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A large effective area multi-core fiber with an optimized cladding thickness

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Abstract: The cladding thickness of trench-assisted multi-core fibers was theoretically and experimentally investigated in terms of excess losses of outer cores. No significant micro-bending loss increase was observed on multi-core fibers with the cladding thickness of about 30 μm . The tolerance for the micro-bending loss of a multi-core fiber is larger than that of the single core fiber. However, the cladding thickness will be limited by the occurrence of the excess loss on outer cores. The reduction of cladding thickness is probably limited around 40 μm in terms of the excess loss. The multi-core fiber with an effective area of 110 μm^2 at 1.55 μm and 181- μm cladding diameter was realized without any excess loss.

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OCIS codes: (060.2270) Fiber characterization; (060.2280) Fiber design and fabrication.

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1. Introduction

A multi-core fiber (MCF) is expected to be a next generation transmission fiber that overcomes the capacity limit by space-division multiplexing technique. Many types of MCFs

have been proposed [1–5]. Crosstalk between cores is a critical issue for MCF. Additionally, low attenuation and large effective area (A_{eff}) characteristics are also important for a transmission fiber to improve OSNR. A MCF with A_{eff} of about $110 \mu\text{m}^2$ at $1.55 \mu\text{m}$ has been reported [3]. However, the cladding diameter of the MCF was about $220 \mu\text{m}$ for suppressing a micro-bending loss. The large cladding diameter is undesirable in terms of a reliability issue and a high density core arrangement.

In this paper, we investigate cladding thickness effect on a micro-bending loss and an excess loss of outer cores to realize a large A_{eff} and small-cladding MCF. The cladding thickness is determined in consideration of the micro-bending loss and the excess loss of outer cores. The micro-bending characteristic of MCFs is compared to that of single-core fibers (SCFs) for various cladding thicknesses. It is confirmed that the tolerance for the micro-bending loss of a multi-core fiber is larger than that of the single core fiber. The excess loss is estimated by the confinement loss of cores and experimentally confirmed. We clarify that the limit of the cladding thickness in the case of the large A_{eff} MCF is about $40 \mu\text{m}$. Our fabricated MCF with a trench index profile realizes A_{eff} of more than $110 \mu\text{m}^2$, cladding diameter of $181\text{-}\mu\text{m}$ and crosstalk of lower than -30 dB at 100 km , simultaneously.

2. Fiber design

We employed a trench-assisted MCF (TA-MCF) design to realize a low crosstalk and dense core arrangement simultaneously. The trench-assisted fiber (TAF) can reduce not only a macro-bending loss [6] but also a micro-bending loss [7]. Figure 1 shows a cross section of a seven-core TA-MCF and an index profile of a core element. The TA-MCFs with A_{eff} of $80 \mu\text{m}^2$ have been reported [4]. We targeted the TA-MCF with A_{eff} of about $110 \mu\text{m}^2$ for long transmission lines. The fiber parameters were determined to achieve A_{eff} of $110 \mu\text{m}^2$ and crosstalk of lower than -30 dB at 100 km . An outer cladding thickness (*OCT*) affects micro-bending loss characteristics and excess loss of outer cores. We fabricated MCFs with *OCT*s of about $30 \mu\text{m}$ and $50 \mu\text{m}$ based on the following consideration on micro-bending loss and excess loss.

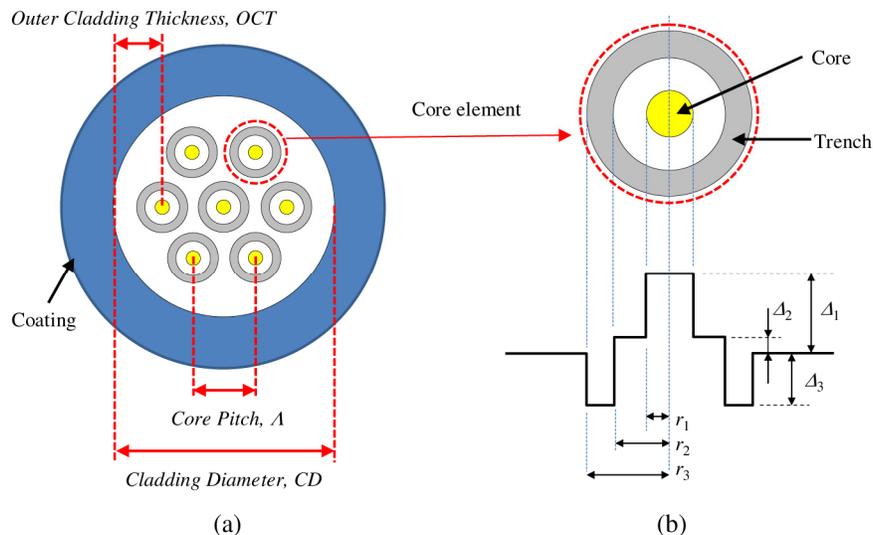


Fig. 1. (a) Cross section of a seven-core trench-assisted multi-core fiber. (b) Trench index profile.

2.1 Micro-bending loss

Figure 2 shows the measurement results of micro-bending loss of SCFs. Three types of fibers were prepared for the measurement. The coating thicknesses of the fibers were set to be same

as the standard single-mode fiber. A Step80 is a conventional single-mode fiber with a step index profile and A_{eff} at 1.55 μm of 80 μm^2 . A Step110 and a TAF110 realize A_{eff} at 1.55 μm of 110 μm^2 with a step profile and a trench-assisted profile, respectively. The step110 is a conventional large A_{eff} fiber. We fabricated the TAF110 to verify the micro-bending reduction due to a trench. The OCT of a SCF corresponds to half of a cladding diameter. The micro-bending loss is a loss increase at 1.625 μm when the fiber was wound on a bobbin whose surface is covered with a sand paper (grade 40 μm) based on the IEC standard [8]. The tension on the fiber during winding was 100 gf. The length of the fiber was 400 m.

The micro-bending loss of Step80 was about 0.1dB/km. The micro-bending loss reduction thanks to a trench was clearly observed from the measurement data of Step110 and TAF110. The micro-bending loss of TAF110 with 50- μm OCT is the similar level with that of Step110 with 62.5- μm OCT .

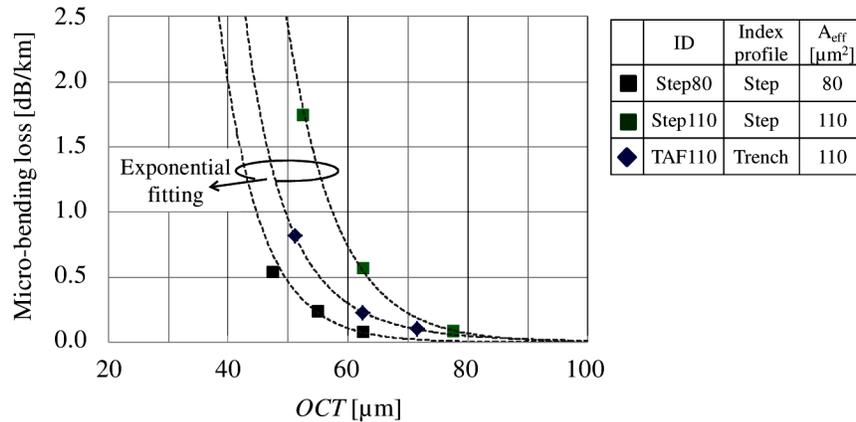


Fig. 2. Micro-bending loss of different kinds of single-core fibers as a function of cladding thickness: Symbols are measurement results. Dashed lines are exponential fitting lines on the measurement results.

2.2 Excess loss in outer cores

In the case of transmission fibers, the refractive index of the coating n_{co} is larger than that of glass region of a fiber. The high index coating causes the excess loss in outer cores for small OCT [5]. To estimate the excess loss in outer cores is important in terms of homogeneous optical properties of all cores. The excess loss can be evaluated with the difference of confinement loss between cores. We simulate the confinement loss of a center core (CL_c) and an outer core (CL_o) with full vector finite element method [9] and define a simulated excess loss in outer cores (EL_{sim}) by the following equation.

$$EL_{\text{sim}} = CL_o - CL_c \quad (1)$$

Figure 3 shows simulation results of CL_o and CL_c as a function of OCT s. $r_1 = 5.13 \mu\text{m}$, $r_2 = 11.10 \mu\text{m}$, $r_3 = 16.00 \mu\text{m}$, $A = 40.7 \mu\text{m}$, $\Delta_1 = 0.260\%$, $\Delta_2 = 0.00\%$, $\Delta_3 = -0.70\%$ and $n_{\text{co}} = 1.486$. The wavelength of the simulation was 1.625 μm . The simulated CL_o was about six-digit larger than the CL_c for the simulated structure. Figure 4 shows EL_{sim} as a function of OCT . The OCT dependence of EL_{sim} was well fitted with an exponential function. The OCT should be larger than 38 μm to suppress EL_{sim} less than 0.001 dB/km.

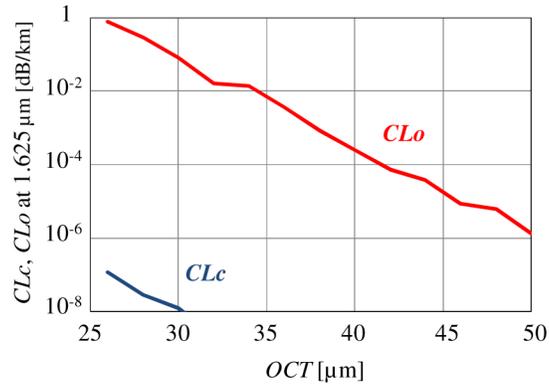


Fig. 3. Simulated confinement loss of a center core and an outer core as a function of OCT : A blue line is the confinement loss of a center core (CL_c). A red line is the confinement loss of outer core (CL_o).

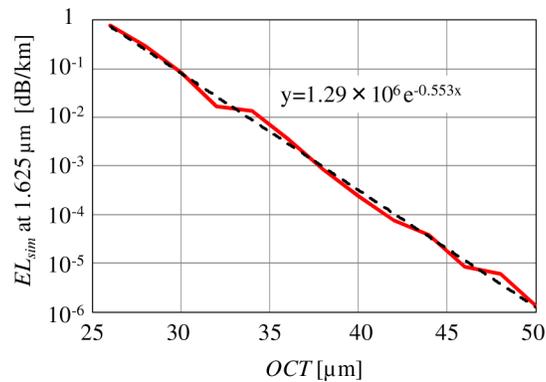


Fig. 4. Simulated excess loss of an outer core as a function of OCT : A red solid line is simulation results. A black dashed line is an exponential fitting line to the simulation results.

3. Characteristics of fabricated fibers

We fabricated three kinds of 7-core TA-MCF. Table 1 shows measurement results of fabricated fibers. Figure 5 shows a cross sectional view of a fabricated fiber (Fiber A). The OCT s of Fiber A, Fiber B and Fiber C were 31.6 μm , 33.6 μm and 47.7 μm , respectively. The coating thicknesses of the fabricated fibers were set to be same as the standard single-mode fiber. The outer-core crosstalk at 1.55 μm was measured on a fiber wound on a spool with a diameter of 210 mm according to the same measurement setup with Ref [1]. Figure 6(a) shows simulated cutoff wavelength as a function of core pitch A . The FEM [9] was used for the simulation. We selected A to be as small as possible while suppressing the lengthening of the cable cutoff wavelength [4]. Figure 6(b) shows 100-km crosstalk as a function of A . Three lines are the simulation results by the coupled power theory [10] for each fabricated MCF. Symbols indicate 100-km crosstalks that are estimated from the measured crosstalks on the fabricated fibers of a few km lengths by the coupled power theory. All the fibers have crosstalks of less than -30 dB at 100 km as designed.

Table 1. Measurement results of fabricated fibers. (* Optical properties of center core)

Item	Fiber A	Fiber B	Fiber C	
Core pitch [μm]	40.7	42.6	43.0	
Cladding thickness [μm]	31.6	33.6	47.7	
Cladding diameter [μm]	144.6	152.4	181.3	
Coating diameter [μm]	272	272	302	
MFD* [μm]	12.1	12.2	12.1	
A_{eff}^* [μm^2]	111.3	114.1	112.4	
Attenuation* at 1.55 μm [dB/km]	0.202	0.198	0.198	
Attenuation* at 1.625 μm [dB/km]	0.211	0.207	0.210	
Cable cutoff wavelength* [μm]	1.33	1.38	1.37	
Bending loss* at 1.625 μm ($r = 10\text{mm}$) [dB/m]	2.6	1.6	1.5	
Length [m]	2765	1765	1905	
Crosstalk at 1.55 μm [dB] (outer core)	average	-45	-55	-56
	max	-44	-54	-54
	min	-47	-56	-57

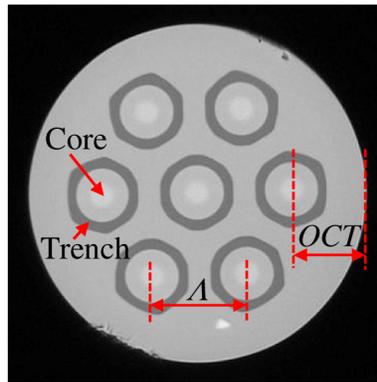


Fig. 5. Cross section of a seven-core TA-MCF (Fiber A).

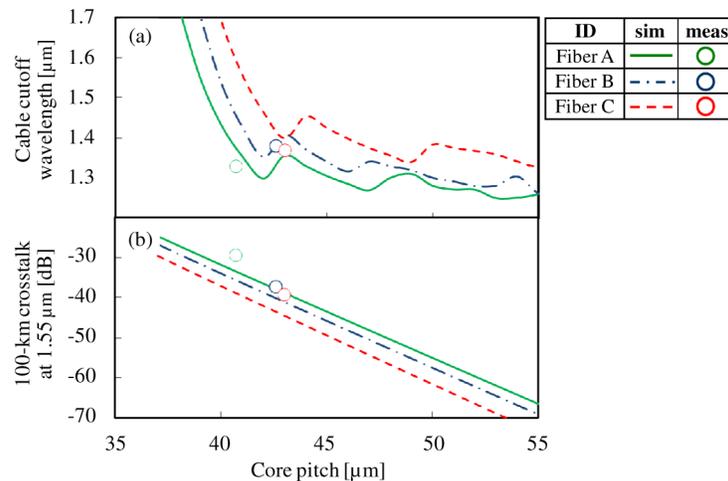


Fig. 6. Core pitch A dependence of (a) cable cutoff wavelength and (b) 100-km crosstalk: Lines are simulation results. Symbols are measurement results.

4. Consideration of the effect of coating thickness on micro-bending loss and excess loss

4.1 Micro-bending loss

Figure 7 shows measured micro-bending losses of the fabricated MCFs and SCFs. The micro-bending losses were measured at the condition as described in section 2.1. Open symbols were averaged micro-bending losses between outer cores and error bars denote maximum and minimum micro-bending losses of outer cores. The measured micro-bending losses of MCFs were smaller than those of SCFs with the same OCT and A_{eff} . No significant loss increase was observed even at the OCT of about 30 μm . We think that large glass diameter and the twisting along the longitudinal direction of MCFs would play a role in the reduction of micro-bending losses with comparison to SCFs. The micro-bending losses of the fabricated MCFs were slightly larger than that of a standard single-mode fiber (Step80, cladding diameter = 125 μm) and were smaller than that of a commercially available large A_{eff} fiber (Step110, cladding diameter = 125 μm). As the results, we can conclude that fabricated MCFs have enough performance for actual use in terms of micro-bending performance. The variations with micro-bending of crosstalk values were smaller than 2dB at the condition as described in section 2.1.

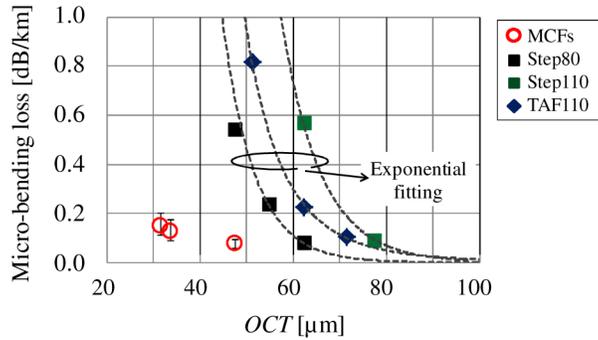


Fig. 7. Cladding thickness dependence of measured micro-bending loss of MCFs and single-core fibers at 1.625 μm : Red open symbols are averaged loss of the outer cores of MCFs. The error bar indicates maximum and minimum values of outer cores. Solid symbols and dashed line are data shown in Fig. 2.

4.2 Excess loss in outer cores

Figure 8 shows measured excess loss of outer cores at 1.625 μm as a function of OCT . The circle symbols were averaged excess losses of outer cores and error bars denote maximum and minimum excess losses of outer cores. A measured excess loss is defined by

$$EL_{\text{meas}} = \alpha_{\text{outer}} - \alpha_{\text{center}}, \quad (2)$$

where α_{outer} is an attenuation of an outer core and α_{center} is an attenuation of a center core. The dashed line is the approximated line of simulated results in Fig. 4. The solid line is an approximate line on the measured data with the same slope as the simulation line. Large excess loss was observed on outer cores of the MCFs with the OCT less than 35 μm and the trend of the measured excess loss well agreed with the simulation results. The reduction of OCT is probably limited around 40 μm in terms of the excess loss.

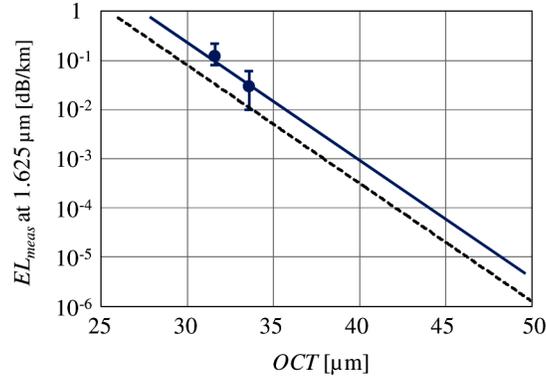


Fig. 8. Outer cladding diameter (OCT) dependence of measured excess loss (EL_{meas}) of fabricated MCFs at $1.625\ \mu\text{m}$: Symbols are averaged excess loss of fabricated MCFs. Error bars denote maximum and minimum EL_{meas} . The dashed line is the exponential fitting line shown in Fig. 4. The solid line is an approximation line on measured data with the same slope as the dashed line.

5. Core multiplicity factor

We introduce a core multiplicity factor (CMF) to compare the core density of MCFs. The CMF is given by

$$CMF = \frac{nA_{eff}}{\pi(D/2)^2}, \quad (3)$$

where n is a number of core with A_{eff} in a cladding and D is a cladding diameter. The CMF indicates the core area ratio in a cladding.

Figure 9 shows the contour plot of relative CMF ($RCMF$) on a 7-core MCFs for various A_{eff} and cladding diameter. The $RCMF$ is ratio between CMF of a MCF and a standard single core single mode fiber with $A_{eff} = 80\ \mu\text{m}^2$ at $1.55\ \mu\text{m}$ and cladding diameter = $125\ \mu\text{m}$. The $RCMF$ of the MCF in [3, 11] was about 3 because of the large cladding diameter. The $RCMF$ s of Fiber A, Fiber B and Fiber C were 7.3, 6.7 and 4.7, respectively. Fiber A and Fiber B realize the $RCMF$ larger than 6.5. However, the OCT s of the fibers are not applicable because the excess losses were observed on the fibers. The $RCMF$ of a TA-MCF with A_{eff} about $110\ \mu\text{m}^2$ and OCT of $40\ \mu\text{m}$ will reach to six without any excess loss. The $RCMF$ of six is two times larger than the previously reported large A_{eff} MCF.

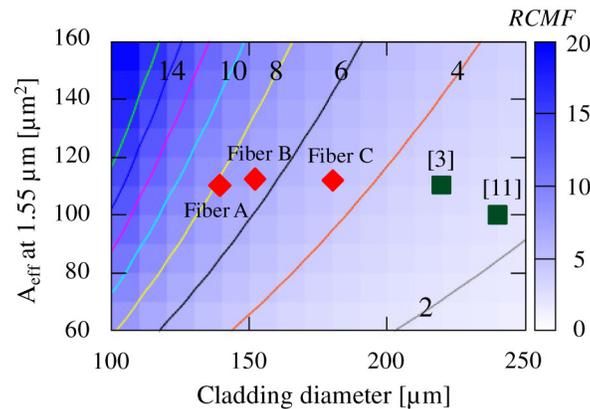


Fig. 9. Contour plot of $RCMF$ on a 7-core MCF for various A_{eff} and cladding diameter: Red symbols are measured data presented in this paper. Green symbols are previously reported data. Solid lines indicate counter lines of $RCMF$.

6. Conclusion

We investigated required cladding thickness of a MCF in terms of a micro-bending loss and an excess loss of outer cores theoretically and experimentally. No significant micro-bending loss increase was observed on MCFs with the cladding thickness of about 30 μm . The tolerance for the micro-bending loss of a MCF is larger than that of the SCF. However, the cladding thickness will be limited by the occurrence of the excess loss on outer cores. Our fabricated MCF realized a *RCMF* of 4.7 without any excess loss of outer cores. The *RCMF* of six, which is about two times larger than that of the previously reported large A_{eff} MCF, will be attainable on a TA-MCF with an optimized cladding thickness.

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