



# HOKKAIDO UNIVERSITY

|                  |                                                                                   |
|------------------|-----------------------------------------------------------------------------------|
| Title            | Stresses in Multi Layered Systems                                                 |
| Author(s)        | Yoshimura, Jin; Ushio, Shunsuke; Sugawara, Teruo                                  |
| Citation         | Memoirs of the Faculty of Engineering, Hokkaido University, 13(2), 75-89          |
| Issue Date       | 1972-03                                                                           |
| Doc URL          | <a href="https://hdl.handle.net/2115/37882">https://hdl.handle.net/2115/37882</a> |
| Type             | departmental bulletin paper                                                       |
| File Information | 13(2)_75-90.pdf                                                                   |



# Stresses in Multi Layered Systems

Jin YOSHIMURA\*

Shunsuke USHIO\*

Teruo SUGAWARA\*

## Abstract

The analysis of elastic layered systems is required for the design and analysis of flexible pavements or rock mechanics. This paper presents a general analysis of three layered systems due to a variety of surface loading conditions and shows some numerical examples including a principal stress analysis.

## 1. Introduction

The analysis of stresses and displacements in a semi infinite elastic solid with a vertical surface load was originally established by Boussinesq.

Burmister<sup>1)</sup>, Fox<sup>2)</sup>, Jelinek<sup>3)</sup> and others gave some solutions for a two layered systems and Acum<sup>4)</sup> and Fox analyzed three layered systems under a uniformly distributed normal load. These solutions, however, are only for a limited case, that is, stresses and displacements in a vertical axis through a center of the normally distributed circular surface load ( $r=0$ ) and in an interface between layers.

Snedden<sup>5)</sup> has presented a method of analysis by integral transforms (Hankel transforms) for three dimensional problems in the theory of elasticity and successfully used to determine the distribution of stresses in a semi infinite solid and other interesting problems under various loading conditions. This method is, however, restricted to the axisymmetric case.

Muki<sup>5)</sup> has extended and generalized Sneddon's method for the axisymmetric problems of the theory of elasticity to the asymmetric problems. This method is applicable to the analysis of layered systems. Schiffman<sup>7)</sup> has applied Muki's method to several interesting problems.

This paper presents a general solution for the three layered systems. Stresses and displacements in any point of layered systems under a vertical and tangential load on its surface were obtained.

## 2. General Solutions

In an asymmetric cylindrical coordinate systems the stress tensor is

$$\sigma_{pq}^i(r, \theta, z) = \begin{bmatrix} \sigma_{rr}^i & \sigma_{r\theta}^i & \sigma_{rz}^i \\ \sigma_{r\theta}^i & \sigma_{\theta\theta}^i & \sigma_{\theta z}^i \\ \sigma_{rz}^i & \sigma_{\theta z}^i & \sigma_{zz}^i \end{bmatrix} \quad (1)$$

and components of stresses are shown in Fig. 1.

The displacement vector is

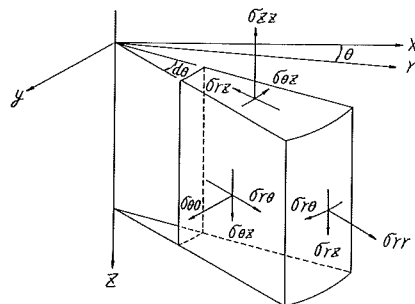


Fig. 1. Components of stresses in cylindrical coordinate

\* Department of Civil Engineering, Faculty of Engineering, Hokkaido University, Sapporo, Japan.

$$u_p^i = \begin{bmatrix} u_r^i \\ u_\theta^i \\ u_z^i \end{bmatrix}. \quad (2)$$

The index ( $i$ ) refers to the layer for which the stresses and displacements are being determined.

The equations of equilibrium in terms of the displacements,  $u_r$ ,  $u_\theta$ ,  $u_z$  in the  $r$ ,  $\theta$  and  $z$  directions are

$$\left. \begin{aligned} \nabla^2 u_r + \frac{1}{1-2\nu} \frac{\partial \Delta}{\partial r} - \frac{1}{r} \left( 2 \frac{\partial u_\theta}{r \cdot \partial \theta} + \frac{u_r}{r} \right) &= 0 \\ \nabla^2 u_\theta + \frac{1}{1-2\nu} \frac{\partial \Delta}{r \partial \theta} - \frac{1}{r} \left( \frac{u_\theta}{r} - 2 \frac{1}{r} \frac{\partial u_r}{\partial \theta} \right) &= 0 \\ \nabla^2 u_z + \frac{1}{1-2\nu} \frac{\partial \Delta}{\partial z} &= 0, \end{aligned} \right\} \quad (3)$$

where  $\nabla^2$  and  $\nu$  denote the Laplacian operator and Poisson's ratio respectively, and  $\Delta$  is

$$\Delta = \frac{\partial u_r}{\partial r} + \frac{u_r}{r} + \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{\partial u_z}{\partial z}. \quad (4)$$

Equations of equilibrium (3) are satisfied if we take in  $i$ th layer by defining stress functions  $\Phi_i$  and  $\Psi_i$  for each layer,

$$\left. \begin{aligned} u_r^i &= \frac{1+\nu_i}{E_i} \left\{ -\frac{\partial^2 \Phi_i}{\partial r \partial z} + \frac{2}{r} \frac{\partial \Psi_i}{\partial \theta} \right\} \\ u_\theta^i &= \frac{1+\nu_i}{E_i} \left\{ -\frac{1}{r} \frac{\partial^2 \Phi_i}{\partial \theta \partial z} - 2 \frac{\partial \Psi_i}{\partial r} \right\} \\ u_z^i &= \frac{1+\nu_i}{E_i} \left\{ 2(1-\nu_i) \nabla^2 \Phi_i - \frac{\partial^2 \Psi_i}{\partial z^2} \right\}, \end{aligned} \right\} \quad (5)$$

where,

$$\nabla^4 \Phi_i = 0, \quad \nabla^2 \Psi_i = 0. \quad (6)$$

The components of stresses in each layer are:

$$\left. \begin{aligned} \sigma_{rr}^i &= \frac{\partial}{\partial z} \left\{ \nu_i \nabla^2 \Phi_i - \frac{\partial^2 \Phi_i}{\partial r^2} \right\} + \frac{2}{r} \frac{\partial}{\partial \theta} \left\{ \frac{\partial \Psi_i}{\partial r} - \frac{1}{r} \Psi_i \right\} \\ \sigma_{\theta\theta}^i &= \frac{\partial}{\partial z} \left\{ \nu_i \nabla^2 \Phi_i - \frac{1}{r^2} \frac{\partial^2 \Phi_i}{\partial \theta^2} - \frac{1}{r} \frac{\partial \Phi_i}{\partial r} \right\} - \frac{2}{r} \frac{\partial}{\partial \theta} \left\{ \frac{\partial \Psi_i}{\partial r} - \frac{1}{r} \Psi_i \right\} \\ \sigma_{zz}^i &= \frac{\partial}{\partial z} \left\{ (2-\nu_i) \nabla^2 \Phi_i - \frac{\partial^2 \Phi_i}{\partial z^2} \right\} \\ \sigma_{r\theta}^i &= \frac{1}{r} \frac{\partial^2}{\partial \theta \partial z} \left\{ \frac{\Phi_i}{r} - \frac{\partial \Phi_i}{\partial r} \right\} - 2 \frac{\partial^2 \Psi_i}{\partial r^2} - \frac{\partial^2 \Psi_i}{\partial z^2} \\ \sigma_{\theta z}^i &= \frac{1}{r} \frac{\partial}{\partial \theta} \left\{ (1-\nu_i) \nabla^2 \Phi_i - \frac{\partial^2 \Phi_i}{\partial z^2} \right\} - \frac{\partial^2 \Psi_i}{\partial r \cdot \partial z} \\ \sigma_{rz}^i &= \frac{\partial}{\partial r} \left\{ (1-\nu_i) \nabla^2 \Phi_i - \frac{\partial^2 \Phi_i}{\partial z^2} \right\} + \frac{1}{r} \frac{\partial^2 \Psi_i}{\partial \theta \cdot \partial z}. \end{aligned} \right\} \quad (7)$$

The steress functions  $\Phi_i$  and  $\Psi_i$  can be written in the following forms,

$$\left. \begin{aligned} \Phi_i(r, \theta, z) &= \sum_{n=0}^{\infty} \Phi_n^i(r, z) \cos n\theta \\ \Psi_i(r, \theta, z) &= \sum_{n=0}^{\infty} \Psi_n^i(r, z) \sin n\theta. \end{aligned} \right\} \quad (8)$$

$\Phi_n^i$  and  $\Psi_n^i$  are the solutions of the following partial differential equations

$$\nabla_n^4 \Phi_n^i = \left( \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} - \frac{n^2}{r^2} + \frac{\partial^2}{\partial z^2} \right)^2 \Phi_n^i = 0 \quad (9)$$

$$\nabla_n^2 \Psi_n^i = \left( \frac{\partial}{\partial r} + \frac{1}{r} \frac{\partial}{\partial r} - \frac{n^2}{r^2} + \frac{\partial^2}{\partial z^2} \right) \Psi_n^i = 0. \quad (10)$$

Applying Hankel transform to Eq. (9) and (10), we have

$$\int_0^{\infty} r \nabla_n^4 \Phi_n^i J_n(mr) dr = \left( \frac{d^2}{dz^2} - m^2 \right)^2 \int_0^{\infty} r \Phi_n^i J_n(mr) dr = 0 \quad (11)$$

$$\int_0^{\infty} r \nabla_n^2 \Psi_n^i J_n(mr) dr = \left( \frac{d^2}{dz^2} - m^2 \right) \int_0^{\infty} r \Psi_n^i J_n(mr) dr = 0. \quad (12)$$

If we write,

$$G_n^i(m, z) = \int_0^{\infty} r \Phi_n^i(r, z) J_n(mr) dr \quad (13)$$

$$H_n^i(m, z) = \int_0^{\infty} r \Psi_n^i(r, z) J_n(mr) dr \quad (14)$$

where,  $J_n(mr)$  is  $n^{\text{th}}$  Bessel function,

Hankel transforms  $G_n^i$  and  $H_n^i$  must be the solutions of the ordinary differential equations

$$\left( \frac{d^2}{dz^2} - m^2 \right)^2 G_n^i(m, z) = 0, \quad (15)$$

$$\left( \frac{d^2}{dz^2} - m^2 \right) H_n^i(m, z) = 0. \quad (16)$$

The general solutions of Eq. (15) and (16) are :

$$G_n^i(m, z) = \{A_n^i(m) + B_n^i(m) \cdot z\} e^{-mz} + \{C_n^i(m) + D_n^i(m) \cdot z\} e^{mz} \quad (17)$$

$$H_n^i(m, z) = E_n^i(m) e^{-mz} + F_n^i(m) e^{mz} \quad (18)$$

where the arbitrary constants  $A_n^i(m) \dots F_n^i(m)$  are to be determined from the given boundary conditions on the surface and interface between layers. Once these constants have been determined,  $G_n^i$  and  $H_n^i$  are known functions of  $z$  and of the parameter  $m$ , and the expressions for  $\Phi_n^i$  and  $\Psi_n^i$  may then be obtained by means of the Hankel inversion theorem

$$\Phi_n^i(r, z) = \int_0^{\infty} m G_n^i(m, z) J_n(mr) dm \quad (19)$$

$$\Psi_n^i(r, z) = \int_0^{\infty} m H_n^i(m, z) J_n(mr) dm. \quad (20)$$

Next, transformations of expressions for the displacements and stress components into relations including  $G_n^i$ ,  $H_n^i$  and their derivatives are required. These results are as follows,

$$\left. \begin{aligned}
 u_r^i &= \frac{1+\nu_i}{2E_i} \sum_{n=1}^{\infty} \left\{ U_{n+1}^i - V_{n-1}^i \right\} \cos n\theta \\
 u_\theta^i &= \frac{1+\nu_i}{2E_i} \sum_{n=0}^{\infty} \left\{ U_{n+1}^i + V_{n-1}^i \right\} \sin n\theta \\
 u_z^i &= \frac{1+\nu_i}{2E_i} \sum_{n=0}^{\infty} \left\{ \int_0^{\infty} m \left[ (1-2\nu_i) \frac{d^2 G_n^i}{dz^2} - 2(1-\nu_i) m^2 G_n^i \right] J_n(mr) dm \right\} \cos n\theta \\
 \sigma_{rr}^i &= \sum_{n=0}^{\infty} \left\{ \int_0^{\infty} m \frac{dW_n^i}{dz} J_n(mr) dm - \frac{n+1}{2r} U_{n+1}^i - \frac{n-1}{2r} V_{n-1}^i \right\} \cos n\theta \\
 \sigma_{\theta\theta}^i &= \sum_{n=0}^{\infty} \left\{ \nu_i \int_0^{\infty} m \left[ \frac{d^3 G_n^i}{dz^3} - m^2 \frac{dG_n^i}{dz} \right] J_n(mr) dm + \frac{n+1}{2r} U_{n+1}^i + V_{n-1}^i \right\} \cos n\theta \\
 \sigma_{zz}^i &= \sum_{n=0}^{\infty} \left\{ \int_0^{\infty} m \left[ (1-\nu_i) \frac{d^3 G_n^i}{dz^3} - (2-\nu_i) m^2 \frac{dG_n^i}{dz} \right] J_n(mr) dm \right\} \cos n\theta \\
 \sigma_{r\theta}^i &= \sum_{n=0}^{\infty} \left\{ \int_0^{\infty} m^3 H_n^i J_n(mr) dm - \frac{n+1}{2r} U_{n+1}^i + \frac{n-1}{2r} V_{n-1}^i \right\} \sin n\theta \\
 \sigma_{\theta z}^i &= \frac{1}{2} \sum_{n=0}^{\infty} \left\{ \int_0^{\infty} m^2 \left[ W_n^i + \frac{dH_n^i}{dz} \right] J_{n+1}(mr) dr + \right. \\
 &\quad \left. + \int_0^{\infty} m^2 \left[ W_n^i - \frac{dH_n^i}{dz} \right] J_{n-1}(mr) dm \right\} \sin n\theta \\
 \sigma_{rz}^i &= \frac{1}{2} \sum_{n=0}^{\infty} \left\{ \int_0^{\infty} m^2 \left[ W_n^i + \frac{dH_n^i}{dz} \right] J_{n+1}(mr) dm - \right. \\
 &\quad \left. - \int_0^{\infty} m^2 \left[ W_n^i - \frac{dH_n^i}{dz} \right] J_{n-1}(mr) dm \right\} \cos n\theta
 \end{aligned} \right\} \quad (21)$$

where

$$\left. \begin{aligned}
 U_{n+1}^i &= \int_0^{\infty} m^2 \left[ \frac{dG_n^i}{dz} + 2H_n^i \right] J_{n+1}(mr) dm \\
 V_{n-1}^i &= \int_0^{\infty} m^2 \left[ \frac{dG_n^i}{dz} - 2H_n^i \right] J_{n-1}(mr) dm \\
 W_n^i &= \nu_i \frac{d^2 G_n^i}{dz^2} + (1-\nu_i) m^2 G_n^i
 \end{aligned} \right\} \quad (22)$$

### 3. Stresses and displacements in three layered systems under normally distributed circular loading on its surface

The solution of a layered system problem consists of determining the constants  $A_n^i$  through  $F_n^i$  for each layer. This will determine the functions  $G_n^i$  and  $H_n^i$  for each layer. Then, stresses are determined by Eq. (21).

For the boundary conditions and continuity conditions, transformed stresses and transformed surface load are used.

In the case of axisymmetric normal load as shown in Fig. 2, we can put  $n=0$ , and  $H_n^z$  vanishes.

The surface loading conditions are

$$\left. \begin{aligned} \sigma_{zz}^1(r, \theta) &= -p(r) & 0 \leq r \leq a \\ \sigma_{zz}^1(r, \theta) &= 0 & r > a \\ \sigma_{rz}^1(r, \theta) &= 0 & 0 \leq r < \infty \end{aligned} \right\} \quad (23)$$

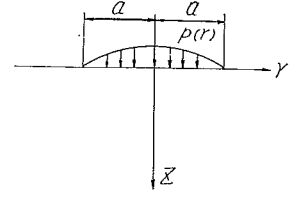


Fig. 2.

In the case of  $p(r)=p_0=\text{const.}$ , transformed surface load is

$$\begin{aligned} M(m) &= -\int_0^\infty r p(r) J_0(mr) dr \\ &= -p_0 \int_0^\infty r J_0(mr) dr = -\frac{p_0 a}{m} J_1(ma). \end{aligned} \quad (24)$$

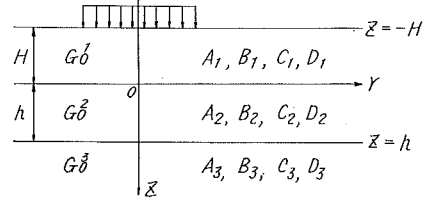


Fig. 3.

A coordinate system for the three layered system are shown in Fig. 3. In the case of flexible loading, boundary conditions at an interface are as follows,

$$\left. \begin{aligned} \text{for } z = -H: & \quad \sigma_{zz}^1 = M(m), & \sigma_{rz}^1 &= 0 \\ \text{for } z = 0: & \quad \sigma_{zz}^1 = \sigma_{zz}^2, & \sigma_{rz}^1 &= \sigma_{rz}^2 \\ & \quad u_z^1 = u_z^2, & u_r^1 &= u_r^2 \\ \text{for } z = h: & \quad \sigma_{zz}^2 = \sigma_{zz}^3, & \sigma_{rz}^2 &= \sigma_{rz}^3 \\ & \quad u_z^2 = u_z^3, & u_r^2 &= u_r^3. \end{aligned} \right\} \quad (25)$$

As the third layer is semi-infinite, the stresses and displacements must vanish at infinity. This condition is accomplished if

$$C_n^3 = D_n^3 = 0. \quad (26)$$

These conditions (25) are represented by the following equations.

$$\left. \begin{aligned} m^3 A_1 e^{mH} + (1 - 2\nu_1 - mH) m^2 B_1 e^{mH} - m^3 C_1 e^{-mH} + \\ + (1 - 2\nu_1 + mH) m^2 D_1 e^{-mH} &= M(m) \\ m^3 A_1 e^{mH} - (2\nu_1 + mH) m^2 B_1 e^{mH} + m^3 C_1 e^{-mH} + (2\nu_1 - mH) m^2 D_1 e^{-mH} &= 0 \\ m^3 A_1 + (1 - 2\nu_1) m^2 B_1 - m^3 C_1 + (1 - 2\nu_1) m^2 D_1 &= \\ = m^3 A_2 + (1 - 2\nu_2) m^2 B_2 - m^3 C_2 + (1 - 2\nu_2) m^2 D_2 & \\ m^3 A_2 e^{-mh} + (1 - 2\nu_2 + mh) m^2 B_2 e^{-mh} - m^3 C_2 e^{mh} + (1 - 2\nu_2 - mh) m^2 D_2 e^{mh} &= \\ = m^3 A_3 e^{-mh} + (1 - 2\nu_3 + mh) m^2 B_3 e^{-mh} - m^3 C_3 e^{mh} + (1 - 2\nu_3 - mh) m^2 D_3 e^{mh} & \\ m^3 A_1 - (2\nu_1 m^2 B_1) + m^3 C_1 + 2\nu_1 m^2 D_1 = m^3 A_2 - 2\nu_2 m^2 B_2 + m^3 C_2 + 2\nu_2 m^2 D_2 & \\ m^3 A_2 e^{-mh} - (2\nu_2 - mh) m^2 B_2 e^{-mh} + m^3 C_2 e^{mh} + (2\nu_2 + mh) m^2 D_2 e^{mh} = & \\ = m^3 A_3 e^{-mh} - (2\nu_3 - mh) m^2 B_3 e^{-mh} + m^3 C_3 e^{mh} + (2\nu_3 + mh) m^2 D_3 e^{mh} & \\ \frac{1 + \nu_1}{E_1} \left\{ -m^2 A_1 - (2m - 4m\nu_1) B_1 - m^2 C_1 + (2m - 4m\nu_1) D_1 \right\} = & \end{aligned} \right\} \quad (27)$$

$$\begin{aligned}
&= \frac{1+\nu_2}{E_2} \left\{ -m^2 A_2 - (2m - 4m\nu_2) B_2 - m^2 C_2 + (2m - 4m\nu_2) D_2 \right\} \\
&\frac{1+\nu_2}{E_2} \left\{ -m^2 A_2 e^{-m\hbar} - (2m + m^2\hbar - 4m\nu_2) B_2 e^{-m\hbar} - m^2 C_2 e^{m\hbar} + (2m - m^2\hbar - \right. \\
&\quad \left. - 4m\nu_2) D_2 e^{m\hbar} \right\} = \frac{1+\nu_3}{E_3} \left\{ -m^2 A_3 e^{-m\hbar} - (2m + m^2\hbar - 4m\nu_3) B_3 e^{-m\hbar} - \right. \\
&\quad \left. - m^2 C_3 e^{m\hbar} + (2m - m^2\hbar - 4m\nu_3) D_3 e^{m\hbar} \right\} \\
&\frac{m(1+\nu_1)}{E_1} \left\{ -mA_1 + B_1 + mC_1 + D_1 \right\} = \frac{m(1+\nu_2)}{E_2} \left\{ -mA_2 + B_2 + mC_2 + D_2 \right\} \\
&\frac{m(1+\nu_2)}{E_2} \left\{ -mA_2 e^{-m\hbar} + (1 - m\hbar) B_2 e^{-m\hbar} + mC_2 e^{m\hbar} + (1 + m\hbar) D_2 e^{m\hbar} \right\} = \\
&= \frac{m(1+\nu_3)}{E_3} \left\{ -mA_3 e^{-m\hbar} + (1 - m\hbar) B_3 e^{-m\hbar} + mC_3 e^{m\hbar} + (1 + m\hbar) D_3 e^{m\hbar} \right\}.
\end{aligned}$$

Solving these 10 simultaneous equations for  $\nu=0.5$ , the ten constants can be determined and represented in the following,

$$\begin{aligned}
A_1 m^2 = & -\frac{M(m)}{m\Delta} \left\{ (1+mH) e^{mH} - K(1-mH) e^{-mH} + \left[ -N(1+K^2)(1+ \right. \right. \\
& + 2m^2\hbar^2 - mH) + 2mhN(1-K^2)(1-mH) + 4mHm^2\hbar^2 K^2 N \left. \right] e^{-mH-2m\hbar} + \\
& + 2KN(1+2m^2\hbar^2)(1+mH) e^{mH-2m\hbar} - KN^2(1-mH) e^{-mH-4m\hbar} + \\
& \left. + K^2 N^2(1+mH) e^{mH-4m\hbar} \right\} \quad (28.1)
\end{aligned}$$

$$\begin{aligned}
B_1 m = & -\frac{M(m)}{m\Delta} \left\{ e^{mH} - (1-2mH) K e^{-mH} - KN^2(1-2mH) e^{-mH-4m\hbar} + \right. \\
& + 2KN(1+2m^2\hbar^2) e^{mH-2m\hbar} - \left[ N(1-2mH) + K^2 N(1-2mH) - 2Nm\hbar + \right. \\
& \left. + K^2 N(1-2m\hbar) 4m^2\hbar^2 + 2K^2 Nm\hbar \right] e^{-mH-2m\hbar} + K^2 N^2 e^{mH-4m\hbar} \left. \right\} \quad (28.2)
\end{aligned}$$

$$\begin{aligned}
C_1 m^2 = & \frac{M(m)}{m\Delta} \left\{ -K(1+mH) e^{mH} + K^2(1-mH) e^{-mH} + N \left[ (1+K^2)(1+ \right. \right. \\
& + 2m^2\hbar^2 + mH) + 2(1-K^2) mh(1+mH) + 4K^2 m^3 H\hbar^2 \left. \right] e^{mH-2m\hbar} + \\
& + N^2(1-mH) e^{-mH-4m\hbar} + 2KN(1+2m^2\hbar^2)(1-mH) e^{-mH-2m\hbar} - \\
& \left. - KN^2(1+mH) e^{mH-4m\hbar} \right\} \quad (28.3)
\end{aligned}$$

$$\begin{aligned}
D_1 m = & \frac{M(m)}{m\Delta} \left\{ K(1+2mH) e^{mH} - K^2 e^{-mH} + KN^2(1+2mH) e^{mH-4m\hbar} + \right. \\
& + \left[ K^2 N(1+2mH) + K^2 N(1+2mH) 4m^2\hbar^2 + 2Nm\hbar + N(1+2mH) - \right. \\
& \left. - 2K^2 Nm\hbar \right] e^{mH-2m\hbar} - 2KN(1+2m^2\hbar^2) e^{-mH-2m\hbar} - N^2 e^{-mH-4m\hbar} \left. \right\} \quad (28.4)
\end{aligned}$$

$$A_2 m^2 = -\frac{M(m)}{m\Delta} (1-K) \left\{ (1+mH) e^{mH} - K(1-mH) e^{-mH} + KN \times \right.$$

$$\begin{aligned} & \times \left[ 1 - 2mh + 2m^2h^2 + mH(1 - 2mh + 4m^2h^2) \right] e^{mH-2mh} - \\ & - N \left[ 1 - 2mh + 2m^2h^2 - mH(1 - 2mh) \right] e^{-mH-2mh} \Big\} \end{aligned} \quad (28.5)$$

$$\begin{aligned} B_2m = & -\frac{M(m)}{m\Delta} (1-K) \left\{ e^{mH} - K(1-2mH) e^{-mH} + KN \left[ 1 - 2mH(1+2mH) \right] \times \right. \\ & \times e^{mH-2mh} - N(1-2mh-2mH) e^{-mH-2mh} \Big\} \end{aligned} \quad (28.6)$$

$$\begin{aligned} C_2m^2 = & \frac{M(m)}{m\Delta} (1-K) \left\{ -N \left[ (1+2mh)(1+mH) + 2m^2h^2 \right] e^{mH-2mh} + \right. \\ & + N^2(1-mH) e^{-mH-4mh} + KN \left[ 1 + 2mh + 2m^2h^2 - mH(1+2mh+4m^2h^2) \right] \times \\ & \times e^{-mH-2mh} - KN^2(1+mH) e^{mH-4mh} \Big\} \end{aligned} \quad (28.7)$$

$$\begin{aligned} D_2m = & \frac{M(m)}{m\Delta} (1-K) \left\{ N(1+2mh+2mH) e^{mH-2mh} - N^2 e^{-mH-4mh} - \right. \\ & - KN \left[ 1 + 2mh(1-2mH) \right] e^{-mH-2mh} + KN^2(1+2mH) e^{mH-4mh} \Big\} \end{aligned} \quad (28.8)$$

$$\begin{aligned} A_3m^2 = & -\frac{M(m)}{m\Delta} (1-K)(1-N) \left\{ (1+mH) e^{mH} - K(1-mH) e^{-mH} - \right. \\ & - N \left[ 1 + 2m^2h^2 - 2mh - mH(1-2mh) \right] e^{-mH-2mh} + KN \left[ 1 - 2mh + \right. \\ & \left. + 2m^2h^2 + mH(1-2mh+4m^2h^2) \right] e^{mH-2mh} \Big\} \end{aligned} \quad (28.9)$$

$$\begin{aligned} B_3m = & -\frac{M(m)}{m\Delta} (1-K)(1-N) \left\{ e^{mH} - K(1-2mH) e^{-mH} + KN \left[ 1 - \right. \right. \\ & \left. \left. - 2mh(1+2mH) \right] e^{mH-2mh} - N(1-2mh-2mH) e^{-mH-2mh} \right\} \end{aligned} \quad (28.10)$$

$$C_3m^2 = 0$$

$$D_3m^2 = 0$$

where,

$$\left. \begin{aligned} M(m) &= -\frac{p_0 a}{m} J_1(ma) \\ K &= \frac{1-k}{1+k}, \quad k = \frac{E_2}{E_1} \\ N &= \frac{1-n}{1+n}, \quad n = \frac{E_3}{E_2} \\ \Delta &= -\left\{ e^{2mH} - 2K(1+2m^2H^2) + K^2 e^{-2mH} - 2N(1+2m^2h^2) e^{-2mh} + \right. \\ & + N^2 e^{-2mH-4mh} - \left[ K^2 N(1+4m^2H^2) + 4K^2 N(1+4m^2H^2) m^2 h^2 + \right. \\ & \left. + K^2 N + 8N(1-K^2) m^2 Hh + 4Nm^2 H^2 \right] e^{-2mh} + 2KN(1+2m^2h^2) \times \\ & \left. (e^{2mH} e^{-2mh} + e^{-2mH-2mh}) - 2KN^2(1+2m^2H^2) e^{-4mh} + K^2 N^2 e^{2mH-4mh} \right\}. \end{aligned} \right\} \quad (29)$$

Substituting these twelve constants from Eq. (26) and (28) into Eq. (21), desired expressions for stresses and displacements in any point in layered systems are obtained. Take  $\sigma_{zz}^1$  and  $u_z^1$  as an instance, they are written as follows,

$$\begin{aligned} \sigma_{zz}^1 = & - \int_0^\infty \frac{M(m) \cdot m}{\Delta} \cdot \left\{ e^{m(H-z)} (1+mH+mz) - K e^{-m(H+z)} [1-mH+ \right. \\ & + mz(1-2mH)] - N \cdot [(1+K^2)(1-mH) + 2(1+K^2)m^2h^2 - \\ & - 2(1-K^2)(1-mH)mh - 4K^2m^3Hh^2 + mz[K^2(1-2mH)(1+4m^2h^2 + \\ & + 2K^2mh + 1-2mH-2mh)]] e^{-m(H+2h+z)} + 2KN(1+2m^2h^2)(1+mH+ \\ & + mz) e^{m(H-2h-z)} - KN^2 e^{-m(H+4h+z)} [1-mH+mz(1-2mH)] + \\ & + K^2N^2 e^{m(H-4h-z)} (1+mH+mz) - K[1+mH-mz(1+2mh)] e^{m(H+z)} + \\ & + K^2(1-mH-mz) e^{-m(H-z)} - KN^2 [1+mH-mz(1+2mH)] e^{m(H-4h+z)} + \\ & + 2KN(1+2m^2h^2)(1-mH-mz) e^{-m(H+2h-z)} + N^2 e^{-m(H+4h-z)} (1-mH- \\ & - mz) + N[1-(1+K^2)(1+2m^2h^2+mH) - 2(1-K^2)(1+mH)mh - \\ & - 4m^3Hh^2K^2 + mz[K^2(1+2mH)(1+4m^2h^2) - 2K^2mh] + 1+2mH+ \\ & \left. + 2mh] e^{m(H-2h+z)} \right\} J_0(mr) dm \end{aligned} \quad (30)$$

$$\begin{aligned} u_z^1 = & - \frac{1.5}{E_1} \int_0^\infty \frac{M(m)}{m \cdot \Delta} \left\{ -(1+mH+mz) e^{m(H-z)} + K[1+mz(1-2mH) - \right. \\ & - mH] e^{-m(H+z)} + N e^{-m(H+2h+z)} [(1+K^2)(1+2m^2h^2-mH) - 2(1-K^2)(1- \\ & - mH)mh - 4K^2m^3Hh^2 + mz[(1-2mH)+K^2(1-2mH) - 2(1-K^2)mh + \\ & + 4K^2(1-2mH)m^2h^2]] - 2KN e^{m(H-2h-z)} (1+2m^2h^2)(1+mH+mz) + \\ & + KN^2 e^{-m(H+4h+z)} [1-mH+mz(1-2mH)] - K^2N^2 e^{-m(H-4h-z)} (1+mH+ \\ & + mz) - K e^{m(H+z)} [1+mH-mz(1+2mH)] + K^2 e^{-m(H-z)} (1-mH-mz) + \\ & + N e^{m(H-h+z)} [-(1+K^2)(1+2m^2h^2+mH) - 2(1-K^2)(1+mH)mh - \\ & - 4K^2m^3Hh^2 + mz[K^2(1+2mH)(1+4m^2h^2) + (1-K^2)2mh] + 1+2mH]] + \\ & + N^2 e^{-m(H+4h-z)} (1-mH-mz) + 2KN e^{-m(H+2h-z)} (1+2m^2h^2)(1-mH-mz) - \\ & \left. - KN^2 e^{m(H-4h+z)} [1+mH-mz(1+2mH)] \right\} m J_0(mr) dm. \end{aligned} \quad (31)$$

If  $E_2 = E_3$ , that is,  $N=0$  in Eq. (29), then expressions for the stress components  $\sigma_{zz}^1$  and displacement  $u_z^1$  shown in Eq. (30) and Eq. (31) are reduced to the expressions for two layered systems. They are

$$\sigma_{zz}^1 = \int_0^\infty \frac{mM(m)}{\Delta} \left\{ K^2 e^{m(z-h)} (1-mh-mz) + K e^{m(z+h)} [mz(1+2mh) - \right. \\ \left. - (1+mh)] - K e^{-m(z+h)} [mz(1-2mh) + (1-mh)] + \right. \\ \left. + e^{-m(z-h)} (1+mh+mz) \right\} J_0(mr) dm$$

$$u_z^1 = \frac{-1.5}{E_1} \int_0^\infty \frac{M(m)}{\Delta} \left\{ (1 + mh + mz) e^{m(h-z)} + K[-1 + mh - mz(1 - 2mh)] e^{-m(h+z)} + K[1 + mh - mz(1 + 2mh)] e^{m(h+z)} + K^2(mh + mz - 1) e^{m(z-h)} \right\} J_0(mr) dm \quad (32)$$

where,  $\Delta = e^{2mh} - 2K(1 + 2m^2h^2) + K^2e^{-mh}$

$$M(m) = -\frac{p_0 a}{m} J_1(ma).$$

Further, if we take  $E_2/E_1=1$ ,  $h=0$ , that is,  $K=0$ ,  $\Delta=1$ , we have the solutions for semi-infinite solid as follows,

$$\begin{aligned} \sigma_{zz}^1 &= -p_0 \int_0^\infty a J_1(ma) e^{-mz} (1 + mz) dm \\ &= -p_0 \left[ a \frac{\sqrt{a^2 + z^2} - z}{a\sqrt{a^2 + z^2}} + az \frac{2a\Gamma(3/2)}{\sqrt{\pi} (a^2 + z^2)^{3/2}} \right] \\ &= -p_0 \left[ 1 - \frac{z^3}{(a^2 + z^2)^{3/2}} \right]. \end{aligned}$$

This result coincides with Boussineq's solution of the problem. In the case of the displacement  $u_z$  (Eq. 31), letting  $K=0$ ,  $h=0$ ,  $r=0$ ,  $z=-h$ , then Eq. (31) is reduced to the expression of the displacement of the surface at its loading center. From Eq. (31) we have

$$\begin{aligned} u_z^1 &= \frac{1.5}{E} p_0 a \int_0^\infty \frac{1}{m} J_1(ma) dm \\ &= \frac{1.5}{E} p_0 a \end{aligned}$$

This result coincides with Boussinesq's solution of the semi-infinite solid problem.

#### 4. Stresses and displacements in three layered systems under tangential load on the surface

We consider the stress distribution in three layered systems under the action of a tangential load applied to the surface. If the tangential load is uniformly distributed over a circular area (Fig. 4), the boundary conditions on the surface become

$$\left. \begin{aligned} \sigma_{rz}(r, \theta, 0) &= -q(r) \cos \theta & r < a \\ \sigma_{\theta z}(r, \theta, 0) &= q(r) \sin \theta & r < a \\ \sigma_{rz}(r, \theta, 0) &= \sigma_{\theta z}(r, \theta) = 0 & r > a \\ \sigma_{zz}(r, \theta, 0) &= 0 & 0 \leq r \leq \infty \end{aligned} \right\} \quad (33)$$

Transformed tangential load  $q(r)$  is

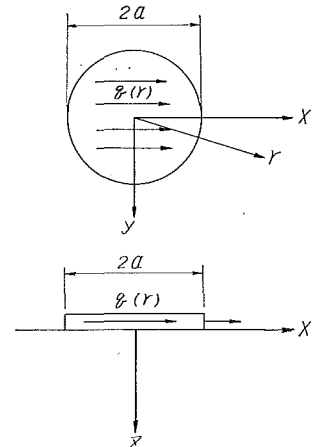


Fig. 4.

$$N(m) = \int_0^\infty r q(r) J_0(mr) dr$$

and in the case of  $q(r) = q_0 = \text{const.}$

$$\begin{aligned} N(m) &= q_0 \int_0^a r J_0(mr) dr \\ &= \frac{q_0 a}{m} J_1(ma). \end{aligned}$$

Putting  $n=1$  for the series expansion for the stresses and displacements, we can obtain the solutions for this problem.

Taking the coordinate system as in Fig. 3, the boundary conditions for this problem become as follows

$$\left. \begin{aligned} \text{for } z = -H: & \quad \sigma_{zz}^1 = 0 \\ & \quad \sigma_{rz}^1 = -q(r) \cos \theta \quad r < a \\ & \quad \sigma_{\theta z}^1 = q(r) \sin \theta \quad r < a \\ & \quad \sigma_{rz}^1 = \sigma_{\theta z}^1 = 0 \quad r > a \\ \text{for } z = 0: & \quad \sigma_{zz}^1 = \sigma_{zz}^2, \quad \sigma_{rz}^1 = \sigma_{rz}^2, \quad \sigma_{\theta z}^1 = \sigma_{\theta z}^2 \\ & \quad u_z^1 = u_z^2, \quad u_r^1 = u_r^2, \quad u_\theta^1 = u_\theta^2 \\ \text{for } z = h: & \quad \sigma_{zz}^2 = \sigma_{zz}^3, \quad \sigma_{rz}^2 = \sigma_{rz}^3, \quad \sigma_{\theta z}^2 = \sigma_{\theta z}^3 \\ & \quad u_z^2 = u_z^3, \quad u_r^2 = u_r^3, \quad u_\theta^2 = u_\theta^3. \end{aligned} \right\} \quad (34)$$

After solving these 15 simultaneous linear equations for  $\nu=0.5$ , we can obtain the following coefficients considering the semi-infinite solid of the third layer,

$$\begin{aligned} A_1 m^2 &= \frac{N(m)}{A \cdot m} \left\{ m H e^{\lambda_1} \left[ 2 K N (1 + 2 m^2 h^2) + e^{2 m h} + K^2 N^2 e^{-2 m h} \right] + \right. \\ & \quad + e^{\lambda_2} \left[ (1 - K^2) 2 N m^2 h^2 \right] - m H e^{\lambda_2} \left[ K e^{2 m h} + N (1 - 2 m h) + K N (1 + 2 m h) + \right. \\ & \quad \left. \left. + 4 m^2 h^2 \right) + K N^2 e^{-2 m h} \right] \left. \right\} \quad (35.1) \end{aligned}$$

$$\begin{aligned} B_1 m &= \frac{N(m)}{A \cdot m} \left\{ e^{\lambda_1} \left[ 2 K N (1 + 2 m^2 h^2) + e^{2 m h} + K^2 N^2 e^{-2 m h} \right] - e^{\lambda_2} \left[ K^2 N (1 - 2 m h) + \right. \right. \\ & \quad + 4 m^2 h^2) + K N^2 e^{-2 m h} + K e^{2 m h} - m H e^{\lambda_2} \left[ 2 K^2 N (1 + 4 m^2 h^2) + 2 K N^2 e^{-2 m h} + \right. \\ & \quad \left. \left. + 2 K e^{2 m h} + 2 N \right] \right\} \quad (35.2) \end{aligned}$$

$$\begin{aligned} C_1 m^2 &= \left\{ \frac{N(m)}{A \cdot m} \left\{ e^{\lambda_1} \left[ (1 - K^2) 2 N m^2 h^2 \right] + m H e^{\lambda_1} \left[ K^2 N (1 - 2 m h) + 4 m^2 h^2 \right) + \right. \right. \\ & \quad + K e^{2 m h} + K N^2 e^{-2 m h} + N (1 + 2 m h) \left. \right] - m H e^{\lambda_2} \left[ K^2 e^{2 m h} + K N + \right. \\ & \quad \left. \left. + N^2 e^{-2 m h} + K N (1 + 4 m^2 h^2) \right] \right\} \quad (35.3) \end{aligned}$$

$$D_1 m = \frac{N(m)}{A \cdot m} \left\{ e^{\lambda_1} \left[ N (1 - 2 m h) + K e^{2 m h} + K^2 N (1 + 2 m h + 4 m^2 h^2) \right] - \right.$$

$$-mHe^{\lambda_1} \left[ +2KN(1+4m^2h^2) + 2KN^2e^{-2mh} + 2Ke^{2mh} + 2N \right] - e^{\lambda_2} \left[ KN + K^2e^{2mh} + KN(1+4m^2h^2) + N^2e^{-2mh} \right] \} \quad (35. 4)$$

$$A_2m^2 = \frac{N(m)}{\Delta m} (1-K) \left\{ -e^{\lambda_1} \cdot 2KNm^2h^2 + mHe^{\lambda_1} \left[ KN(1-2mh+4m^2h^2 + e^{2mh}) + e^{\lambda_2} \cdot 2Nm^2h^2 - mHe^{\lambda_2} \left[ N(1-2mh) + Ke^{2mh} \right] \right] \right\} \quad (35. 5)$$

$$B_2m = \frac{N(m)}{\Delta \cdot m} (1-K) \left\{ e^{\lambda_1} \left[ e^{2mh} + KN(1+2mh) \right] - mHe^{\lambda_1} \cdot 4KNmh - e^{\lambda_2} \left[ Ke^{2mh} + N(1+2mh) \right] - mHe^{\lambda_2} (2Ke^{2mh} + 2N) \right\} \quad (35. 6)$$

$$C_2m^2 = \frac{N(m)}{\Delta \cdot m} (1-K) \left\{ e^{\lambda_1} \left[ 2Nm^2h^2 \right] + mHe^{\lambda_1} \left[ KN^2e^{-2mh} + N(1+2mh) \right] - e^{\lambda_2} \cdot 2KNm^2h^2 - mHe^{\lambda_2} \left[ KN(1+2mh+4m^2h^2) + N^2e^{-2mh} \right] \right\} \quad (35. 7)$$

$$D_2m = \frac{N(m)}{\Delta \cdot m} (1-K) \left\{ e^{\lambda_1} \left[ KN^2e^{-2mh} + N(1-2mh) \right] - e^{\lambda_2} mH(2KN^2e^{-2mh} + 2N) - e^{\lambda_2} \left[ N^2e^{-2mh} + KN(1-2mh) \right] + mHe^{\lambda_2} \cdot 4KNmh \right\} \quad (35. 8)$$

$$A_3m^2 = \frac{N(m)}{\Delta m} (1-K)(1-N) \left\{ -e^{\lambda_1} \cdot 2KNm^2h^2e^{-mh} + mHe^{\lambda_2} \cdot 2Nm^2h^2e^{-mh} + mHe^{\lambda_1} \left[ e^{mh} + KN(1-2mh+4m^2h^2) e^{-mh} \right] - mHe^{\lambda_2} \left[ Ke^{mh} + N(1-2mh) e^{-mh} \right] \right\} \quad (35. 9)$$

$$B_3m = \frac{N(m)}{\Delta \cdot m} (1-K)(1+N) \left\{ e^{\lambda_2} \left[ e^{mh} + KN(1+2mh) e^{-mh} \right] - mHe^{\lambda_1} \cdot 4KNmhe^{-mh} - e^{\lambda_2} \left[ Ke^{mh} + N(1+2mh) e^{-mh} \right] - mHe^{\lambda_2} \left[ 2(Ne^{-mh} + Ke^{mh}) \right] \right\} \quad (35. 10)$$

$$C_3m^2 = 0 \quad (35. 11)$$

$$D_3m = 0 \quad (35. 12)$$

$$E_1m = \frac{N(m)}{\delta \cdot m} (1 + KNe^{-2mh}) \quad (35. 13)$$

$$F_1m = \frac{N(m)}{\delta \cdot m} (K + Ne^{-2mh}) \quad (35. 14)$$

$$E_2m = \frac{N(m)}{\delta m} (1-K) \quad (35. 15)$$

$$F_2m = \frac{N(m)}{\delta \cdot m} (1-K) Ne^{-2mh} \quad (35. 16)$$

$$E_3 m = \frac{N(m)}{\delta m} (1-K)(1-N) \quad (35.17)$$

$$F_3 m = 0 \quad (35.18)$$

$$\left. \begin{aligned} \text{where, } N(m) &= \frac{q_0 a}{m} J_1(ma) \\ K &= \frac{1-k}{1+k}, \quad k = \frac{E_2}{E_1} \\ N &= \frac{1-n}{1+n}, \quad n = \frac{E_3}{E_2} \\ \lambda_1 &= mH + mh, \quad \lambda_2 = -mH - mh \\ \Delta &= - \left\{ e^{2mH} - 2K(1+2m^2H^2) + K^2e^{-2mH} - 2N(1+2m^2h^2)e^{-2mh} + N^2e^{-8m^2Hh} - \right. \\ &\quad - \left[ (1+4m^2H^2)K^2N + 4K^2N(1+4m^2H^2)m^2h^2 + K^2N + 8m^2Hh(1 - \right. \\ &\quad \left. - K^2)N + 4m^2H^2N \right] e^{-2mh} + 2KN(1+2m^2h^2)(e^{2m(H-h)} + e^{-2m(H+h)}) - \\ &\quad \left. - 2KN^2(1+2m^2H^2)e^{-4mh} + K^2N^2e^{2m(H-2h)} \right\} \\ \delta &= e^{mh}(1 + KNe^{-2mh}) - e^{-mh}(K + Ne^{-2mn}) \end{aligned} \right\} \quad (36)$$

Substituting Eq. (35) into Eq. (20), we obtain the solution for this problem. Take  $\sigma_{\theta z}^1$  and  $\sigma_{rz}^1$  as an instance, they are written as follows,

$$\left. \begin{aligned} \left. \begin{aligned} \sigma_{\theta z}^1 \\ \sigma_{rz}^1 \end{aligned} \right\} &= \frac{1}{2} \left\{ \int_0^\infty \frac{mN(m)}{\Delta} \cdot \left[ -e^{m(H-2h-z)}(1-mH-mz) \left[ 2KN(1+2m^2h^2 + e^{2mh} + \right. \right. \right. \\ &\quad \left. \left. + K_1^2N^2e^{-2mn} \right] + e^{-m(H+2h+z)} \left[ 2N(1-K^2)m^2h^2 + (1-mz) \left[ K^2N(1 - \right. \right. \right. \\ &\quad \left. \left. - 2mh + 4m^2h^2) + K_1^2N^2e^{-2mh} + Ke^{2mh} + N(1+2mh) \right] \right] - \\ &\quad - mHe^{-m(H+2h+z)} \left[ Ke^{2mh} + N(1-2mh)(+K^2N(1+2mh+4m^2h^2) + \right. \\ &\quad \left. + KN^2e^{-2mh} - (1-mz) \left[ 2K^2N(1+4m^2h^2) + 2KN^2e^{-2mh} + 2Ke^{2mh} + \right. \right. \\ &\quad \left. \left. + 2N \right] \right] + e^{m(H-2h+z)} \left[ 2N(1-K^2)m^2h^2 + (1+mz) \left[ N(1-2mh) + Ke^{2mh} + \right. \right. \\ &\quad \left. \left. + K^2N(1+2mh+4m^2h^2) + KN^2e^{-2mh} \right] \right] + mHe^{m(H-2h+z)} \left[ K^2N(1 - \right. \\ &\quad \left. - 2mh + 4m^2h^2) + Ke^{2mh} + KN^2e^{-2mh} + N(1+2mh) - (1+mz) \times \right. \\ &\quad \left. \times \left[ 2K^2N(1+4m^2h^2) + 2KN^2e^{-2mh} + 2Ke^{2mh} + 2N \right] \right] - e^{-m(H+2h-z)}(1 + \\ &\quad \left. + mH + mz) \left[ K^2e^{2mh} + N^2e^{-2mh} + 2KN(1+2m^2h^2) \right] \right] \left[ J_2(mr) \pm \right. \\ &\quad \left. J_0(mr) \right] dm + \int_0^\infty \frac{mN(m)}{\delta} \left[ e^{-mz} + KNe^{-2hm-mz} - Ke^{mz} - Ne^{-2mh+mz} \right] \times \\ &\quad \left. \left[ J_2(mr) \mp J_0(mr) \right] dm \right\} \begin{matrix} \sin \theta \\ \cos \theta \end{matrix} \end{aligned} \right\} \quad (37)$$

Putting  $N=0$ , the results are reduced to the solutions of the two layered system. They are

$$\left. \begin{aligned} \sigma_{\theta z}^1 \\ \sigma_{rz}^1 \end{aligned} \right\} = \frac{1}{2} \left\{ - \int_0^\infty \frac{mN(m)}{A} \left[ e^{-m(z-h)} (mh-1+mh) + Ke^{-m(z+h)} [1+mh - \right. \right. \\ \left. \left. - mz(1+2mh)] + Ke^{m(z+h)} [1-mh+mz(1-2mh)] - K^2 e^{m(z-h)} (mh + \right. \\ \left. + 1+mz) \right] [J_2(mr) \pm J_0(mr)] dm + \int_0^\infty \frac{mN(m)}{\delta} (e^{-mz} + Ke^{mz}) \times \\ \left. \times [J_2(mr) \mp J_0(mr)] dm \right\} \begin{matrix} \sin \theta \\ \cos \theta \end{matrix} \quad (38)$$

Further, if we put  $E_1/E_2=1$ , ie,  $K=0$ , these expressions coincide with the solutions for a semi-infinite solid with a tangential surface load obtained by Muki.

### 5. Numerical Examples

Numerical calculations were carried out for various cases by a electronic computer. A calculation of a definite integration was done by the help of Simpson's formula. Many interesting results and important characteristics of the multi-layered systems were obtained. Here, only two examples of them are shown in Fig. 5 and Fig. 6. Fig. 5 shows the pressure bulbs and Fig. 6 shows the principal stresses in the two layered system subjected to a normal load and a tangential load simultaneously on its surface.

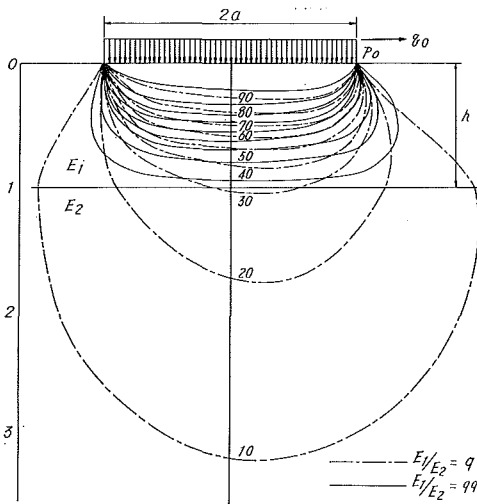


Fig. 5. (a)

Pressure bulb of  $\sigma_{zz}$ , (in the case of  $a/h=1.0$ )  
(Numerical values on each curve show the percentage to  $(p_0+q_0)$  ( $q_0 = \frac{p_0}{2}$ ))

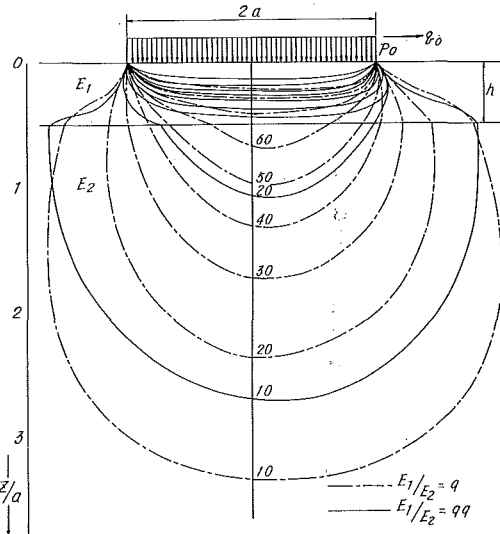


Fig. 5. (b)

Pressure bulb of  $\sigma_{zz}$  (in the case of  $a/h=1.5$ )

$$(q_0 = \frac{p_0}{2})$$

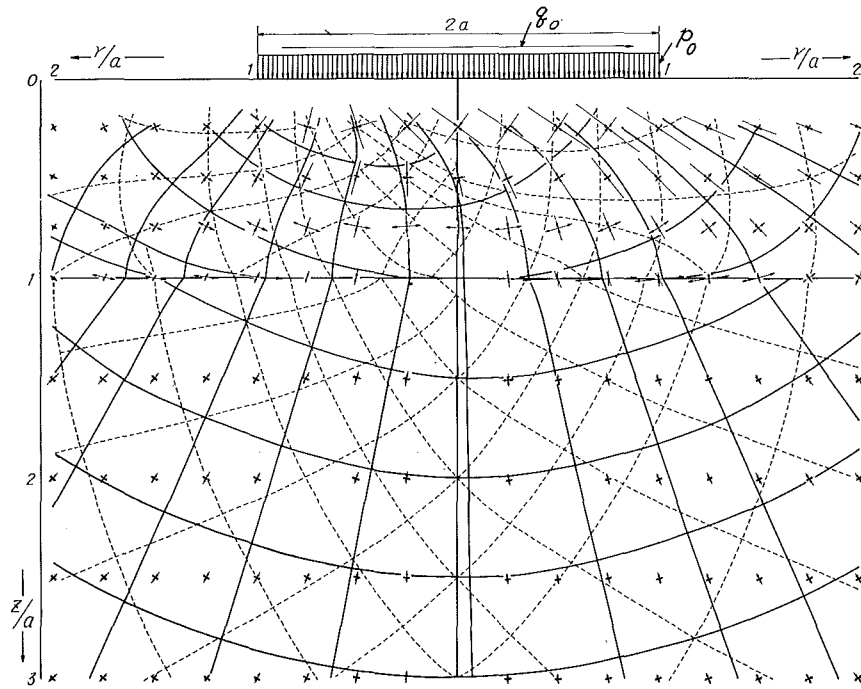


Fig. 6. (a) Principal stress line (solid curve) and Principal shearing stress line (dotted line). ( $E_1/E_2=9$ ) ( $q_0 = \frac{p_0}{2}$ )

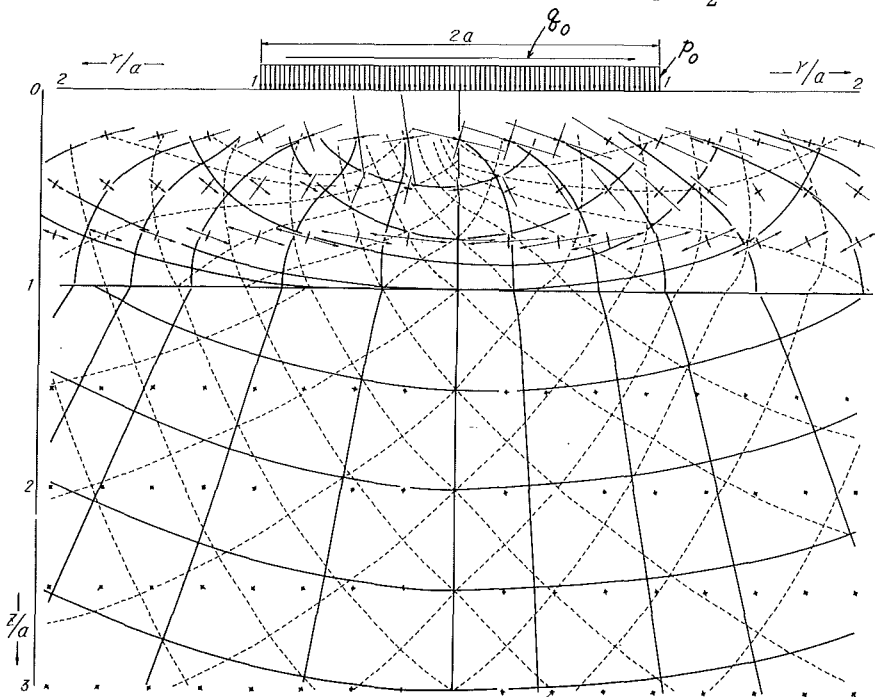


Fig. 6. (b) Principal stress line (solid curve) and Principal shearing stress line (dotted curve). ( $E_1/E_2=99$ ) ( $q_0 = \frac{p_0}{2}$ )

### References

- 1) Burmister, D. M.: "The theory of stresses and displacements in layered system and applications to the design of airport runways", Proc., 23rd-Annual Meeting of H.R.B., Vol. 23 (1943).  
"The general theory of stresses and displacements in layered systems", J. App. phys. Vol. 16 (1945).
- 2) Fox, L.: "Computation of traffic stresses in a simple road structure", Road Research Tech. Paper No. 9 (1948).
- 3) Jelinek R., and Ranke, A.: "Berechnung der Spannungs verteilung in einem Zweischichten system", Bautech. Heft. 2 (1970).
- 4) Acum, W. E. and Fox, L.: "Computation of Load Stresses in a Three-Layer Elastic System," Geotechnique (1951), No. 4, pp. 293-300.
- 5) Sneddon, I. N.: Fourier Transforms (1951). McGraw-Hill.
- 6) Muki, R.: "Three dimensional Problem of elasticity theory for a semi-infinite solid and a thick plate", Progress in Solid Mechanics, pp. 400-439 (1956), North-Holl and Pub. Co.
- 7) Schiffmann, R. L.: "General analysis of stresses and displacements in layered systems", Int. Nat. Conf. on the structural design of Asphalt Pavements Proc. (1962).