



HOKKAIDO UNIVERSITY

Title	Polythermal modelling of steady states of the Antarctic ice sheet in comparison with the real world
Author(s)	Hansen, I. ; Greve, Ralf
Citation	Annals of Glaciology, 23, 382-387
Issue Date	1996
Doc URL	https://hdl.handle.net/2115/47917
Rights	© 1996 International Glaciological Society
Type	journal article
File Information	Hansen_Greve_1996_AnnGlac.pdf



Polythermal modelling of steady states of the Antarctic ice sheet in comparison with the real world

I. HANSEN AND R. GREVE

Department of Mechanics, Technische Hochschule Darmstadt, D-64289 Darmstadt, Germany

ABSTRACT An approach to simulate the present Antarctic ice sheet with respect to its thermomechanical behaviour and the resulting features is made with the three-dimensional polythermal ice-sheet model designed by Greve and Hutter. It treats zones of cold and temperate ice as different materials with their own properties and dynamics. This is important because an underlying layer of temperate ice can influence the ice sheet as a whole, e.g. the cold ice may slide upon the less viscous binary ice–water mixture.

Measurements indicate that the geothermal heat flux below the Antarctic ice sheet appears to be remarkably higher than the standard value of 42 mW m^{-2} that is usually applied for Precambrian shields in ice-sheet modelling. Since the extent of temperate ice at the base is highly dependent on this heat input from the lithosphere, an adequate choice is crucial for realistic simulations. We shall present a series of steady-state results with varied geothermal heat flux and demonstrate that the real ice-sheet topography can be reproduced fairly well with a value in the range $50\text{--}60 \text{ mW m}^{-2}$. Thus, the physical parameters of ice (especially the enhancement factor in Glen's flow law) as used by Greve (1995) for polythermal Greenland ice-sheet simulations can be adopted without any change. The remaining disagreements may be explained by the neglected influence of the ice shelves, the rather coarse horizontal resolution (100 km), the steady-state assumption and possible shortcomings in the parameterization of the surface mass balance.

1. INTRODUCTION

This paper presents studies of the influence of varied geothermal heat flux beneath Antarctica on the overlying ice sheet. The work is based on experiments that have been performed with Greve's (1995) polythermal ice-sheet model which ran successful simulations for the Greenland ice sheet; its numerical code SICOPOLIS has now been adopted for the southern polar continent.

A particular property of this model is the different treatment of cold and temperate zones in the ice sheet; most of the ice volume may consist of the first type of ice which is regarded as an incompressible single-component material, while the second can be found in bottom regions as a binary mixture of ice at its local pressure-melting point and water, e.g. when the pressure is high enough to melt the ice. The energetic behaviour of cold ice is determined by its temperature field; since the temperature in the temperate zones is locally constant, here the production and advection of water content take over this role. A non-material surface called CTS (cold-temperate transition surface) separates both regions from each other; it migrates depending on the conditions supported by the ice on both sides. More detailed information about this

topic and the theory of polythermal ice sheets can be read in the papers by Hutter (1982, 1983, 1993) and Greve (1995) and Greve and Hutter (1995). The numerics have been developed by Greve (1995) and a short description is given in section 3.

Interactions with the atmosphere and the lithosphere are stated in the following form: the surface temperature is parameterized as a function of geographical latitude and height; the accumulation function is represented by a temporally constant snowfield which was supplied from precipitation model output of the ECHAM3 T42-GCM belonging to the Deutsches Klimarechenzentrum Hamburg. Melting at the ice surface is not taken into account, because temperatures are so low that this phenomenon virtually does not occur. The lithosphere adjusts to the ice load following a simple model of vertical moveable rock columns sinking in the viscous asthenosphere, and the primary topography has been calculated from the present-day rock-bottom topography and ice thickness after Drewry (1983). The geothermal heat flux is kept constant in space and time; it has been varied between 42 and 105 mW m^{-2} in the experiments described below. As we are only interested in steady states, thermal inertia of the lithosphere is not taken into account.

Our results demonstrate a strong dependence of the characteristic ice-sheet properties on the basal thermal regime which in turn seems to be very sensitive to variations in the geothermal heat flux, as has already been demonstrated for the Greenland ice sheet by Greve and Hutter (1995).

2. THEORY AND NUMERICS

The theoretical background of the polythermal ice model used in our study can be found in Greve (1995); we will not write down here the entire set of equations, which build the physical structure of the problem, for reasons of brevity. Briefly, it consists of balance equations for mass, momentum and energy for the region of cold ice, combined with constitutive assumptions for example the material law for viscous fluids containing Glen's flow law and a rate factor depending on the homologous temperature. The energy balance can be evolved in an equation for the temperature field

$$\frac{\partial T}{\partial t} = -v_x \frac{\partial T}{\partial x} - v_y \frac{\partial T}{\partial y} - v_z \frac{\partial T}{\partial z} + \frac{1}{\rho c} \frac{\partial}{\partial z} \left(\kappa \frac{\partial T}{\partial z} \right) + \frac{2}{\rho c} EA(T') f(\sigma) \sigma^2 \quad (1)$$

(T temperature, T' homologous temperature, $v_{x,y,z}$ velocities in the x, y and z directions, ρ density of ice, c specific heat of ice, κ heat conductivity of ice, E enhancement factor, $A(T')$ rate factor for cold ice, $f(\sigma)$ creep function using Glen's flow law with $n=3$ and σ shear stress). Ice-temperature changes by horizontal and vertical advection, by vertical heat conduction and by heat production based on internal friction. The shallow-ice approximation, which assumes typical height scales to be very much smaller than typical length scales, eliminates lateral heat conduction.

Temperate ice is described by similar equations to those for cold ice, yet valid for the mixture of ice and water. A balance equation for the water content ω is added. As temperature equals pressure melting

$$T = T_m = T_0 - \beta(h - z) \quad (2)$$

(T_m pressure-melting point, T_0 melting point at zero pressure, β Clausius–Clapeyron gradient and h z coordinate of the free surface), the water content takes over the role of the energetic variable determining the material behaviour. Its temporal evolution is given by

$$\frac{\partial \omega}{\partial t} = -v_x \frac{\partial \omega}{\partial x} - v_y \frac{\partial \omega}{\partial y} - v_z \frac{\partial \omega}{\partial z} + \frac{2}{\rho L} EA_t(\omega) f_t(\sigma) \sigma^2 + \frac{\beta^2}{\rho L} \frac{\partial \kappa}{\partial T} + \frac{c\beta}{L} \left(\frac{\partial h}{\partial t} + v_x \frac{\partial h}{\partial x} + v_y \frac{\partial h}{\partial y} - v_z \right) - \frac{1}{\rho} D(\omega) \quad (3)$$

(L latent heat of ice, $A_t(\omega)$ rate factor for temperate ice, $f_t(\sigma) = f(\sigma)$ creep function for temperate ice and $D(\omega)$ water-drainage function). As in Equation(1), water content varies as a result of horizontal and vertical advection and heat production due to internal friction; furthermore, there is a small Clausius–Clapeyron correction (first two terms in the second line) and the

contribution of water drainage. Note that for temperate ice the rate factor in the flow law strongly depends on the water content.

The interface separating the two ice regions (CTS) shows no jump in temperature, i.e. the temperature on both sides must be at the melting point. In the case of melting conditions, there is a volume flux of ice directed from the cold region into the temperate region, leading to a continuous water content and temperature gradient; in the case of freezing conditions (opposite ice-flow direction), however, these two quantities can be discontinuous.

The most obvious quantity representing the dynamic behaviour of the ice sheet is the ice thickness H which is simply the difference between the z -coordinates of ice surface h and ice base b ; its temporal evolution is given by

$$\frac{\partial H}{\partial t} = \frac{\partial(h - b)}{\partial t} = -\frac{\partial q_x}{\partial x} - \frac{\partial q_y}{\partial y} + a_s^\perp - \frac{\mathcal{P}_b^w}{\rho}, \quad (4)$$

with the mass flux \mathbf{q} defined as

$$(q_x, q_y) := \int_b^h (v_x, v_y) dz' \quad (5)$$

(a_s^\perp accumulation–ablation function for the ice surface and \mathcal{P}_b^w basal melting rate derived from the mass jump condition for water w), integrated from the ice base b to the ice surface h . The ice thickness grows or shrinks depending on the divergence of the mass flux, on snowfall and on basal melting, which in turn is a function of the heat-conduction gradient at the ice–lithosphere interface and of basal friction.

As for the numerics, the three-dimensional model is integrated with finite differences. The horizontal grid-point distance is 100 km, while in the vertical σ coordinates for cold ice (51 points with densification towards the bottom), temperate ice (11 equidistant points) and lithosphere (11 equidistant points) are used. The time step is 10 a for the calculation of the velocities and the topography, and 100 a for integration of temperature and water content. The latter equations are discretized implicitly for the z derivatives and explicitly (upwind scheme) for the x and y derivatives, i.e. the horizontal advection terms. For the ice-thickness-evolution equation, an ADI scheme (alternating implicit and explicit discretization in the horizontal directions) is applied. The external forcing has already been described in the introduction. At the ice base, the sliding law is of Weertman-type (Calov, 1994), if the base is temperate and no-sliding conditions are assumed in the case of a cold base. The associated discontinuity that appears at the transition between sliding and adhesion does not cause any problems in the numerical solution, because it is smeared out by the finite grid resolution*. The most important physical quantities are listed in Table 1.

* A mathematically and physically correct sliding law could be worked out with a temporally or spatially smoothed transition between sliding and adhesion.

Table 1. Values for physical quantities used in the model calculations

Quantity	Value
Ice density, ρ	910 kg m^{-3}
Heat conductivity of ice, κ	$9.828 e^{-0.0057T[\text{K}]} \text{ W m}^{-1} \text{ K}^{-1}$
Specific heat of ice, c	$(146.3 + 7.253T[\text{K}]) \text{ J kg}^{-1} \text{ K}^{-1}$
Latent heat of ice, L	335 kJ kg^{-1}
Clausius–Clapeyron gradient, β	$8.7 \times 10^{-4} \text{ Km}^{-1}$
Gravity acceleration, g	9.832 m s^{-2}

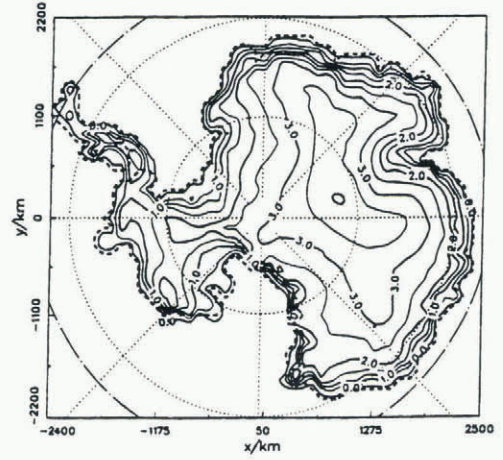


Fig. 1. Observed free-surface topography after Drewry (1983). Equidistance of the contours is 500 m.

3. ANALYSIS OF HEAT-FLUX DATA

The “new global heat-flow compilation” derived from on-line computer devices, a description of which has been given by Pollack and others (1993), contains some heat-flux data gained by different research workers. The positions of these measurements lie quite close together near Ross Island. The data vary over a wide range ($Q_{\text{geoth}} = 63 \dots 164 \text{ mW m}^{-2}$); an explanation may be the rough topography of this region, which extends from the Ross Sea floor to the Transantarctic Mountains. With respect to our model grid, the maximum distances between the measurements are about 150 km in x and 300 km in y directions, which gives us almost single-point information. We decided to ignore the two peak values of 164 and 142 mW m^{-2} and obtain an average from the remaining seven values of $Q_{\text{geoth}} = 70.2 \text{ mW m}^{-2}$ with a standard deviation of 6.4 mW m^{-2} , which is obviously much higher than the value $Q_{\text{geoth}} = 42 \text{ mW m}^{-2}$ commonly used in ice-sheet modelling, e.g. for Greenland. As we have no more detailed information about the thermal conditions at the ice–lithosphere interface, we assume the heat flux is spatially constant beneath the Antarctic continent and take our average of 70 mW m^{-2} as standard. Therefore, experiments have been performed with geothermal heat fluxes of 42 (Greenland), 50, 60, 70 (standard), 80, 90 and 105 mW m^{-2} (standard + 50%).

4. MODEL RUNS WITH VARIOUS GEOTHERMAL HEAT FLUXES

Because of the above-mentioned hint that heat flux beneath Antarctica may be higher than the commonly assumed $Q_{\text{geoth}} = 42 \text{ mW m}^{-2}$, we carried out a series of experiments, starting with an initial ice-free rock topography over 10^5 years, until a steady state is approximately reached. The atmospheric forcing fields remain unchanged; only variations in geothermal heat flux will be considered.

Figure 1 shows the free ice-surface topography based on measurements, taken from Drewry (1983); the topographies resulting from the model runs are depicted in Figure 2. The associated homologous temperature at the ice base and the distribution of temperate ice above

the base can be seen in Figure 3. Other characteristic quantities such as total ice volume V_{tot} , maximum height of the free surface h_{max} , maximum ice thickness H_{max} and maximum thickness of the temperate-ice layer $H_{\text{t,max}}$ are given in Figure 4a–c, supplemented with observed data where possible.

As expected, the free-surface topography is modified significantly by the geothermal heat flux. The local height shrinks with intensified heating from below and simultaneously the total ice volume decreases by about 11.5%, but the available rock-bottom area remains ice-covered. Also, smaller features are concerned, e.g. the central Argus Dome flattens and the domes in West Antarctica also seem to vanish. The maximum ice thickness H_{max} is reduced by more than 600 m over the range of the varied geothermal heat fluxes; in the most probable range 42–70 mW m^{-2} for Q_{geoth} , H_{max} also reacts very sensitively. Since effects of atmospheric forcing can be excluded in this case, the geothermal heat flux must induce the mechanics to build up ice sheets with different volumes and slightly varying structures. The stronger the lithosphere heats the ice, the weaker the lower ice layers become; these are responsible for greater horizontal velocities which then result in a smaller ice sheet.

The amount of ice which is directly being influenced by the geothermal heat flux, namely the volume of temperate ice V_{temp} , astonishingly decreases by more than 40%; at first sight, this seems to be a contradiction as the area covered with temperate ice grows. Yet, a closer look reveals that areas with an overlying temperate-ice layer do not expand that much; they only change their site and the maximum thickness $H_{\text{t,max}}$ (Fig. 4c) of the temperate-ice layer (this maximum is located in the widest area in Wilkes Land) shrinks for the same reasons as the whole ice mass does. Generally, zones with a temperate-ice base can be found all along the coastline. For small values of the geothermal heat flux, most of these points possess an overlying temperate-ice layer with melting conditions at the CTS, while central Antarctica shows a cold-ice base. As heating from the lithosphere increases in strength, the ring of temperate ice becomes more uniform around the continent and the inner land also acquires a temperate base. For 105 mW m^{-2} , almost the entire Antarctic ice base is at the pressure-melting point.

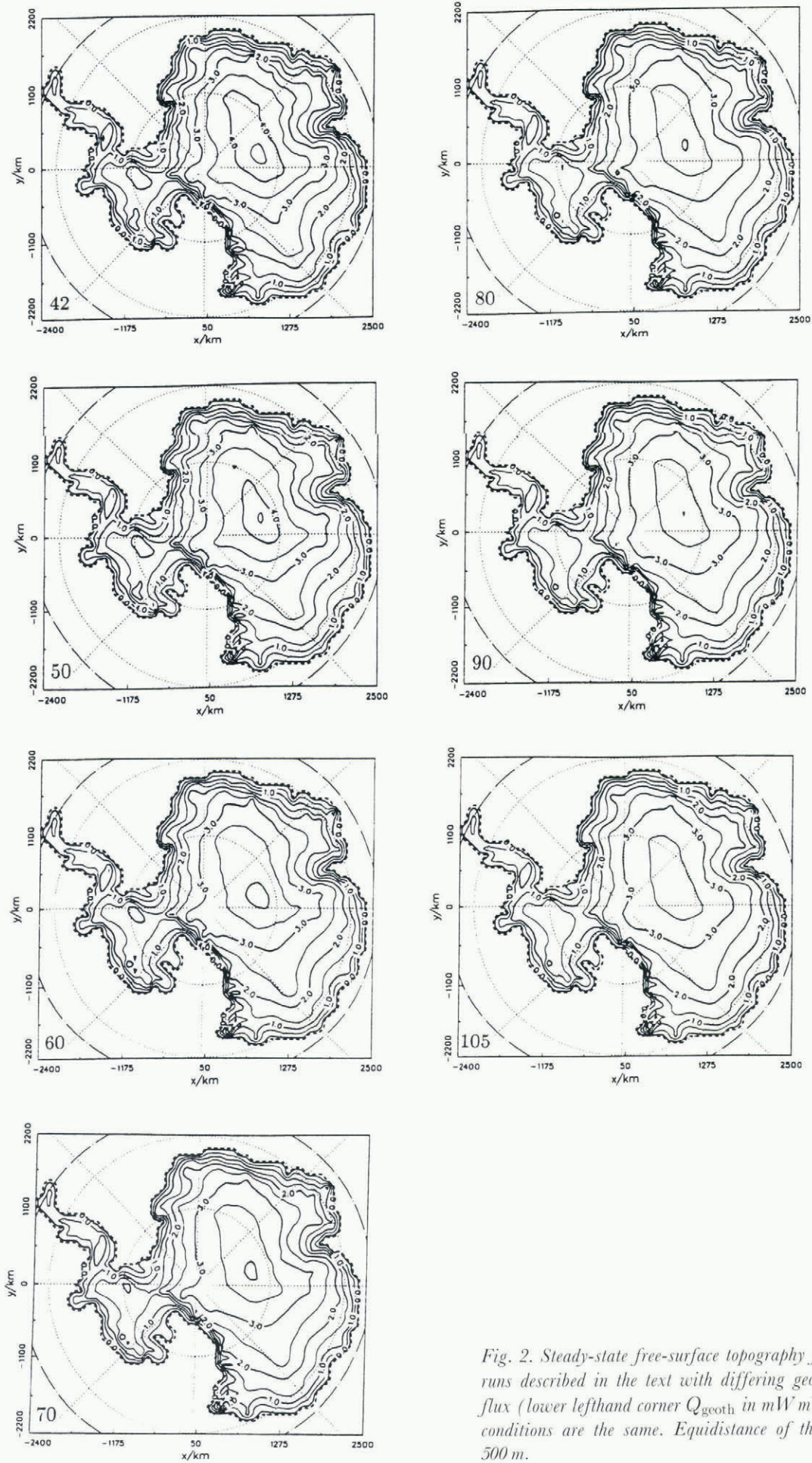


Fig. 2. Steady-state free-surface topography for the model runs described in the text with differing geothermal heat flux (lower lefthand corner Q_{geoth} in mW m^{-2}); all other conditions are the same. Equidistance of the contours is 500 m.

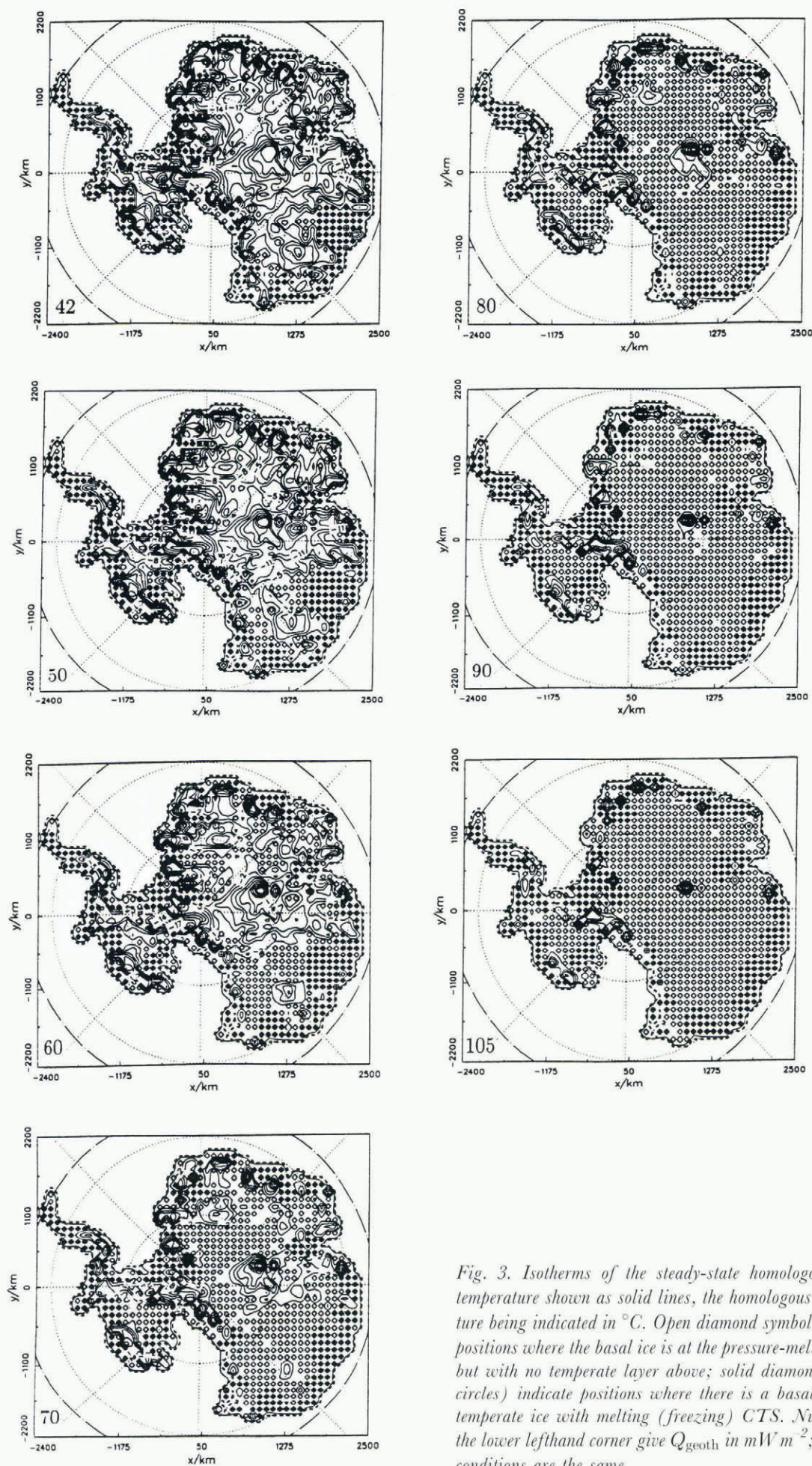


Fig. 3. Isotherms of the steady-state homologous basal temperature shown as solid lines, the homologous temperature being indicated in $^{\circ}\text{C}$. Open diamond symbols indicate positions where the basal ice is at the pressure-melting point but with no temperate layer above; solid diamonds (solid circles) indicate positions where there is a basal layer of temperate ice with melting (freezing) CTS. Numbers in the lower lefthand corner give Q_{geoth} in mW m^{-2} ; all other conditions are the same.

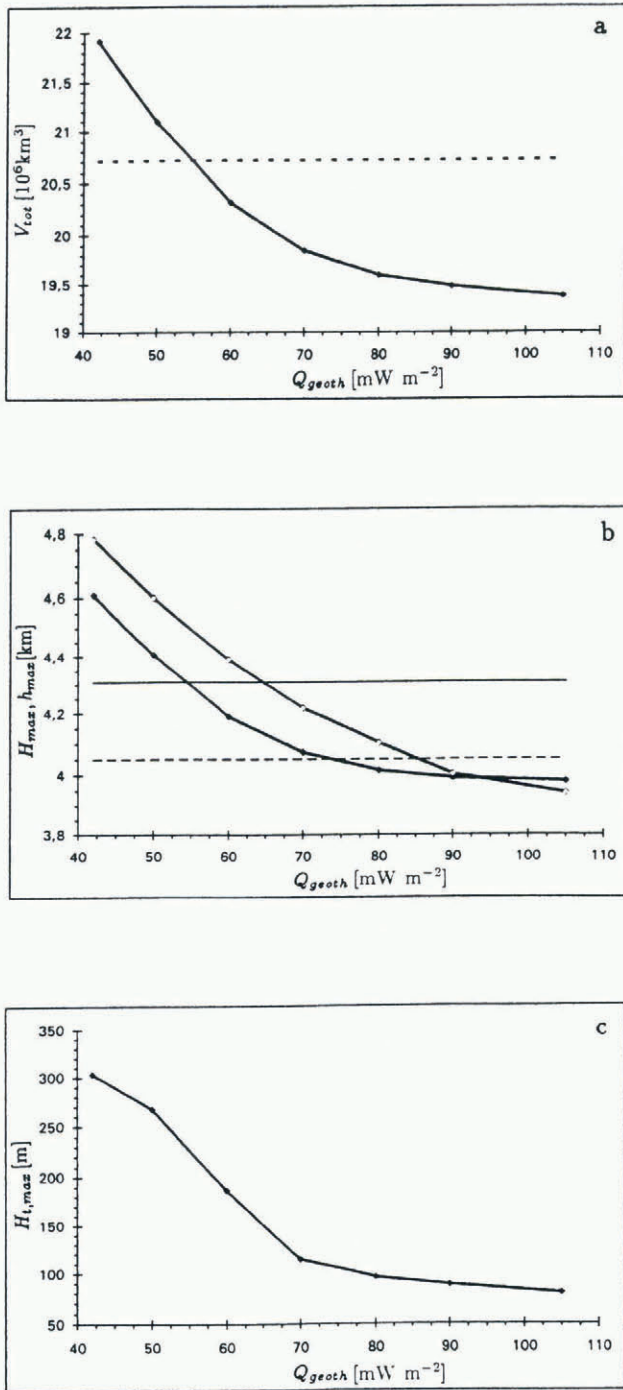


Fig. 4. Model output for (a) total ice volume V_{tot} , the dashed line indicating the observed value; (b) maximum ice thickness H_{max} (solid diamonds) and maximum height of the ice sheet h_{max} (open diamonds) with the corresponding observed values indicated by a thin solid line for H_{max} and a thin dashed line for h_{max} ; (c) maximum thickness of the temperate-ice layer $H_{t,max}$; all are displayed as a function of the geothermal heat flux Q_{geoth} .

In comparison with reality, which is documented in Figure 1 and as single values in Figure 4a and c, the model reproduces the major features and structures of the ice-sheet topography quite well. Argus Dome and the West Antarctic maxima are located at the righthand site; however, the Antarctic Plateau becomes too steep in the middle and too flat towards the coast; West Antarctica, on the other hand, is simulated very close to reality. The best coincidence of model results and measurements with regard to properties such as total ice volume and maximum ice thickness is achieved for a geothermal heat flux of about $50\text{--}60 \text{ mW m}^{-2}$. Therefore, 42 mW m^{-2} seems to be too low but 70 mW m^{-2} is exaggerated as a spatially constant geothermal heat flux for the entire south polar continent. Still, the maximum height of the ice sheet obtained is too high; this might be an effect of the incorrect shape, which in turn can be a consequence of the rather low resolving grid and insufficient precision of atmospheric forcing fields; such problems will be removed in the future. Another idea is to improve the lithospheric behaviour by implementing a more elaborate model, because the position of the simulated height maximum need not be the same as the actual peak.

A final encouraging remark is that most of the observed ice lakes cited by Herterich (1990) from Oswald and Robin (1973), are located in regions where our model predicts the ice temperature is at least at the melting point.

REFERENCES

- Calov, R. 1994. Das thermomechanische Verhalten des grönländischen Eisschildes unter der Wirkung verschiedener Klimaszenarien — Antworten eines theoretisch-numerischen Modells. (Ph.D. thesis, Technische Hochschule, Darmstadt.)
- Drewry, D.J., ed. 1983. *Antarctica: glaciological and geophysical folio*. Cambridge, Scott Polar Research Institute.
- Greve, R. 1995. Thermomechanische Verhalten polythermer Eisschilder — Theorie, Analytik, Numerik. (Ph.D. thesis, Technische Hochschule, Darmstadt.)
- Greve, R. and K. Hutter. 1995. Polythermal three-dimensional modelling of the Greenland ice sheet with varied geothermal heat flux. *Ann. Glaciol.*, **21**, 8–12.
- Herterich, K. 1990. *Modellierung eiszeitlicher Klimaschwankungen*. Hamburg, Universität Hamburg, Fachbereichs Geowissenschaften. (Habilitationsschrift im Fachgebiet Meteorologie.)
- Hutter, K. 1982. A mathematical model of polythermal glaciers and ice sheets. *Geophys. Astrophys. Fluid Dyn.*, **21**(3–4), 201–224.
- Hutter, K. 1983. *Theoretical glaciology; material science of ice and the mechanics of glaciers and ice sheets*. Dordrecht, etc., D. Reidel Publishing Co./Tokyo, Terra Publishing Co.
- Hutter, K. 1993. Thermo-mechanically coupled ice-sheet response — cold, polythermal, temperate. *J. Glaciol.*, **39**(131), 65–86.
- Oswald, G.K.A. and G.deQ. Robin. 1973. Lakes beneath the Antarctic ice sheet. *Nature*, **245**(5423), 251–254.
- Pollack, H.N., S.J. Hurter and J.R. Johnson. 1993. Heat flow from the Earth's interior: analysis of the global data set. *Rev. Geophys.*, **31**(3), 267–280.