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Title	Estimation of uncertainty for massive Porites coral skeletal density
Author(s)	Sowa, Kohki; Watanabe, Tsuyoshi; Nakamura, Takashi et al.
Citation	JAMSTEC Report of Research and Development, 16, 31-39 https://doi.org/10.5918/jamstecr.16.31
Issue Date	2013-03
Doc URL	https://hdl.handle.net/2115/55799
Rights	Copyright 2013 by Japan Agency for Marine-Earth Science and Technology
Type	journal article
File Information	JAMSTEC_Rep_Res_Dev_16_31-.pdf



— Report —

Estimation of uncertainty for massive *Porites* coral skeletal density

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Previous studies have not demonstrated the estimate errors in growth parameters (skeletal density, extension rate and calcification rate) for massive coral skeletons. In order to discuss the variability of coral skeletal growth, it is crucial for quantitative evaluation of the parameters with errors. We report the protocol of calculating errors as combined standard uncertainty for coral skeletal density ($u_{\rho_{SA}}$) based on ISO/IEC Guide 98-3 (2008). We applied the non-destructive transparent X-ray 2-D imaging scanner, TATSCAN-X1, which enabled to quick and quantitative analysis of the $u_{\rho_{SA}}$ parameters with digital procedures. We analyzed the annual skeletal density for massive *Porites* coral collected from Ishigaki Island. The skeletal densities changed from 1.45 to 1.70 g/cm³ and $u_{\rho_{SA}}$ were ca. 0.02 g/cm³. Our results indicated that the $u_{\rho_{SA}}$ was derived from the combined effects of 78.5% from the standard uncertainty of deducing of analytical curve ($u_{\ln OD(Y) \rightarrow \rho_{SA}(X)}$) and 6.3% from that of the sample thickness error ($u_{t_{SA}}$).

Keywords: coral, skeleton, skeletal density, uncertainty, coral growth, TATSCAN-X1

Received 9 October 2012 ; Revised 13 December 2012 ; Accepted 14 December 2012

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1. Introduction

Coral calcification is one of the key indicators to quantify the influence of recent elevating sea surface temperature (SST) due to the global rising temperature (termed ocean warming) and declining pH of the upper seawater layers, due to the absorption of increasing atmospheric CO₂ (termed ocean acidification), which has potential to weaken the physiological activity such as scleractinia coral calcification rate (e.g. Langdon and Atkinson, 2005). The corals are one of the main reef-builder and they contribute up to 75% carbonate budgets of modern coral reefs (Hart and Kench, 2006). Thus, reduction of coral calcification will decrease the production of carbonate budget and the structural complexity of coral reefs where tens of thousands of species live.

Massive coral skeleton is useful for providing a long-term (over several hundred years) retrospective data about coral calcification trends where are no *in situ* environmental record. The corals grow by depositing an aragonitic skeleton and create successive growth bands with high and low porosity, termed skeletal density (Knutson et al., 1972). Growth bands provide the growth parameters of averaged skeletal density (g/cm³), annual extension rate (cm/year), and calcification rate (g/cm²/year). Annual calcification rate is a product of average annual skeletal density and annual extension rate (cf. Lough and Cooper, 2011). These growth parameters have been analyzed by the non-destructive methods of X-radiography, computed tomography (CT) and γ -densitometry (Carricart-Ganivet and Barnes, 2007; Bosscher, 1993; Chalker and Barnes, 1990).

In order to use coral skeleton as the past ocean historical record, quantitative evaluation of the coral growth parameters is essentially important. A coral chronology mainly performed by cross-validating skeletal density and geochemical signals (e.g. Bessat and Buigues, 2001) or suggesting the high/low-density band forms in same season for all analysis coral (e.g. Carricart-Ganivet et al., 2012; Carilli et al., 2012; Cooper et al., 2012; Helmle et al., 2011; Castillo et al., 2011; Cantin et al., 2010; De'ath et al., 2009; Cooper et al., 2008). As geochemical signals ($\delta^{18}\text{O}$, Sr/Ca ratio) can support chronologies through quantitative verification, coral growth parameters should be the primary data set. Depositional timing of high or low skeletal density area should be evaluated by geochemical signals or chemical staining methods for each sampling site because different deposition timing of high-density band has been reported (Rosenfeld et al., 2003; Klein et al., 1993; Lough and Barnes, 1990 review there in).

In the terms of quantitative evaluation of the coral growth parameters, estimation of errors for the parameters is necessary

(Miller and Miller, 1988) to compare data sets estimated by several methods such as CT and γ -densitometry. Although only an image analyzing software, Coral X-radiograph Densitometry System (CoralXDS), estimated the error of coral growth (available on the web site of the National Coral Reef Institute of Florida, USA; www.nova.edu/ocean/coralxds/index.html), there was no discussion about the error estimation. Thus, further studies needs to estimate the error of coral growth parameters.

The all digital procedure for coral X-radiograph would be recommended because the intensity were changed by every films and cassette, which caused the ca. 25% variation of optical density in the films (Carricart-Ganivet and Barnes, 2007). Non-destructive transparent X-ray 2-D imaging scanner, TATSCAN-X1 enable to analyze coral skeletal density with all digital procedures and would minimum the error estimation of skeletal density.

In this study, we present a new procedure for quantifying the coral skeletal density with uncertainty (e.g. ISO/IEC Guide 98-3, 2008) using all digital procedures of TATSCAN-X1 instrument developed at JAMSTEC.

2. Material and methods

2.1. Coral collection and digital X-radiography

We collected massive *Porites lutea* from sub-tidal area of several meter depths below low tide in the Shiraho fringing reef, Japan, on August 2009 (Fig. 1). The coral slab was cut the central growth axis using a rock saw equipped with diamond-tipped blade and water and flattened it.

The slab was rinsed with Milli-Q water with ultrasonically for several times, dried at 50°C in laboratory oven for one day and X-radiograph using TATSCAN-X1 with digital imaging intensifier X-ray camera. The digital image of X-radiography has positive and the resolution is 0.10638 mm/pixel. Exposure was 28.6 kV and 2.02 mA. It is possible to scan coral samples up to 1500 mm-long and 68 mm-wide. The X – Y stage was moved in the X-direction in 2.55 mm steps in this study. An X-radiography of the sample is synthesized by a successive image of 2.55 mm length and 68 mm width, which is extracted from the center of an image of 51 mm length and 68 mm width using Adobe Photoshop (Adobe Systems Incorporated, USA) and TSBsimpleanimator (TSB program systems, JAPAN).

2.2. Coral growth analysis

The coral growth of skeletal density, annual extension rate and calcification rate were calculated from the X-radiography. To correct the effects of inverse square law and heel effect (Carlton

and Adler, 1996) by comparing to the averaged optical density (OD) of Al-bar, we developed the software “CoreCal 2 (Dr. Nakamura Takashi, JAPAN)”. An aluminum bar with the same thickness as the coral slab was included on each digital X-radiograph, placed along X (horizontal) and Y (vertical) - axis of the X-ray machine, as well as an aragonitic step wedge built of blocks cut from a shell of the giant clam *Hippopus hippopus* as standards (STD) for analyzing coral skeletal density. The skeletal density of the giant clam was 2.85 g/cm^3 and synthesized standard uncertainty was $u_{p_{STD}} = 0.00223 \text{ g/cm}^3$. The averaged OD (the grey-scale value of pixels; 0–255) was used to obtain factors that corrected for the effects at any distance (d) on the X-radiography. X and Y line resulted when OD values for aluminum bars were adjusted in an X-radiography by CoreCal2 using following equation.

$$\text{Correction factor}_{(d)} = OD_{(d)} / OD_{\text{average}} \quad (1)$$

The OD was analyzed using the software Image J 1.46g (Wayne Rashband, National Institute of Health, USA). The OD , corrected digital X-radiographies, were used to measure the skeletal density along the vertical growth axis. The thickness of coral slices ($3.026 \pm 0.007 \text{ cm}$ with standard uncertainty in this study) was

measured 10 times along the growth axis using a set of calipers ($\pm 0.001 \text{ mm}$).

Skeletal density was calculated by the following equation (2~4). The procedure substitutes empirically derived constants for most of the assumptions that have been made by previous workers (Chalker et al, 1985; Carricart-Ganivet and Barnes, 2006). The analyzed OD s were converted to logarithmical ($\ln OD$) (Y). Plots of corrected $\ln OD$ values vs. thickness $\times$ density for each step of the aragonitic step-wedge resulted in 2-degree polynomial ($r^2 > 0.99$). The equation for 2-degree polynomial fit gave the relationship between the product (X) of aragonite density (ρ) and thickness of step-wedge aragonite (t) and Y :

$$Y = a + bX + cX^2 \quad (r^2 > 0.99) \quad (2)$$

where a , b and c were constants for 2-degree polynomial fit and derived from STD analysis.

The skeletal density of samples (ρ_{SA} ; g/cm^3) was calculated by the equations

$$\rho_{SA} = \frac{X_{SA}}{t_{SA}} \quad (3)$$

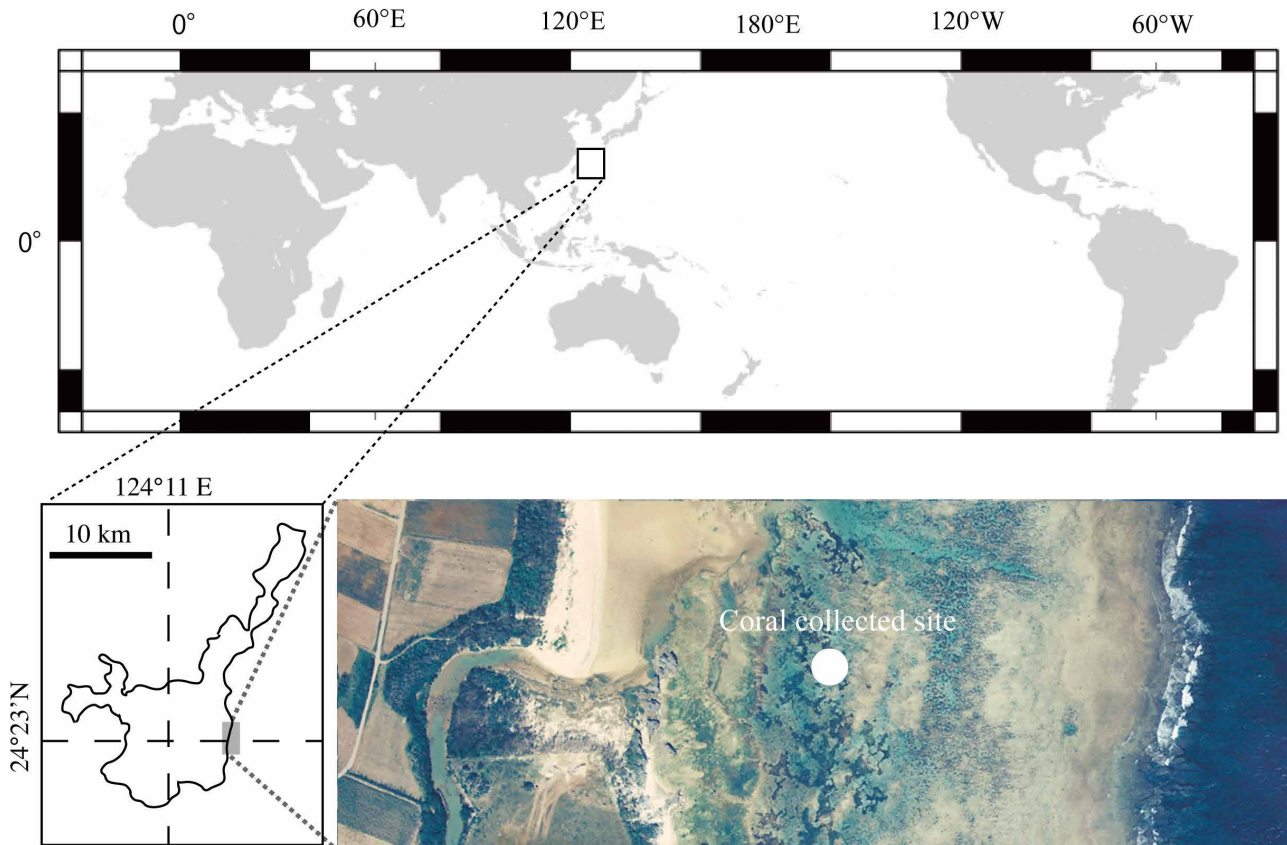


Fig. 1. Coral study area and sampling locality at Shiraho fringing reef, Ishigaki Island, Japan.

$$\begin{aligned} X_{SA} &= \frac{-b - \sqrt{b^2 - 4c(a-Y)}}{2c} \quad (\text{if } X_{STD(max)} < -\frac{b}{2c}) \\ X_{SA} &= \frac{-b + \sqrt{b^2 - 4c(a-Y)}}{2c} \quad (\text{if } X_{STD(max)} > -\frac{b}{2c}) \end{aligned} \quad (4)$$

where X_{SA} derived from Eq.(4). The t_{SA} denotes the sample thickness (cm).

2.3. Geochemical analysis ($\delta^{18}\text{O}$)

To determine the chronology of these corals skeleton, we analyzed stable oxygen and carbon isotope ratio ($\delta^{18}\text{O}$ and $\delta^{13}\text{C}$, respectively) of coral skeleton along the coral growth direction for coupled skeletal density band using a GV IsoPrime mass spectrometer with an automated carbonate system (IsoPrime Multiprep) at JAMSTEC. Oxygen isotope ratio were analyzed every 0.4 mm interval using Geomill326 (Izumo-web, JAPAN) for several cm long. The external precision (1σ) is $\sim \pm 0.064\%$ for $\delta^{18}\text{O}$ values and $\sim \pm 0.05\%$ ($N=10$) for $\delta^{13}\text{C}$ values. Oxygen isotope confirmed that the coral low-density band formed in high SST season (summer) and high-density band in lower SST season (winter). Annual bands were then identified manually between density maxima.

The coral growth parameters were calculated by mean annual skeletal density as the average skeletal density between adjacent annual skeletal density maxima (g/cm^3); mean annual extension rate as the linear distance between adjacent annual skeletal density maxima (cm/year).

3. The combined standard uncertainty of skeletal density ($u_{\rho_{SA}}$)

The $u_{\rho_{SA}}$ was based on ISO/IEC Guide 98-3 (2008). In general, numerical liner model is given in following equation.

$$y = f(x_1, x_2, \dots, x_N) \quad (5)$$

The component of combined uncertainty expressed as $u_c(y)$ is generated by the standard uncertainties expressed as $u(x_i)$. If there is no correlation between x_i and x_j ($j \neq i$). In general, following equation represents law of propagation.

$$u_c^2(y) = \sum_{i=1}^N \left(\frac{\partial f}{\partial x_i} \right)^2 u^2(x_i) \quad (6)$$

The partial derivatives $\partial f / \partial x_i$ are sensitivity coefficients.

Type A and B evaluation denotes the standard uncertainty of directly measurement and measurement machine (e.g. caliper) in this study. We applied rectangular distribution for all type B evaluations.

The $u_{\rho_{SA}}$ was (IV) combined the standard uncertainties of (I) thickness of standard (STD) and sample (SA), (II) skeletal density of STD and (III) analytical curve and soft-wear calibration.

(I) The standard uncertainty of STD ($u_{t_{STD}}$) and SA ($u_{t_{SA}}$) thickness derives from propagation of type A ($u_{t_{STD-A}}$, $u_{t_{SA-A}}$) of direct measurement and B evaluation (u_{t-B}) of the caliper. We adopted largest $u_{t_{STD}}$, which were applied for estimating analytical curve.

$$u_{t_{STD}}^2 = u_{t_{STD-A}}^2 + u_{t-B}^2 \quad (7)$$

$$u_{t_{SA}}^2 = u_{t_{SA-A}}^2 + u_{t-B}^2 \quad (8)$$

(II) The standard uncertainty of STD density ($u_{\rho_{STD}}$) is combined by the standard uncertainty of weight (u_w) and the volume (u_v), which are represented by the equations.

$$\rho_{STD} = \frac{W}{V} \quad (9)$$

$$u_{\rho_{STD}}^2 = \left(\frac{1}{V} \right)^2 u_w^2 + \left(-\frac{W}{V^2} \right)^2 u_v^2 \quad (10)$$

Where W and V are weight (g) and volume (cm^3) of STD respectively. There are no correlation between W and V .

The standard uncertainty of weight and volume are combined by type A and B evaluation respectively.

$$u_W^2 = u_{W-A}^2 + u_{W-B}^2 \quad (11)$$

$$u_V^2 = u_{V-A}^2 + u_{V-B}^2 \quad (12)$$

The standard uncertainty of the product of skeletal density and thickness of STD denoted by u_{X-STD} is represented by the equation.

$$u_{X-STD}^2 = t_{STD}^2 u_{\rho_{STD}}^2 + \rho_{STD}^2 u_{t-STD}^2 \quad (13)$$

Where the $u_{\rho_{STD}}$ and $u_{t_{STD}}$ is the standard uncertainty of the density and thickness of STD. Averaged skeletal density of STD is substituted for ρ_{STD} . The t_{STD} is adopted by largest value of STD, which were applied for estimating analytical curve.

(III) The standard uncertainty of OD in samples (u_{OD-SA}) is defined by combined type A and type B estimation. Type A estimation was selected as u_{OD-A} from maximum experimental standard deviation of Al-bar of X (u_{OD-A-X}) or Y axis (u_{OD-A-Y}) corresponding to coral skeletal analysis area.

$$u_{OD-A}^2 = u_{OD-A-X}^2 \text{ or } u_{OD-A-Y}^2 \quad (14)$$

Type B estimation is expressed as OD resolution of ± 0.5 (u_{OD-B}). The propagation is represented by the equation.

$$u_{OD-SA}^2 = u_{OD-A}^2 + u_{OD-B}^2 \quad (15)$$

The propagation of logarithmical conversion from OD to Y of u_{OD-SA} was expressed as u_{Y-SA} .

$$u_{Y-SA} = \frac{\partial Y}{\partial OD} u_{OD-SA} = \frac{1}{OD} u_{OD-SA} \quad (16)$$

The standard uncertainty of the sample derived from combination of analytical curve of two-degree polynomial formula ($u_{Y \rightarrow X}$) and u_{Y-SA} (u_{X-SA}) is calculated from the following equation.

$$Y = X\alpha + \varepsilon \quad (17)$$

Matrixes and vectors express each parameter.

$$Y = \begin{pmatrix} Y_1 \\ Y_2 \\ \vdots \\ Y_n \end{pmatrix}, X = \begin{pmatrix} 1, X_1, X_1^2 \\ 1, X_2, X_2^2 \\ \vdots \\ 1, X_n, X_n^2 \end{pmatrix}, \quad (18)$$

$$\alpha = \begin{pmatrix} a \\ b \\ c \end{pmatrix}, \varepsilon = \begin{pmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \vdots \\ \varepsilon_n \end{pmatrix}$$

Where n is number of standards used for estimating analytical curve, X_k is $X (= \rho_{STD} \cdot t_{STD})$ value of standard k ($= 1, 2, \dots, n$), and Y_k is measured $Y (= \ln OD)$ value of standard k . ε_k denotes the error of the 2-degree polynomial. Then, $\hat{a}$, $\hat{b}$, $\hat{c}$ are estimators of a , b , c respectively, and $\hat{\alpha}$ is estimator of vector α calculated by least square method.

$$\hat{\alpha} = (X^T X)^{-1} X^T Y \quad (19)$$

The uncertainties of $\hat{a}$, $\hat{b}$, $\hat{c}$ are expressed by u_a , u_b , u_c , which are estimated by the following equations. u_a^2 , u_b^2 , u_c^2 are diagonal components of eq. (20).

$$\sigma^2 = \frac{1}{n-3} (Y - X\hat{\alpha})^T (Y - X\hat{\alpha}) \quad (20)$$

$$(X^T X)^{-1} \sigma^2 = \hat{\Sigma} \quad (21)$$

In general, the law of propagation is expressed by following equation if there is correlation between x_i and x_j .

$$u_c^2(y) = \sum_{i=1}^N \left(\frac{\partial f}{\partial x_i} \right)^2 u^2(x_i) + 2 \sum_{i=1}^{N-1} \sum_{j=i+1}^N \frac{\partial f}{\partial x_i} \frac{\partial f}{\partial x_j} u(x_i, x_j) \quad (22)$$

Estimated correlation coefficient between x_i and x_j ($i < j$) is denoted by $r(x_i, x_j)$. The estimated covariance of x_i and x_j is denoted by $u(x_i, x_j)$. $u(x_i, x_j)$ were expressed the following equation.

$$u(x_i, x_j) = r(x_i, x_j) \times u(x_i) \times u(x_j) \quad (23)$$

When $c^T = \left(\frac{\partial f}{\partial x_1}, \frac{\partial f}{\partial x_2}, \dots, \frac{\partial f}{\partial x_N} \right)$ and V is expressed as

variance-covariance matrix of $u(x_i, x_j)$ ($u(x_i, x_i) = u^2(x_i)$). The $u_c(y)$ of eq. (22) is expressed by the following equation.

$$u_c^2(y) = c^T V c \quad (24)$$

In eq. (2), there is correlation among X . To evaluate the u_{X-SA} , eq. (2) converts to liner equation from non-liner one.

$$X = f(a, b, c, Y) \quad (25)$$

Then, the u_{X-SA} is expressed by the following equations.

$$u_{X-SA}^2 = c^T V' c' \quad (26)$$

$$c'^T = \left(\frac{\partial X}{\partial a}, \frac{\partial X}{\partial b}, \frac{\partial X}{\partial c}, \frac{\partial X}{\partial Y} \right) \quad (27)$$

$$V' = \begin{pmatrix} \hat{\Sigma} & 0 \\ 0 & u_{Y-SA}^2 \end{pmatrix} \quad (28)$$

and,

$$\begin{aligned} \frac{\partial X}{\partial a} &= -\frac{1}{2\hat{c}X_{SA} + \hat{b}} & \frac{\partial X}{\partial b} &= -\frac{X_{SA}}{2\hat{c}X_{SA} + \hat{b}} \\ \frac{\partial X}{\partial c} &= -\frac{X_{SA}^2}{2\hat{c}X_{SA} + \hat{b}} & \frac{\partial X}{\partial Y} &= -\frac{1}{2\hat{c}X_{SA} + \hat{b}} \end{aligned} \quad (29)$$

In this study, X_{SA} and Y_{SA} are defined as one time analysis. We referred to web site of Dr. Shirono K. (National Institute of Advanced Industrial Science and Technology, JAPAN; http://staff.aist.go.jp/k.shirono/index_e.html) for the calculation program of (III) section.

(IV) The u_{X-SA} is represented by the propagation in the following equation.

$$u_{X-comb}^2 = u_{X-SA}^2 + u_{X-STD}^2 \quad (30)$$

The $u_{\rho_{SA}}$ is represented and the following equation.

$$u_{\rho_{SA}}^2 = \left(\frac{1}{t_{SA}} \right)^2 u_{X-comb}^2 + \left(-\frac{X_{SA}}{t_{SA}^2} \right)^2 u_{t_{SA}}^2 \quad (31)$$

The t and X_{SA} are treated as individual quantity.

4. Results and Discussions

4.1 The coral skeletal density analysis by TATSCAN-XI

Stable isotopic and X-radiography evidence indicated that skeleton of greatest skeletal density was supposed as deposited in winter and did not show any evidence of sub-annual banding by cyclic variation of the oxygen isotope (Fig. 2). If we would compare coral growth and environmental data, we should check the depositional timing of coral skeleton for each slab or at least one slab at each site where environmental variation would be same.

The skeletal density, annual extension rate and calcification rate were measured based on chronology developed by oxygen isotope. Skeletal densities changed from 1.45 to 1.70 g/cm³ and $u_{\rho_{SA}}$ were ca. 0.02 g/cm³ (Table 1). Annual extension rate changed from 0.149 to 0.468 cm/year and calcification rate did from 0.237 to 0.722 g/cm²/year (Table 1).

4.2 Contribution of the uncertainty factors

Table 2 indicate the standard uncertainty and its factor of coral skeletal density collected at 200 m from inshore in 2008 as a typical rate. The 93.7% of $u_{\rho_{SA}}$ was explained by u_{X-comb} . The u_{X-SA} was mainly originated from $u_{Y \rightarrow X}$, which was 78.5% of $u_{\rho_{SA}}$. Any studies did not consider contribution of $u_{Y \rightarrow X}$. We will improve $u_{Y \rightarrow X}$ because it depends on the preparation of standard conditions such as thickness.

On the other hand, $u_{t_{SA}}$ would enhance $u_{\rho_{SA}}$ although the 6.3% of $u_{\rho_{SA}}$ was explained by $u_{t_{SA}}$. We calculated contribution of $u_{t_{SA}}$ in $u_{\rho_{SA}}$ calculated from eq.(31) (Fig. 3). The relative $u_{t_{SA}}$ was changed from ca. 0.23 to 4.0%. Then, $u_{\rho_{SA}}$ was changed from ca. 0.0175 to 0.05 g/cm³, which were corresponding to the contribution

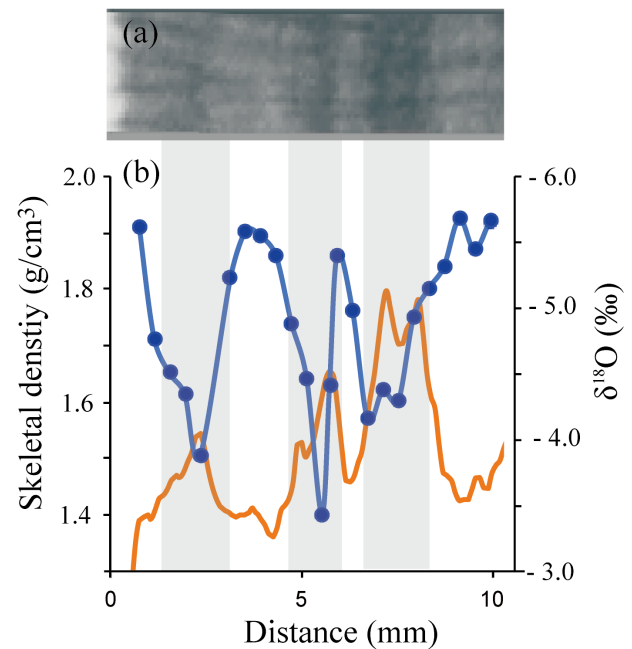


Fig. 2. (a) X-radiograph (0.10638 mm/pixel), and (b) comparison of skeletal density (orange line) and oxygen isotope (blue line with circles). Grey bar indicate high density bands estimated from X-radiography.

Table 1. Summary of annual coral growth with uncertainty.

Year	Skeletal density (g/cm ³)	Uncertainty of skeletal density (g/cm ³)	Extension rate (cm)	Calcification rate (g/cm ² /year)
2008	1.45	0.02	0.340	0.494
2007	1.59	0.02	0.149	0.237
2006	1.54	0.02	0.468	0.722
2005	1.54	0.02	0.372	0.572
2004	1.60	0.02	0.351	0.561
2003	1.66	0.02	0.330	0.548
2002	1.70	0.02	0.383	0.652

from 6 to 88.5% in $u_{\rho_{SA}}$. This indicates that $u_{t_{SA}}$ was one of the main factors for $u_{\rho_{SA}}$. Depend on study goals, we have to pay attention to the $u_{t_{SA}}$. Our protocol for estimating $u_{\rho_{SA}}$ basically enables to apply to γ -densitometry and CT analysis. Future research should estimate the uncertainties of coral growth to compare its information and machine conditions.

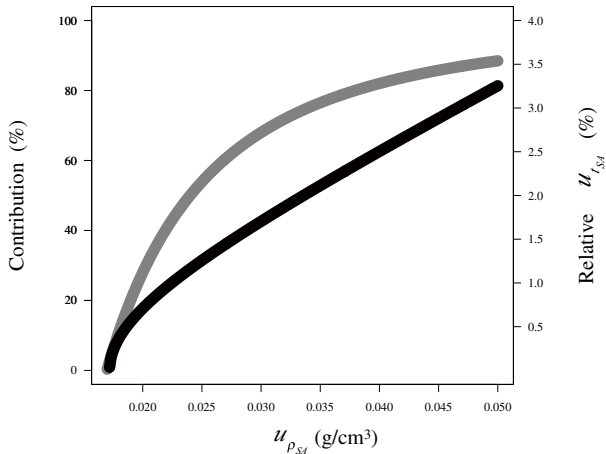


Fig. 3. The contribution of $u_{t_{SA}}$ to $u_{\rho_{SA}}$. The black lines indicate the contribution of square of sensitivity coefficients * $u_{t_{SA}}$ to that of sensitivity coefficients * $u_{\rho_{SA}}$ (Y-axis is left side). The gray lines indicate contribution of relative $u_{t_{SA}}$ to $u_{\rho_{SA}}$ (Y-axis is light side).

In this report, we did not show the uncertainty of extension rate and calcification rate. Most studies did not estimate coral extension rate and calcification rate because it was suggested that coral slab was collected perpendicular to the main vertical growth axis of the colony and there were small uncertainty (e.g. Knutson et al., 1972). If we use the hypothesis, we would calculate the uncertainty of extension rate by digital resolution and that of calcification rate by propagation of uncertainty of skeletal density and extension rate. However, Le Tissier et al. (1994) indicated that errors of density band related to coral growth parameters analyzed by X-radiography may be caused from (1) coral slab not following the growth axis of the colony, and (2) changes in corallite orientation. Although recent studies select and analyzed the maximum coral extension rate by CT to avoid the errors of density band (Carilli et al., 2012; Cantin et al., 2010), they did not clear the uncertainty of extension rate. Further basic studies for estimating uncertainty of coral growth would be needed in the future.

This study reported the new protocol for estimating $u_{\rho_{SA}}$ by TATSCAN-X1, developed at JAMSTEC, for the first time. Our results indicate that the $u_{\rho_{SA}}$ is derived from the combined effects of 78.5% from $u_{Y \rightarrow X}$, and 6.3% from $u_{t_{SA}}$. The $u_{t_{SA}}$ depends on cutting technique of coral skeleton. The coral core center, constructed in Hokkaido University, Japan, had the machine for cutting the

Table 2. Summary of contribution of each standard uncertainty for $u_{\rho_{SA}}$.

Evaluation type	Growth parameter	Uncertainty (u)	Rate (%)
	Skeletal density (g/cm^3 ; $u_{\rho_{SA}}$)	1.75E-02	100.0
	Square of sensitivity coefficients * uncertainty		
(A)	Sample thickness (cm; $u_{t_{SA}}$)	4.39E-03	6.3
(B)	Deducing of analytical curve + STD ($u_{X\text{-comb}}$)	1.70E-02	93.7
(B-1)	Deducing of analytical curve (X ; $u_{X\text{-SA}}$)	1.61E-02	84.8
(B-2)	STD ($u_{X\text{-STD}}$)	5.23E-03	8.9
(B-1-1)	Deducing of analytical curve ($u_{Y \rightarrow X}$)	1.55E-02	78.5
(B-1-2)	Type B (u_{OD-B})	2.77E-03	2.5
(B-1-3)	Al-bar (u_{OD-A})	3.44E-03	3.8
(B-2-1)	Thickness of STD ($u_{t_{STD}}$)	5.60E-04	0.1
(B-2-2)	Density of STD ($u_{t_{STD}}$)	5.20E-03	8.8

flattened coral slab with 100 μm interval. If we use the machine and TATSCAN-X1, we would get the minimum uncertainty of skeletal density.

Acknowledgments

We thank to Mr. Jumpei Isasa, Suguru Kawamura and Masataka Ikeda for field assistance. We also thank to Mr. Koichi Iijima for research advice. The authors acknowledge Hidehiko Nomura, Kosuke Nakamura at Thin Section Technician's Lab, Hokkaido University for technical advising of sample preparation. The authors are grateful to Dr. Kazumasa Oguri and to anonymous reviewers for their corrections and comments, which help improving that manuscript.

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