y corresponds to W_{ex} , x is N_{tr} , t_i is the characteristic training cycles N_i , and y_0 is the equilibrium W_{ex} of the cyclic training. From the fitting we obtained training cycle parameters $N_1(\sim 0.6)$ and $N_2(\sim 15)$ for W_{ex} of the PPEA.

Material	λ_{tr}	Total training	Full recovery time	Full recovery time
		time	for $W_{\rm ex}^{a}$	for $\lambda_{\rm res}^{b}$
PPEA elastomer	1.3	14.2 ks	1147 s	67 s
PPEA elastomer	1.8	35.2 ks	3847 s	547 s
PPEA elastomer	2.1	45.1 ks	7447 s	547 s
s-PA gel	1.3	8.7 ks	18247 s	7447 s
s-PA gel	1.7	17.8 ks	68647 s	18247 s
s-PA gel	2.1	26.1 ks	>86647 s	18247 s

Table S1. The comparison of training time and full recovery time of s-PA gel and PPEA elastomer.

^{*a*} Full recovery time for W_{ex} represents the time it took for $W_{\text{ex}}(t_{\text{rest}})$ to recover to W_{ex0} which was the work of extension of the first loading to corresponding λ_{tr} . ^{*b*} Full recovery time for $\lambda_{\text{res}}(t_{\text{rest}})$ represents the time it took for $\lambda_{\text{res}}(t_{\text{rest}})$ to recover to a value of 1.

Section S2. The Prony series fitting of training curves

The W_{ex} and λ_{res} in training process are obtained from the loading-unloading curves as shown in **Fig. 2** (**B**, **C** and **D**). **Fig. S7B** shows that W_{ex} and λ_{res} change rapidly at the beginning training cycles and then reach the plateau. This is universal for training at varied λ_{tr} . As shown in **fig. S7C**, all the normalized W_{ex}/W_{ex0} (W_{ex0} is the work of extension of the first loading to corresponding λ_{tr}) versus N_{tr} curves exhibit similar behavior, that the required energy to deform the gel to a certain stretch ratio (λ_{tr}) decreases with training cycle and finally almost reaches saturation.

To elucidate the contribution of the hierarchy structure to training process, we use the generalized Maxwell model (Prony series) to analyze the plot of W_{ex} versus N_{tr} . The Prony series consists of a spring and *n* Maxwell elements connected in parallel (68, 69), which is a phenomenological model commonly used to fit the relaxation dynamics of viscoelastic material such as biological tissues (70), elastomers (69, 71), hydrogels (72, 73), etc. Here, we try to use the Prony series to fit the reduction of energy required for a preset λ_{tr} during training, we rewrite the Prony series as

$$W(N_{tr}) = W_{\infty} + \sum_{i=1}^{n} W_{i} e^{-N_{tr}/N_{i}}$$
(S1)

where $W(N_{tr})$ is the W_{ex} at the N_{tr} , W_{∞} is the equilibrium W_{ex} of the cyclic training, N_i are the characteristic training cycles, W_i are training strengths correlated to the reduction of W_{ex} , and n is the series order. We find that n = 3 were sufficient to fit the W_{ex} versus N_{tr} curves (**fig. S6A**). **Fig. S7D** shows an example of the fitting result at $\lambda_{tr} = 2.9$ and total $N_{tr} = 10^4$ cycles. From the fitting results, we obtain three characteristic training cycles $N_1 = 1$ cycle, $N_2 = 18$ cycle, $N_3 = 1003$ cycle, with the training strengths $W_1 = 49.3$ kJ/m³, $W_2 = 29.8$ kJ/m³, $W_3 = 19$ kJ/m³, and $W_{\infty} = 31.1$ kJ/m³.

The Prony series fitting parameters of gel training at varied λ_{tr} for $N_{tr} = 10^4$ cycles are presented in **fig. S7E** and the normalized W_i/W_{ex0} and W_{∞}/W_{ex0} are shown in **fig. S7F**. The characteristic training cycles $N_1(\sim 1)$, $N_2(\sim 20)$, $N_3(\sim 1000)$ are shown in **Fig. 3A**. By comparing the characteristic times with the non-phase-separated PPEA and rheological result, we assign $N_1(\sim 1)$, $N_2(\sim 20)$, $N_3(\sim 1000)$ to short scale ionic breaking, the local adaption of transient networks, and the adaption of hard phase network, respectively. The decrease of W_{∞}/W_{ex0} and W_3/W_{ex0} at $\lambda_{affine} < \lambda_{tr} < \lambda_c$ support that the broken of hard phase network (with longest characteristic training time) weakens the training effect. The characteristic training times, τ_1 , τ_2 , τ_3 , are obtained from the product of N_i and the corresponding training time per cycle. τ_1 , τ_2 , τ_3 in three different orders of magnitude increase with λ_{tr} (**fig. S7G**). But the slopes of τ_i versus λ_{tr} change around the λ_{affine} , indicating that the training dynamics are affected by the damage in the hard phase network.



Fig. S7. Evolution of work of extension (W_{ex}) with training cycle N_{tr} of s-PA gel and the Prony series fitting. (A) Pure shear geometry ($L_0 = 50 \text{ mm}$, $H_0 = 10 \text{ mm}$) and triangle loading profile for cyclic training. During cyclic training, the maximum and minimum stretch ratios are kept at preset values λ_{tr} and 1, respectively. (B) The W_{ex} and λ_{res} as a function of N_{tr} . Training at $\lambda_{tr} = 2.9$ is taken as an example. (C) Normalized W_{ex}/W_{ex0} versus N_{tr} for the samples tested at varied λ_{tr} . W_{ex0} is work of extension of the first loading to λ_{tr} . Inset shows the plots in a logarithmic scale. (D) Fitting the W_{ex} versus N_{tr} curve by the Prony series. $\lambda_{tr} = 2.9$ is taken as an example. The number of terms in the Prony series is picked to be n = 3. (E) The Prony series fitting parameter W_i , W_{∞} and W_{ex0} as a function of λ_{tr} . (F) Normalized Prony series fitting parameter W_i/W_{ex0} and W_{∞}/W_{ex0} as a function of λ_{tr} . (G) The characteristic training times τ_1 , τ_2 , τ_3 of W_{ex} (product of characteristic training cycles N_i and time consumption per cycle t_{cycle}) as a function of λ_{tr} . The vertical dotted line in **F-G** indicates λ_{affine} . The dashed lines are a guide for the eyes. The error bar ($\lambda_{tr} = 2.1$ to 3.7) is standard error (SE) from at least three measurements.

The λ_{res} increases sharply with N_{tr} at the beginning of the training and then reach a steady state (**fig. S8A**). To study the dynamics of residual stretch ratio λ_{res} during training, we use the Prony series to fit the normalized λ_{res} versus N_{tr} curves. The λ_{res} is normalized as

$$R(N_{\rm tr}) = \frac{\lambda_{\rm res}(N_{\rm tr}) - \lambda_{\rm res}(\infty)}{\lambda_{\rm res}(0) - \lambda_{\rm res}(\infty)}, \text{ where } \lambda_{\rm res}(N_{\rm tr}) \text{ is the residual stretch ratio at cycle } N_{\rm tr}, \lambda_{\rm res}(\infty) \text{ is the}$$

residual stretch ratio at the steady state of training (**fig. S8B**). $\lambda_{res}(0) = 1$ denotes the λ_{res} at undeformed state. The $R(N_{tr})$ denotes the relative training effect away from the steady state. Thus, the Prony series for fitting $R(N_{tr})$ is rewritten as

$$R(N_{tr}) = R_{\infty} + \sum_{i=1}^{n} R_{i} e^{-N_{tr}/N_{i}}$$
(S2)

Where R_{∞} is close to 0 since $N_{tr} = 10^4$ already reaches the steady state, R_i are training strengths for λ_{res} , and N_i are the characteristic training cycles of λ_{res} . **Fig. S8C** shows an example of the fitting result ($\lambda_{tr} = 2.9$) using n = 3. The obtained characteristic training cycles are $N_1 = 1$, $N_2 = 19$, and $N_3 = 962$, with the fitting parameters $R_1 = 0.51$, $R_2 = 0.27$, $R_3 = 0.21$, and $R_{\infty} = 0.01$.

The characteristic training cycles N_i of λ_{res} for s-PA gel are shown in **Fig. 3B**, and the corresponding fitting parameters are shown in **fig. S8D**. As expected, the R_{∞} is close to 0. The training strength of the first term R_1 , corresponding to $N_1 \approx 1$, has a largest value than others as the first training cycle induces a large λ_{res} by breaking the ionic bonds and elongating polymer network. R_1 decreases while the second and third term R_2 , R_3 increase slightly with λ_{tr} at $\lambda_{tr} < \lambda_{affine}$. This could be correlated to a higher oriented phase networks formed at larger λ_{tr} , and the contribution from the long-term adaptation increasing. At $\lambda_{affine} < \lambda_{tr} < \lambda_c$, all the parameters almost keep constant due to the damage of the hard phase network.



Fig. S8. Evolution of residual stretch ratio (λ_{res}) with training cycle N_{tr} of s-PA gel and the Prony series fitting. (A) The residual stretch ratio λ_{res} versus N_{tr} for the samples trained at varied λ_{tr} . (B) λ_{res} at the steady state of training ($\lambda_{res}(\infty)$) as a function of λ_{tr} . (C) Prony series fitting of normalized λ_{res} . Here $\lambda_{tr} = 2.9$ is taken as an example. The λ_{res} is normalized as $R(N_{tr}) = \frac{\lambda_{res}(N_{tr}) - \lambda_{res}(\infty)}{\lambda_{res}(0) - \lambda_{res}(\infty)}$. The $\lambda_{res}(0) = 1$ denotes the λ_{res} at the undeformed state. (D) The Prony

series fitting parameter R_i and R_{∞} as a function of λ_{tr} . The vertical dotted line indicates λ_{affine} . The dashed lines are a guide for the eyes. The error bar ($\lambda_{tr} = 2.1$ to 3.7) is SE from at least three measurements.



Fig. S9. The characteristic training cycles of hysteresis energy density U_{hys} of s-PA gel as a function of λ_{tr} . The U_{hys} versus N_{tr} profiles are fitted by $U_{hys}(N_{tr}) = U_{hys}, + \sum_{i=1}^{n} U_{hys}, e^{-N_{tr}/N_i}$, where

 $U_{hys}(N_{tr})$ is the U_{hys} (the area between the load and unload curves) at the cycle N_{tr} , $U_{hys,\infty}$ is the U_{hys} in the steady state of cyclic loading, N_i are the characteristic training cycles, $U_{hys,i}$ are training strengths, and *n* is the series order, n = 3. The vertical dotted line indicates λ_{affine} . The error bar ($\lambda_{tr} = 2.1$ to 3.7) is SE from at least three measurements.

Section S3. The Prony series fitting of detraining curves

Detraining experiment is performed by resting the trained sample at 24 °C for varied time $t_{rest.}$ As schemed in **fig. S10A**, the trained s-PA gels (trained at λ_{tr} for $N_{tr} = 10^4$ cycles) are allowed to rest at a strain-free state for different times t_{rest} , then are loaded to λ_{tr} to detect the self-recovery efficiency. The longest t_{rest} we tracked are 87 ks for $\lambda_{tr} < 4.1$, and 500 ks for $\lambda_{tr} > 4.1$ (ks means 1000 seconds). We find that the change of mechanical behavior during rest is similar to detraining of muscles, that the temporary memories formed during training process are gradually forgotten during rest. As an example, Fig. 2C shows the loading-unloading curves at trest after the sample being trained at $\lambda_{tr} = 3.7$ for $N_{tr} = 10^4$. The gel self-recovers to its original length, showing no residual strain ($\lambda_{res} = 1$) after resting for $t_{rest} = 25$ ks, while the softening of stress and loss of hysteresis loop still slightly remain after resting for 87 ks. Then, we systematically study the effect of training intensity (λ_{tr}) on the relaxation dynamics when the training duration is fixed at $N_{tr} = 10^4$. Fig. S10B plots the normalized work of extension $W_{ex}(t_{rest})/W_{ex0}$ as a function of t_{rest} for several representative λ_{tr} , $\lambda_{tr} = 2.9$, 3.7 and 7.1. Note that the $\lambda_{tr} = 2.9$ is smaller than the λ_{affine} , $\lambda_{tr} = 3.7$ is above the λ_{affine} , and $\lambda_{tr} = 7.1$ is far beyond the λ_{affine} . It shows that $W_{ex}(t_{rest})/W_{ex0}$ increases rapidly at the beginning of rest and gradually approaches to 0.9, 0.8 and 0.6 for $\lambda_{tr} = 2.9$, 3.7 and 7.1, respectively, after a long t_{rest}. In contrast, the residual stretch ratios $\lambda_{res}(t_{rest})$ of all the trained samples recover to 1 during the rest process in our observation time scale (fig. S11A). These detraining curves show that detraining dynamics become slower after suffering a higher training intensity λ_{tr} .

To clarify the difference in dynamics between the $W_{ex}(t_{rest})$ and $\lambda_{res}(t_{rest})$ during detraining, we also use the Prony series to fit the detraining curves. First, the Prony series is used to fit the normalized $W_{ex}(t_{rest})$, that is $w(t_{rest}) = \frac{W_{ex}(t_{rest}) - W_{ex0}}{W_{\infty} - W_{ex0}}$, where W_{ex0} and W_{∞} are the W_{ex} of the first

loading and equilibrium W_{ex} in training at λ_{tr} , respectively. The $w(t_{rest}) = 1$ means no detraining,

and $w(t_{rest}) = 0$ means full recovery during rest. To fit the normalized $w(t_{rest})$, the Prony series is rewritten

$$w(t_{rest}) = w_{\infty} + \sum_{i=1}^{n} w_i e^{-t_{rest}/\tau_{f,i}}$$
(S3)

where w_{∞} is the ratio of irrecoverable part within the maximum observation t_{rest} , w_i are detraining strengths of $W_{\text{ex}}(t_{\text{rest}})$, and $\tau_{\text{f,i}}$ are characteristic detraining times, correlated to the forgetting rate of the training effect. Same as the fitting applied in training process, the series order n = 3 is used. Taking the gel trained at $\lambda_{\text{tr}} = 3.7$ for $N_{\text{tr}} = 10^4$ as an example, **fig. S10C** shows that n = 3 gives an excellent fitting ($\mathbb{R}^2 = 0.999$) for the detraining curve. The characteristic detraining times are $\tau_{\text{f,1}} =$ 42.8 s, $\tau_{\text{f,2}} = 916.4$ s, and $\tau_{\text{f,3}} = 12170.9$ s with the detraining parameters $w_1 = 0.11$, $w_2 = 0.17$, $w_3 =$ 0.42, and $w_{\infty} = 0.29$.

The detraining curves of $W_{ex}(t_{rest})$ of the gels trained at varied λ_{tr} were fitted by **Eq. S3**. The detraining strength w_i is shown in **fig. S10D**, and the characteristic detraining times $\tau_{f,1}$, $\tau_{f,2}$, $\tau_{f,3}$ of $W_{ex}(t_{rest})$ as a function of λ_{tr} is shown in **fig. S10E**. The w_i slightly decrease with λ_{tr} , and have an order of $w_3 > w_2 > w_1$, indicating that the long-term relaxation due to the mesoscale phase networks contributes more than the short-term relaxation due to the transient network. Expectedly, the irrecoverable term w_{∞} increases with λ_{tr} at $\lambda_{affine} < \lambda_{tr} < \lambda_c$, indicating an increased damage of the hard phase network.



Fig. S10. Prony series fitting of $W_{ex}(t_{rest})$ versus t_{rest} curves of detraining process for s-PA gel. (A) Experimental protocol for detraining. After resting for t_{rest} , the trained gels (trained at λ_{tr} for $N_{tr} = 10^4$ cycles) are reloaded to the corresponding λ_{tr} to detect the recovery efficiency. (B) Evolution of $W_{ex}(t_{rest})/W_{ex0}$ as a function of rest time t_{rest} after cyclic training under $\lambda_{tr} = 2.9$, 3.7 and 7.1 for $N_{tr} = 10^4$. Inset shows the logarithm plots. (C) Prony series fitting of normalized $W_{ex}(t_{rest})$. Here $\lambda_{tr} = 3.7$ for $N_{tr} = 10^4$ is taken as an example. The $W_{ex}(t_{rest})$ is normalized as $w(t_{rest}) = \frac{W_{ex}(t_{rest}) - W_{ex0}}{W_{\infty} - W_{ex0}}$, where $W_{ex}(t_{rest})$ is the W_{ex} for deforming the trained gel to the

corresponding λ_{tr} after resting for t_{rest} . W_{ex0} and W_{∞} are the W_{ex} of the first loading and equilibrium W_{ex} for training at λ_{tr} , respectively. The w(t_{rest}) versus t_{rest} denotes forgetting curve. (**D**) The Prony series parameters w_i and w_{∞} versus λ_{tr} . (**E**) The characteristic detraining time (forgetting time) $\tau_{f,1}$, $\tau_{f,2}$, and $\tau_{f,3}$ of $W_{ex}(t_{rest})$ as a function of λ_{tr} . The vertical dotted line indicates λ_{affine} . The dashed lines are a guide for the eyes. The error bar ($\lambda_{tr} = 2.1$ to 3.7) is SE from at least three measurements.

Then, the Prony series is used to fit the detraining process of the normalized $\lambda_{res}(t_{rest})$, which is

$$R_f(t_{rest}) = \frac{\lambda_{res}(t_{rest})}{\lambda_{res}(\infty)}$$
. Now the Prony series is rewritten as

$$R_{f}(t_{rest}) = \sum_{i=1}^{n} R_{f,i} e^{-t_{rest}/\tau_{f,i}}$$
(S4)

Note that, due to all the $\lambda_{res}(t_{rest})$ can recover to pristine state, there is no infinity term in **Eq. S4**. $R_{f,i}$ are the detraining strengths of $\lambda_{res}(t_{rest})$, and $\tau_{f,i}$ are the characteristic detraining time of $\lambda_{res}(t_{rest})$. **Figure S11B** shows one example of the fitting result of normalized residual stretch ratio $R_f(t_{rest})$ at $\lambda_{tr} = 3.7$ using n = 3. The good fitting ($R^2 = 0.994$) gives characteristic detraining times $\tau_{f,1} = 1$ s, $\tau_{f,2} = 119.9$ s, and $\tau_{f,3} = 4630.9$ s with the detraining parameters $R_{f,1} = 0.34$, $R_{f,2} = 0.28$, $R_{f,3} = 0.36$.

The detraining curves of $\lambda_{res}(t_{rest})$ of the gel trained at varied λ_{tr} were fitted by **Eq. S4**. The detraining strengths $R_{f,i}$ are shown in **fig. S11C** and the characteristic detraining times $\tau_{f,1}$, $\tau_{f,2}$, $\tau_{f,3}$ of $\lambda_{res}(t_{rest})$ as a function of λ_{tr} is shown in **fig. S11D**. The three fitting parameters $R_{f,i}$ have a similar value (around 0.3), and depend little on the training λ_{tr} . This indicates that the structures with varied length scales almost contribute equal to the detraining strengths of λ_{res} .



Fig. S11. Prony series fitting of $\lambda_{res}(t_{rest})$ versus t_{rest} curves of detraining process for s-PA gel. (A) Evolution of $\lambda_{res}(t_{rest})$ as a function of rest time t_{rest} after cyclic training under $\lambda_{tr} = 2.9$, 3.7 and 7.1 for $N_{tr} = 10^4$. Inset shows the logarithm plots. (B) Prony series fitting of normalized $\lambda_{res}(t_{rest})$. Here $\lambda_{tr} = 3.7$ for $N_{tr} = 10^4$ is taken as an example. The $\lambda_{res}(t_{rest})$ is normalized as $R_f(t_{rest}) = \frac{\lambda_{res}(t_{rest})}{\lambda_{res}(\infty)}$,

where $\lambda_{res}(t_{rest})$ is the λ_{res} at rest time t_{rest} , and $\lambda_{res}(\infty)$ is the equilibrium λ_{res} in the training process. (**C**) The Prony series parameters $R_{f,i}$ as a function of λ_{tr} . (**D**) The characteristic detraining time (forgetting time) $\tau_{f,1}$, $\tau_{f,2}$, and $\tau_{f,3}$ of $\lambda_{res}(t_{rest})$ as a function of λ_{tr} . The vertical dotted line indicates λ_{affine} . The dashed lines are a guide for the eyes. The error bar ($\lambda_{tr} = 2.1$ to 3.7) is SE from at least three measurements.



Fig. S12. Effect of training duration N_{tr} **on detraining dynamics of s-PA gel.** (A) The W_{ex}/W_{ex0} and (B) the residual stretch ratio λ_{res} in cyclic training and detraining as a function of time (both training and rest time). Training at fixed $\lambda_{tr} = 3.7$ for $N_{tr} = 200$, 2000, 10⁴ are taken as examples. Cyclic training is plotted by spheres and the detraining process is plotted by open symbols. The arrows indicate the points at which the samples are allowed to rest, and the corresponding N_{tr} are shown next to each detraining curve. (C) Evolution of $W_{ex}(t_{rest})/W_{ex0}$ as a function of rest time t_{rest} . The data is extracted from (A). (D) Evolution of $\lambda_{res}(t_{rest})$ as a function of rest time t_{rest} . The data is extracted from (B). (E) The characteristic detraining time (forgetting time) $\tau_{j.1}$, $\tau_{j.2}$, and $\tau_{j.3}$ of $W_{ex}(t_{rest})$ versus N_{tr} . **Eq. S3** is used for fitting the $W_{ex}(t_{rest})$ versus N_{tr} . **Eq. S4** is used for fitting the $\lambda_{res}(t_{rest})$ curves of detraining at $\lambda_{tr} = 2.9$ for varied N_{tr} and the spheres denote training at $\lambda_{tr} = 3.7$ for varied N_{tr} . The characteristic detraining time $\tau_{f.1}$, $\tau_{f.2}$, and $\tau_{f.3}$ of both $W_{ex}(t_{rest})$ and $\lambda_{res}(t_{rest})$ indicate that $N_{tr} \ge 1000$ is required for saturated training.



Fig. S13. Loading-unloading curves of the unnotched s-PA samples during cyclic training under $\lambda_{tr} = 2.9$ (< λ_{affine}) and $\lambda_{tr} = 3.7$ (> λ_{affine}).



Fig. S14. Crack tip profiles of s-PA gels during fatigue test at $\lambda_{\text{fatigue}} = 2.9$ after trained at varied conditions and the radius of curvature at the crack tip (*R*). The data is extracted from Fig. 4B. X = 0 denotes the position of pre-cut perpendicular to loading direction, and Y = 0 denotes the center of crack along the loading direction. The radius of curvature at the crack tip *R* is obtained $\frac{|(1+X')^{3/2}|}{|(1+X')^{3/2}|} = \frac{dX}{d^2X}$

at
$$Y \approx 0$$
 by $R = \left| \frac{(1+X')}{X''} \right|$, where $X' = \frac{dX}{dY}$ and $X'' = \frac{d^2X}{dY^2}$

Section S4. Direct fatigue test

For the direct fatigue test, the pre-notched s-PA gel with the pure shear geometry (inset of **fig. 15A**) was used. Consecutive cyclic loading without interval between cycles was performed at preset λ_{fatigue} . The crack propagation with cycles is recorded as *c*. Self-training effect is observed at $\lambda_{\text{fatigue}} \leq \lambda_{\text{tran}}$ while overtraining happens at $\lambda_{\text{fatigue}} > \lambda_{\text{tran}}$. The former shows that the stress concentration gradually weakens with cycle number N_{fatigue} (**fig. S15B**), whereas the latter shows that the crack tip always has severe stress concentration (**fig. S15C**). The $\lambda_{\text{tran}} = 3.1$ ($\approx \lambda_{\text{affine}}$) is the slow-to-fast crack propagation transition stretch ratio in the direct fatigue test as indicated in our previous work (*49*).



Fig. S15. Self-training and overtraining effect in direct fatigue test using pre-notched s-PA samples. (A) Fatigue behavior of the pristine notched gel (inset, $L_0 = 50 \text{ mm}$, $H_0 = 10 \text{ mm}$, and $c_0 = 10 \text{ mm}$) at $\lambda_{\text{fatigue}} = 2.7 < \lambda_{\text{tran}}$ and $\lambda_{\text{fatigue}} = 3.5 > \lambda_{\text{tran}}$. Typical evolution of birefringence images with cycle number N_{fatigue} at $\lambda_{\text{fatigue}} = 2.7$ (B) and $\lambda_{\text{fatigue}} = 3.5$ (C).



Fig. S16. Mechanical adaptation of s-PA gel under stepwise cyclic stretching. (A) Experiment proposal for training. One piece of s-PA gel undergoes the following training protocol. Initially, it is subjected to cyclic loading at a preset $\lambda_{tr} = 2.9$ for $N_{tr} = 5000$ cycles. Subsequently, the λ_{tr} is increased to $\lambda_{tr} = 3.7$ and the sample undergoes an additional $N_{tr} = 5000$ cycles. Finally, the λ_{tr} is reduced back $\lambda_{tr} = 2.9$ for cyclic training. The corresponding (B) strain energy density obtained from the loading curves (W_{ex}) and (C) the residual stretch ratio (λ_{res}). We can see that both the W_{ex} and λ_{res} can rapidly adapt to the mechanical training. Notably, at the two $\lambda_{tr} = 2.9$, the W_{ex} and λ_{res} exhibit similar values in the steady state, despite having different training histories.

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