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Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

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In order to better predict kinetic behavior of a nuclear fission reactor, improvement of delayed neutron parameters is essential. Since it is required to establish a path from the microscopic nuclear data to the macroscopic delayed neutron parameters for the improvement, the present paper identifies important nuclear data for reactor kinetics. Sensitivities of the reactor stable period, which describes reactor kinetic behavior, to microscopic nuclear data such as independent fission yields, decay constants and decay branching ratios are calculated efficiently by using the adjoint kinetics equation. Furthermore, nuclide-wise and nuclear data-wise uncertainties of the reactor stable period are quantified using the variance data given in the nuclear data file, and the nuclear data which require further improvement are identified.

The results obtained through the present study are quite helpful, and can be a driving force of further nuclear physic studies.

KEYWORDS: *reactor kinetics, reactor stable period, one-point adjoint kinetics equations, fission yield, decay constant*

1. Introduction

The reactor stable period, which is a time constant describing kinetic behavior of a nuclear fission reactor, is quite an important measurable parameter. By putting a value of the reactor stable period into the well-known inhour equation, we can deduce a reactivity of a reactor and quantify how far the reactor state is from a critical state, *i.e.*, a balanced state from a view point of fission chain reactions. Even though a very small fraction of fission neutrons is emitted from fission product nuclides with some of time delay, these neutrons, called as delayed neutrons, play a crucial role in fission chain reactions especially below a prompt critical state.

The inhour equation which gives a relation between a reactivity and a reactor stable period includes some physical parameters such as fission yields and decay constants of delayed neutron precursors. Since there are so many fission product nuclides which or whose daughter nuclides emit delayed neutrons after radioactive decay, these fission product nuclides are grouped to a few *families* in accordance with their decay constants, and the grouped delayed neutron precursors are treated in the inhour equation. From the very old day when the nuclear energy utilization began, the delayed neutron precursors have been grouped into the six families and the treatment of the six-group delayed neutron precursors has been widely applied[1, 2]. It should be noted that the eight-group treatment was also proposed about ten years ago in order to improve the prediction of reactor behavior under a large negative reactivity insertion, and the JEFF-3.1 nuclear data library adopts the eight-group parameters[3].

A challenge by Brady and England made in 1989 have shown us a new possibility to

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improve the delayed neutron-related data[4]. They have evaluated the delayed neutron-related physical data for each fission product nuclide with the measurement data and model calculation results, have performed a summation calculation using the evaluated delayed neutron data and have fitted the six-group constants to the results of the summation calculation. This challenge connects the microscopic nuclear data with the macroscopic grouped delayed neutron data, and it gives us a possibility to better understand reactor kinetic behavior through studying the fundamental nuclear physics. The delayed neutron parameters evaluated by Brady and England have been adopted in the ENDF/B-VI nuclear data library and also the latest version of the ENDF/B library, ENDF/B-VII.1.

Though the work done by Brady and England has played quite an important role in this field, a problem of their evaluated parameters has been pointed out by some authors[5, 6]. While the widely used delayed neutron parameters evaluated by Keepin yields consistent results with experimental data for the reactor kinetic behavior, some deficiencies have been observed when Brady and England's data are used. When the same value of the reactor stable period is given, a reactivity value deduced with Brady and England's delayed neutron parameters is over 10% lower than that deduced with Keepin's data for the uranium-235 thermal fission. This difference is significantly large from a view point of actual application.

A study done by Oyamatsu has addressed this issue[7]. He has pointed out that the iodine-137 contribution may be responsible for the difference between Keepin's evaluated parameters and Brady&England's parameters, and also has quantified a nuclide-wise contribution to the reactor stable period T at a limit of $T \rightarrow \infty$. He has identified some delayed neutron precursors which have strong influence on the reactor kinetic behavior.

More recently, the present authors have carried out a sensitivity analysis[8] for the

reactor stable period in order to identify important delayed neutron-related nuclear data with a different approach to Oyamatsu's work. They have used an adjoint equation of the one-point reactor kinetics equation and have quantified importance of fission product nuclides for the reactor kinetics. Since their approach is not restricted to a limit of $T \rightarrow \infty$ as Oyamatsu's work, they have obtained information which complements Oyamatsu's preceding work. They have also calculated sensitivities of the reactor stable period to the delayed neutron-related nuclear data using several different nuclear data files, and have shown that there are large differences in the sensitivities among the different nuclear data files even though currently evaluated nuclear data files are used.

While there have been several works on the adjoint reactor kinetics equation, its application to the one-point equation with the explicit fission product treatment is new as far as authors' knowledge. Here we cite only two papers on the adjoint reactor kinetics equation.[9, 10] The paper written by van Rooijen and Lathouwers presents a sensitivity analysis for six-group delayed neutron data in multi-dimensional problems.

Once sensitivities of the reactor stable period to nuclear data are obtained, uncertainty propagation calculations from nuclear data to the reactor stable period can be easily done. In the present study, the uncertainty of the reactor stable period is quantified using the sensitivities calculated with the manner proposed in the previous study and uncertainty information given in the nuclear data file. By quantifying nuclide-wise and nuclear data-wise uncertainties in the reactor stable period, delayed neutron data which should be more precisely measured and/or more accurately modeled can be identified. Such an information can be a driving force of further nuclear physic studies.

Due to the page limitation, reference [8] gives the very brief theoretical background of sensitivity calculations with the adjoint kinetics equation and limited numerical examples

only for the uranium-235 and plutonium-239 thermal fission cases. In order to complement the previous paper, the present paper includes very detail description of the theoretical background and gives numerical results for the plutonium-239 and uranium-238 fast fission cases in addition to the thermal fission cases.

The present paper is organized as follows. Section 2 explains the one-point reactor kinetics equation and its adjoint form, and a theory of sensitivity calculations using the adjoint function. In Sec. 3, a numerical procedure and used nuclear data are described, and we will show sensitivities of reactor stable periods to fission yields and decay constants of fission product nuclides, and nuclide-wise and nuclear data-wise uncertainties in the reactor stable period for various types of fissioning systems. These are summarized in Sec. 4.

2. Theory

2.1. One-point reactor kinetics equation and its adjoint form

The theory of the adjoint kinetics equation has been well established. Here it is briefly described for readers' benefits.

Let us consider a system to which a constant (time-independent) reactivity ρ is added.

The one-point reactor kinetics equations are written as follows:

$$\frac{dn(t)}{dt} = \frac{\rho - \beta}{\Lambda} n(t) + \sum_{i=1}^N \lambda_i C_i(t) P n_i, \quad (1)$$

$$\frac{dC_i(t)}{dt} = \frac{y_i}{\nu \Lambda} n(t) - \lambda_i C_i(t) + \sum_{j=1}^N \lambda_j C_j(t) P_{ji}, \quad (i = 1, \dots, N), \quad (2)$$

where $n(t)$ is the number of neutrons at time t , Λ is the neutron generation time, ν is the averaged number of neutrons emitted by a fission reaction, and N denotes the total

number of considered fission product nuclides. Parameters C_i , Pn_i , y_i , λ_i denote a number density, a neutron emission probability per a decay, a fission yield and a decay constant of a fission product nuclide i . β is a delayed neutron fraction and is defined as

$$\beta = \frac{\sum_{i=1}^N \bar{y}_i Pn_i}{\nu} = \frac{\sum_{i=1}^N y_i D_i}{\nu}, \quad (3)$$

where $\bar{y}_i$ is the cumulative fission yield and D_i the total number of emitted delayed neutrons per a generation of nuclide i : total number of delayed neutrons emitted by the nuclide i and its all daughter nuclides. P_{ji} gives a probability that nuclide i is produced by a decay of nuclide j . Equations (1) and (2) consider delayed neutron emissions from not only precursors which are generated directly by a fission reaction but also those generated by a radioactive decay of a parent fission product nuclide. This effect is referred to as a decay chain effect in the present paper. The importance of the decay chain effect has been pointed out in the previous studies.[11, 12]

If we neglect the decay chain effect and assume that all the delayed neutron precursors are generated instantaneously by a fission reaction, the one-point kinetics equations can be simply written as follows:

$$\frac{dn(t)}{dt} = \frac{\rho - \beta}{\Lambda} n(t) + \sum_{i=1}^N \lambda_i C_i(t) Pn_i, \quad (4)$$

$$\frac{dC_i(t)}{dt} = \frac{\bar{y}_i}{\nu \Lambda} n(t) - \lambda_i C_i(t), \quad (i = 1, \dots, N). \quad (5)$$

In this case, relation between a reactivity ρ and a reactor stable period T can be easily derived as

$$\rho = \frac{l}{T + l} + \frac{T}{T + l} \sum_{i=1}^N \frac{\beta_i}{1 + \lambda_i T}, \quad (6)$$

where l denotes a prompt neutron life time and $\beta_i = \bar{y}_i Pn_i / \nu$.

For the purpose of the present study, the one-point kinetics equations (1) and (2) are

rewritten as follows:

$$\frac{dn(t)}{dt} = \frac{k_p - 1}{l} n(t) + \sum_{i=1}^N \lambda_i C_i(t) P n_i, \quad (7)$$

$$\frac{dC_i(t)}{dt} = \frac{k_p}{l} \frac{y_i}{\nu_p} n(t) - \lambda_i C_i(t) + \sum_{j=1}^N \lambda_j C_j(t) P_{ji}, \quad (i = 1, \dots, N), \quad (8)$$

where k_p is a prompt neutron multiplication factor which neglects delayed neutron contributions to a fission chain reaction and ν_p is the averaged number of prompt neutrons emitted by a fission reaction. For simplicity, these equations are written in a matrix form as

$$\frac{d\mathbf{y}}{dt} = \mathbf{A}\mathbf{y}, \quad (9)$$

where $\mathbf{y} = (n, C_1, C_2, \dots, C_N)^T$. An adjoint equation to Equation (9) can be easily derived as

$$-\frac{d\mathbf{y}^\dagger}{dt} = \mathbf{A}^T \mathbf{y}^\dagger, \quad (10)$$

where $\mathbf{y}^\dagger = (n^\dagger, C_1^\dagger, C_2^\dagger, \dots, C_N^\dagger)^T$. Its explicit form is given as

$$-\frac{dn^\dagger(t)}{dt} = \frac{k_p - 1}{l} n^\dagger(t) + \sum_{i=1}^N \frac{k_p}{l} \frac{y_i}{\nu_p} C_i^\dagger(t), \quad (11)$$

$$-\frac{dC_i^\dagger(t)}{dt} = \lambda_i P n_i n^\dagger(t) - \lambda_i C_i^\dagger(t) + \sum_{j=1}^N \lambda_i C_j^\dagger(t) P_{ij}, \quad (i = 1, \dots, N). \quad (12)$$

2.2. Sensitivity of reactor stable period to delayed neutron data

A reactor stable period T can be defined from the numbers of neutrons at two different time points t_1 and $t_2 = t_1 + \Delta t$ in an asymptotic state as

$$T = \frac{\Delta t}{\ln \{n(t_2)/n(t_1)\}}. \quad (13)$$

A derivative of T to a delayed neutron data p , such as a fission yield and a decay constant, can be calculated as

$$\frac{\partial T}{\partial p} = \frac{\partial T}{\partial n(t_1)} \frac{\partial n(t_1)}{\partial p} + \frac{\partial T}{\partial n(t_2)} \frac{\partial n(t_2)}{\partial p}. \quad (14)$$

In order to obtain $\frac{\partial T}{\partial p}$, it is required to calculate $\frac{\partial n(t_1)}{\partial p}$ and $\frac{\partial n(t_2)}{\partial p}$. These derivatives can be obtained numerically by taking a difference of two numerical results: a base result and a perturbed result. This approach, however, requires so many cases of numerical calculations. In the present study, we propose to use the adjoint function $\mathbf{y}^\dagger$ to calculate these derivatives as follows.

By differentiating the both sides of Equation (9) by p , we can obtain

$$\frac{d}{dt} \left(\frac{d\mathbf{y}}{dp} \right) = \frac{d\mathbf{A}}{dp} \mathbf{y} + \mathbf{A} \frac{d\mathbf{y}}{dp}. \quad (15)$$

Multiplying $\mathbf{y}^{\dagger T}$ to the both sides of this equation and integrating them on $0 \leq t \leq t_k$, we obtain

$$\int_0^{t_k} dt \left\{ \mathbf{y}^{\dagger T} \frac{d}{dt} \left(\frac{d\mathbf{y}}{dp} \right) \right\} = \int_0^{t_k} dt \left(\mathbf{y}^{\dagger T} \frac{d\mathbf{A}}{dp} \mathbf{y} \right) + \int_0^{t_k} dt \left(\mathbf{y}^{\dagger T} \mathbf{A} \frac{d\mathbf{y}}{dp} \right). \quad (16)$$

This equation can be rewritten as

$$\left[\mathbf{y}^{\dagger T} \frac{d\mathbf{y}}{dp} \right]_0^{t_k} = \int_0^{t_k} dt \left(\mathbf{y}^{\dagger T} \frac{d\mathbf{A}}{dp} \mathbf{y} \right) + \int_0^{t_k} dt \left\{ \frac{d\mathbf{y}^T}{dp} \left(\mathbf{A}^T \mathbf{y}^\dagger + \frac{d\mathbf{y}^\dagger}{dt} \right) \right\}. \quad (17)$$

Note that

$$\mathbf{y}^{\dagger T} \mathbf{A} \frac{d\mathbf{y}}{dp} = \left(\mathbf{y}^{\dagger T} \mathbf{A} \frac{d\mathbf{y}}{dp} \right)^T = \frac{d\mathbf{y}^T}{dp} \mathbf{A}^T \mathbf{y}^\dagger \quad (18)$$

since $\mathbf{y}^{\dagger T} \mathbf{A} \frac{d\mathbf{y}}{dp}$ is scalar. Using Equation (10), Equation (17) is transformed to

$$\mathbf{y}^{\dagger T}(t_k) \frac{d\mathbf{y}(t_k)}{dp} - \mathbf{y}^{\dagger T}(0) \frac{d\mathbf{y}(0)}{dp} = \int_0^{t_k} dt \left(\mathbf{y}^{\dagger T} \frac{d\mathbf{A}}{dp} \mathbf{y} \right). \quad (19)$$

Since the initial condition for $\mathbf{y}$ is given, the second term of the left hand side of the above equation is zero. Now we are interested in a derivative of the number of neutrons

to p at $t = t_k$. In order to obtain this quantity, we set the final condition of $\mathbf{y}^\dagger$ as $\mathbf{y}^\dagger(t_k) = (1, 0, \dots, 0)^T$, and then we can obtain the following equation:

$$\frac{\partial n(t_k)}{\partial p} = \int_0^{t_k} dt \left(\mathbf{y}^{\dagger T} \frac{d\mathbf{A}}{dp} \mathbf{y} \right). \quad (20)$$

Since the derivative $\frac{d\mathbf{A}}{dp}$ can be easily calculated, the derivative $\frac{\partial n}{\partial p}$ is also easily calculated using $\mathbf{y}$ and $\mathbf{y}^\dagger$.

The physical meaning of $\mathbf{y}^\dagger$ can be explained as follows. By multiplying $\mathbf{y}^{\dagger T}$ to the both sides of Equation (9) and $\mathbf{y}^T$ to the both sides of Equation (10), integrating them over $t' \leq t \leq t_k$, and subtracting one by another, we obtain the following equation:

$$[\mathbf{y}^T \mathbf{y}^\dagger]_{t'}^{t_k} = 0. \quad (21)$$

Since $\mathbf{y}^\dagger(t_k) = (1, 0, \dots, 0)^T$, we obtain the following relation:

$$n(t_k) = \mathbf{y}^{\dagger T}(t') \mathbf{y}(t') = n^\dagger(t') n(t') + \sum_{i=1}^N C_i^\dagger(t') C_i(t') = \hat{n}(t') + \sum_{i=1}^N \hat{C}_i(t'). \quad (22)$$

From this equation, we can find that $\hat{n}(t')$ and $\hat{C}_i(t')$ are *ancestors* at $t = t'$ of neutrons at $t = t_k$, and those divided by $n(t_k)$ are relative contributions of neutrons and fission product nuclides at $t = t'$ to the neutrons at $t = t_k$.

While the averaged number of delayed neutrons emitted per a fission reaction ν_d is accurately measured generally, delayed neutron-related data such as independent fission yield and decay branching ratio for each fission product nuclide are not the case. Thus ν_d calculated from the delayed neutron data for fission product nuclides does not agree with ν_d given in a general-purpose nuclear data file. In order to reproduce ν_d given in the JENDL-4.0 nuclear data file from the microscopic nuclear data, we normalize all the fission yield values in the present study. This normalization should be considered when we calculate sensitivities to delayed neutron data which affect the ν_d value. For example,

let us consider a sensitivity to a fission yield of nuclide j , y_j . When a perturbation Δy_j is given to y_j , the following relation holds:

$$\sum_{i=1}^N (y_i + \Delta y_j \delta_{ij}) D_i = \nu_d + \Delta y_j D_j, \quad (23)$$

where δ_{ij} is Kronecker's delta. This equation can be transformed to

$$\sum_{i=1}^N \frac{\nu_d}{\nu_d + \Delta y_j D_j} (y_i + \Delta y_j \delta_{ij}) D_i = \sum_{i=1}^N y'_i D_i = \nu_d. \quad (24)$$

Thus a change in y_i , Δy_i , can be written as

$$\Delta y_i = y'_i - y_i = \frac{\Delta y_j}{\nu_d + \Delta y_j D_j} (\nu_d \delta_{ij} - D_j y_i) \approx \frac{\Delta y_j}{\nu_d} (\nu_d \delta_{ij} - D_j y_i), \quad (25)$$

and the following equation is derived:

$$\frac{dy_i}{dy_j} = \delta_{ij} - \frac{D_j y_i}{\nu_d}. \quad (26)$$

When the normalization of fission yields is considered, the *constrained* sensitivity of the reactor stable period T to the fission yield y_j , $\bar{S}_j$, can be written as

$$\begin{aligned} \bar{S}_j &= \left(\frac{\partial T}{\partial y_j} \right) \left(\frac{y_j}{T} \right) = \sum_{i=1}^N \left(\frac{\partial T}{\partial y_i} \right) \left(\frac{y_i}{T} \right) \left(\frac{y_j}{y_i} \right) \left(\frac{dy_i}{dy_j} \right) \\ &= \sum_{i=1}^N S_i \frac{y_j}{y_i} \left(\delta_{ij} - \frac{D_j y_i}{\nu_d} \right) = S_j - \frac{D_j y_j}{\nu_d} \sum_{i=1}^N S_i, \end{aligned} \quad (27)$$

where S_i denotes the *unconstrained* sensitivity to y_i .

Note that another normalization is considered in the case of calculating sensitivities to a decay branching ratio; a sum of all the values of branching ratio should be unity.

3. Numerical result

3.1. Numerical procedure

We numerically solve the one-point reactor kinetics equations (7) and (8) with a fixed value of k_p , and obtain a corresponding reactor stable period. Decay data of fission product nuclides such as decay constants, decay modes and their branching ratios are taken from the JENDL FP Decay Data File 2011 (JENDL/FPD-2011)[13]. Fission yield data are taken from the JENDL FP Fission Yields Data File 2011 (JENDL/FPY-2011)[13]. In the present calculation, thermal fissions by uranium-235 and plutonium-239, and fast fissions (at 500 keV) by plutonium-239 and uranium-238 are considered.

At an initial time step, a unit neutron and some delayed neutron precursors are introduced to a system. The number densities of the delayed neutron precursors at the initial time step, $C_i(0)$, is set as

$$C_i(0) = \frac{k_p y_i}{\lambda_i l \nu_p}, \quad (28)$$

which is an estimate of the number densities in a critical state. The kinetics equation is solved with fine time steps ($\Delta t=0.1[s]$) under a constant (time-independent) reactivity: a fixed value of k_p . After a system reaches to its asymptotic state, a reactor stable period is calculated. Prompt neutron life time is assumed 1.5×10^{-5} seconds for the thermal fission cases and 1.5×10^{-7} seconds for the fast fission cases. The forward and adjoint kinetics equations are solved by the matrix exponential method with the Chebyshev rational approximation[14].

3.2. Relation between reactivity and reactor stable period

Relation between a reactivity and a reactor stable period is numerically obtained. In the present study, the prompt neutron multiplication factor is regarded as a reactivity-related parameter for convenience. **Figure 1** shows the relation between a prompt neutron multiplication factor and a reactor stable period above the delayed critical for thermal fissions as an example.

Next, we evaluate the decay chain effect on the relation between reactor stable period and prompt neutron multiplication factor for the thermal fission cases. **Figure 2** shows a relative difference between two reactor stable periods deduced from the same prompt neutron multiplication factor; one is calculated with the decay chain effect consideration and the other is calculated without its consideration. When the chain effect is considered, delayed neutron precursors which are daughter nuclides of other fission product nuclides are produced by decay of the parent nuclides after a fission reaction, and then they emit delayed neutrons after decay. On the other hand, these delayed neutron precursors are generated instantaneously after a fission reaction and emit delayed neutrons according to their decay constants when the decay chain effect is neglected. Thus considering the decay chain effect makes the reactor stable period longer. The reason why the larger effect is observed in the uranium-235 fission will be discussed later.

3.3. Ancestor quantifications

As described in the preceding section, ancestors of neutrons at a certain time can be quantified with the function $\hat{C}_i(t)$ as shown in Equation (22). As an example, ancestors of neutrons are calculated for the uranium-235 thermal fission with different values of k_p (or

reactor stable period). **Figures 3 to 5** show relative contributions of fission product nuclides iodine-137, bromine-88, -89, -90 and rubidium-94 as ancestors of neutrons at $t = 0$. As the time t approaches to zero, the contributions of fission products having long half-lives such as iodine-137 (24.5 seconds) and bromine-88 (16.5 seconds) decrease and those having short half-lives such as rubidium-94 (2.7 seconds) and bromine-89 (4.4 seconds) increase. It is interesting to see that the contribution of each ancestor nuclide converges to a constant value as the time t becomes far from zero. In order to see dependence of these converged values of ancestor contributions on a reactor stable period T , ancestor contributions are calculated at $t = -3T$ with different values of T . **Table 1** shows summary of the results. In the case of a long reactor stable period, fission product nuclides having long half-lives show large contributions. This result suggests that sensitivities of reactor stable period to nuclear data such as decay constants and fission yields depend on a value of a reactor stable period.

3.4. Sensitivity calculations

Sensitivities of reactor stable periods to fission yields and decay constants are calculated using Equations (14) and (20) with different values of reactor stable period. Note that all the sensitivities shown in the present section are relative ones: $\{(\partial T / \partial p) / (T / p)\}$.

Firstly two types of sensitivities, constrained and unconstrained sensitivities, are compared with each other. **Figure 6** shows these two sensitivities to fission yields, which are calculated for the uranium-235 thermal fission with a reactor stable period of about 100 seconds. All the unconstrained sensitivities take negative values since an increase in the fission yield results in an increase of ν_d , an averaged number of delayed neutrons. It is

easily understood that the increase of ν_d under a constant value of ν_p makes the reactor stable period shorter since the averaged number of fission neutrons ν also increases. The magnitude of unconstrained sensitivities of nuclide i is determined from an independent fission yield y_i , a total number of emitted neutrons per a nuclide generation D_i , and half-lives of delayed neutron precursors which are generated from the nuclide i ; the sensitivity of nuclide i takes a large value if y_i and D_i are large and the half-lives of related precursors are short. **Table 2** summarizes the fundamental data related to delayed neutron emission for some fission product nuclides. Since daughter nuclides of some of these nuclides such as germanium-86 and selenium-87 can be also delayed neutron precursors, an effective half-life is newly introduced here. A delayed neutron precursor i with unit number density is introduced at an initial state and a time-dependent delayed neutron emission rate is numerically calculated. Then the effective half-life is defined as a time when a delayed neutron emission rate becomes half relative to its initial value. The effective half-life is also shown in Table 2. Please remember that time behavior of delayed neutron emission rate for these nuclides cannot be described by a unique exponential function. Taking selenium-87 for example, the delayed neutron emission rate increases for a while after the unit selenium-87 is introduced, and then it begins to decrease with the half-life of the daughter nuclide, bromine-87. The effective half-life of germanium-86 is longer than the physical half-life since its daughter nuclide arsenic-86 has long half-life of 0.945 second and large branching ratio to decay channel with neutron emission. The large value of the germanium-86 unconstrained sensitivity can be understood from a large value of D_i and a small value of the effective half-life. On the other hand, even though the product of y_i and D_i of iodine-137 is also large, the iodine-137 unconstrained sensitivity is not as large as the germanium-86 sensitivity. This is because the half-life of iodine-137 is much longer

than the effective half-life of germanium-86.

The constrained sensitivities take both positive and negative values. Signs of constrained sensitivities are determined from (effective) half-lives of delayed neutron precursors. As shown in Equation (27), a difference between constrained and unconstrained sensitivities becomes significant if a product of y_i and D_i is large. When contribution of short-lived precursors such as germanium-86 and bromine-90 becomes large, a reactor stable period becomes short. Thus the constrained sensitivities are negative. On the other hand, when contribution of long-lived precursors such as iodine-137 becomes large, a reactor stable period becomes long. In the following, only the constrained sensitivities will be considered.

Sensitivities of reactor stable periods to independent fission yields are shown in **Tables 3 to 6** for various types of fissioning systems. Sensitivities whose absolute values are larger than 0.02 are only shown and relatively large sensitivities (larger than 0.1) are shown in bold characters. Sensitivities to fission yields of bromine isotopes in the uranium-235 thermal fission are larger than those in other cases and those to fission yields of iodine isotopes in the plutonium-239 fission cases are larger than those in the uranium fission cases. A sensitivity to the germanium-86 fission yield is large only in the uranium-235 thermal fission case since a large fission yield value of 0.00628 is given in the uranium-235 thermal fission.

Similarly, sensitivity calculations are carried out without a consideration of the decay chain effect. In this case, sensitivities of reactor stable periods to not independent but cumulative fission yields are calculated. In the uranium-235 thermal fission case, a sensitivity to germanium-86 cumulative yield becomes very small and a sensitivity to arsenic-86 cumulative yield becomes large. These come from a fact that germanium-86 is not only

a delayed neutron precursor but also a parent nuclide of different precursor arsenic-86 as described above. Branching ratios to decay channel with delayed neutron emissions of germanium-86 and arsenic-86 are 0.06 and 0.33, respectively, and half-lives of germanium-86 and arsenic-86 are 87.8 ms and 0.945 s. Thus it can be said that germanium-86 is rather important as a parent nuclide of a delayed neutron precursor arsenic-86.

Here let us consider the reason why the decay chain effect on reactor stable periods in the uranium-235 thermal fission case is larger than that in the plutonium-239 thermal fission case. Parent fission product nuclides of delayed neutron precursors, whose fission yields affect reactor stable periods, are germanium-86, selenium-87, antimony-137 and tellurium-137. As shown in Tables 3 and 4, sensitivities to fission yields of these nuclides in the uranium-235 thermal fission case are clearly larger than those in the plutonium-239 thermal fission case. Among of them, selenium-87 and tellurium-137 seem more important since those nuclides have relatively long half-lives: 5.29 seconds for selenium-87 and 2.49 seconds for tellurium-137.

Finally, sensitivities of reactor stable periods to decay constants are shown from **Tables 7 to 10**. As a reactor stable period becomes shorter, sensitivities to decay constants of fission product nuclides having short half-lives become larger.

3.5. Uncertainty quantifications

Variances of independent fission yields, decay constants and decay branching ratios of fission product nuclides have been evaluated and given in JENDL/FPY-2011 and JENDL/FPD-2011. Using these variances and sensitivities calculated above, uncertainty of the reactor stable period can be quantified. Although there should be strong correla-

tions among independent fission yields and among the fission yield and branching ratio of fission product nuclides having the same mass number, such correlations are ignored in the present study since the main purpose of the present study is to identify the important delayed neutron-related nuclear data for the reactor kinetics. Calculated uncertainties of reactor stable period are summarized in **Table 11**. In all the cases, dominant sources of uncertainties are fission yields and contributions of decay constant uncertainties are negligible. Total uncertainties of the plutonium-239 fast fission case are the largest and the those of the uranium-235 thermal case are the smallest. Notice again that these results are obtained without considering the correlations among fundamental delayed neutron data.

Figures 7 to 10 show nuclide-wise and nuclear data-wise uncertainties and **Table 12** summarizes independent fission yields with their relative uncertainties of important fission product nuclides. In the uranium-235 thermal fission case, the fission yield uncertainty of germanium-86 is a dominant contributor. This can be understood from a large sensitivity and a large uncertainty to/of independent fission yield of germanium-86 as shown in Tables 3 and 12. The fission yield of iodine-137, which has a large sensitivity, does not contribute to total uncertainty as much as the germanium-86 since its uncertainty is very small in comparison with that of germanium-86. In the plutonium-239 thermal fission case, the fission yield uncertainties of selenium-87, yttrium-98m and iodine-137 are dominant contributors. The branching ratio uncertainty of yttrium-98m is also a dominant contributor in this case. In the plutonium-239 fast fission case, the fission yield uncertainty of iodine-137 is about twice as those in the thermal fission case. This comes from a difference in uncertainties of iodine-137 independent fission yield as shown in Table 12. Contributions of bromine-88, rubidium-94 and -95 independent fission yield uncertainties are also large because of the large values of independent yield uncertainties. In the

uranium-238 fast fission case, the fission yield uncertainties of bromine-91, tellurium-137 and iodine-137, some of which do not contribute to the uncertainty at all in other cases, are dominant contributors.

4. Conclusion

In order to better predict kinetic behavior of a nuclear fission reactor, improvement of delayed neutron parameters is essential. Such improvement can be realized by efforts done in the nuclear physics field, and it is required to establish a path from the microscopic nuclear data to the macroscopic delayed neutron parameters. The present paper has identified important nuclear data for reactor kinetics with a help of the adjoint kinetics equation and it has been found that they are dependent on an inserted reactivity (or a reactor stable period). Furthermore, nuclide-wise and nuclear data-wise uncertainties of the reactor stable period have been quantified using the variance data given in the nuclear data file, and the nuclear data which require further improvement have been identified.

The authors believe that the results obtained through the present study are helpful for the nuclear data community to improve delayed neutron-related nuclear data. We hope that more accurate and reliable delayed neutron data will be realized by joint contributions of the microscopic and macroscopic approaches in future.

Acknowledgment

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Table 1 Ancestor contributions dependent on reactor stable period

	k_p	Period	Br-87	Br-88	Br-89	Br-90	Rb-94	I-137	I-138
		[s]	(55.7*)	(16.3)	(4.40)	(1.92)	(2.70)	(24.5)	(6.23)
	0.99400	99.8	0.106	0.145	0.069	0.031	0.052	0.343	0.051
U-235 thermal	0.99500	19.5	0.029	0.109	0.108	0.061	0.094	0.191	0.070
	0.99600	6.9	0.009	0.058	0.112	0.088	0.120	0.085	0.061
	0.99806	102.9	0.069	0.080	0.042	0.022	0.043	0.522	0.084
Pu-239 thermal	0.99848	20.1	0.022	0.068	0.072	0.047	0.085	0.327	0.125
	0.99885	7.3	0.009	0.042	0.084	0.076	0.122	0.171	0.124
	0.99798	97.5	0.089	0.096	0.045	0.014	0.045	0.476	0.077
Pu-239 fast	0.99841	20.4	0.029	0.082	0.077	0.029	0.088	0.305	0.115
	0.99882	7.1	0.011	0.049	0.090	0.047	0.128	0.153	0.113
	0.98548	100.7	0.046	0.073	0.073	0.047	0.060	0.341	0.075
U-238 fast	0.98742	20.1	0.011	0.047	0.099	0.079	0.095	0.163	0.087
	0.98969	7.0	0.003	0.022	0.093	0.105	0.110	0.064	0.068

* Half-life in seconds.

Table 2 Fundamental data related to delayed neutron emission

	y_i^*	D_i^{**}	Half-life [s]
Ge-86	0.0063	0.41	0.088 (0.29 ^{***})
Se-87	0.0073	0.03	5.3 (80.6)
Br-87	0.0127	0.03	55.7
Br-88	0.0139	0.07	16.3
Br-89	0.0104	0.14	4.4
Br-90	0.0055	0.25	1.9
Rb-94	0.0156	0.11	2.7
I-137	0.0262	0.07	24.5
I-139	0.0077	0.10	2.28

* Independent fission yield of uranium-235 thermal fission.

** A total number of emitted neutrons per a nuclide generation.

*** Effective half-life.

Table 3 Sensitivities of reactor stable period to fission yield of uranium-235 thermal fission

	Reactor stable period [s]		
	99.8	19.5	6.9
Ge-86	-0.134	-0.165	-0.169
As-85	-0.029	-0.029	-0.019
Se-87	0.064	0.047	0.053
Br-87	0.101	0.074	0.053
Br-88	0.084	0.112	0.106
Br-89	-0.022	0.007	0.040
Br-90	-0.059	-0.059	-0.042
Br-91	-0.026	-0.034	-0.038
Rb-94	-0.055	-0.042	-0.013
Rb-95	-0.040	-0.053	-0.063
Rb-96	-0.014	-0.019	-0.023
Y-98m	-0.026	-0.026	-0.018
Sb-137	-0.018	-0.026	-0.034
Te-136	0.018	0.023	0.021
Te-137	0.042	0.046	0.040
I-137	0.282	0.302	0.254
I-139	-0.030	-0.027	0.043

Table 4 Sensitivities of reactor stable period to fission yield of plutonium-239 thermal fission

	Reactor stable period [s]		
	102.9	19.5	6.9
Se-87	0.021	0.016	0.012
Br-87	0.077	0.060	0.045
Br-88	0.041	0.061	0.064
Br-89	-0.033	-0.022	-0.000
Br-90	-0.065	-0.078	-0.072
Rb-94	-0.077	-0.082	-0.061
Rb-95	-0.058	-0.084	-0.107
Y-98m	-0.082	-0.097	-0.088
Y-99	-0.036	-0.045	-0.047
Sb-135	-0.018	-0.023	-0.022
Te-137	0.021	0.025	0.022
I-137	0.399	0.461	0.415
I-139	-0.037	-0.042	-0.036

Table 5 Sensitivities of reactor stable period to fission yield of plutonium-239 fast fission

	Reactor stable period [s]		
	97.5	20.4	7.1
As-85	-0.034	-0.040	-0.037
Se-87	0.031	0.024	0.018
Br-87	0.096	0.075	0.057
Br-88	0.047	0.070	0.074
Br-89	-0.036	-0.025	-0.002
Br-90	-0.041	-0.048	-0.046
Rb-94	-0.082	-0.088	-0.067
Rb-95	-0.045	-0.064	-0.082
Rb-96	-0.015	-0.021	-0.028
Y-98m	-0.085	-0.100	-0.093
Y-99	-0.036	-0.046	-0.048
Y-100m	-0.018	-0.024	-0.028
Sb-135	-0.017	-0.021	-0.021
Te-136	0.015	0.021	0.021
Te-137	0.021	0.024	0.022
I-137	0.362	0.419	0.380
I-138	-0.025	0.004	0.037
I-139	-0.026	-0.030	-0.026

Table 6 Sensitivities of reactor stable period to fission yield of uranium-238 fast fission

	Reactor stable period [s]		
	100.7	20.1	7.0
As-85	-0.033	-0.027	-0.012
Se-87	0.046	0.030	0.020
Se-88	0.025	0.028	0.024
Br-87	0.032	0.021	0.014
Br-88	0.038	0.043	0.037
Br-89	0.015	0.025	0.045
Br-90	-0.051	-0.044	-0.024
Br-91	-0.037	-0.046	-0.050
Br-92	-0.020	-0.012	-0.029
Rb-94	-0.027	-0.012	0.009
Rb-95	-0.036	-0.045	-0.051
Rb-96	-0.042	-0.054	-0.065
Sb-135	-0.038	-0.036	-0.024
Te-136	0.033	0.035	0.029
Te-137	0.116	0.109	0.086
I-137	0.250	0.233	0.178
I-138	0.020	0.044	0.056
I-139	-0.027	-0.019	-0.004
I-140	-0.018	-0.021	-0.021
Cs-145	-0.020	-0.024	-0.026

Table 7 Sensitivities of reactor stable period to decay constant in uranium-235 thermal fission

	Reactor stable period [s]		
	99.8	19.5	6.9
As-85 (2.03*)	-0.022	-0.042	-0.060
As-86 (0.95)	-0.022	-0.048	-0.082
Br-87 (55.7)	-0.107	-0.030	-0.009
Br-88 (16.3)	-0.145	-0.109	-0.057
Br-89 (4.40)	-0.069	-0.108	-0.112
Br-90 (1.92)	-0.031	-0.061	-0.087
Rb-93 (5.84)	-0.028	-0.040	-0.036
Rb-94 (2.70)	-0.052	-0.094	-0.120
Y-98m (2.0)	-0.014	-0.028	-0.040
Y-99 (1.48)	-0.007	-0.014	-0.021
Te-136 (17.6)	-0.024	-0.017	-0.009
I-137 (24.5)	-0.343	-0.191	-0.085
I-138 (6.23)	-0.051	-0.070	-0.061
I-139 (2.28)	-0.020	-0.039	-0.053

* Half-life in second.

Table 8 Sensitivities of reactor stable period to decay constant in plutonium-239 thermal fission

	Reactor stable period [s]		
	102.9	19.5	6.9
Br-87 (55.7)	-0.070	-0.022	-0.009
Br-88 (16.3)	-0.080	-0.068	-0.042
Br-89 (4.40)	-0.042	-0.072	-0.084
Br-90 (1.92)	-0.022	-0.047	-0.076
Rb-93 (5.84)	-0.022	-0.034	-0.034
Rb-94 (2.70)	-0.043	-0.086	-0.122
Y-98m (2.0)	-0.029	-0.062	-0.098
Y-99 (1.48)	-0.009	-0.020	-0.035
I-137 (24.5)	-0.522	-0.327	-0.164
I-138 (6.23)	-0.084	-0.125	-0.123
I-139 (2.28)	-0.016	-0.033	-0.050

Table 9 Sensitivities of reactor stable period to decay constant in plutonium-239 fast fission

	Reactor stable period [s]		
	97.5	20.4	7.1
As-85 (2.03)	-0.012	-0.026	-0.041
Br-87 (55.7)	-0.042	-0.029	-0.011
Br-88 (16.3)	-0.102	-0.082	-0.049
Br-89 (4.40)	-0.046	-0.077	-0.091
Br-90 (1.92)	-0.014	-0.029	-0.047
Rb-93 (5.84)	-0.029	-0.042	-0.043
Rb-94 (2.70)	-0.046	-0.088	-0.129
Y-98m (2.0)	-0.030	-0.062	-0.101
Y-99 (1.48)	-0.009	-0.020	-0.035
Te-136 (17.6)	-0.026	-0.020	-0.012
I-137 (24.5)	-0.505	-0.305	-0.155
I-138 (6.23)	-0.079	-0.115	-0.114
I-139 (2.28)	-0.011	-0.022	-0.035

Table 10 Sensitivities of reactor stable period to decay constant in uranium-238 fast fission

	Reactor stable period [s]		
	100.7	20.1	7.0
As-85 (2.03)	-0.032	-0.054	-0.070
Br-87 (55.7)	-0.056	-0.011	-0.003
Br-88 (16.3)	-0.072	-0.047	-0.022
Br-89 (4.40)	-0.073	-0.099	-0.093
Br-90 (1.92)	-0.046	-0.079	-0.105
Rb-93 (5.84)	-0.019	-0.023	-0.018
Rb-94 (2.70)	-0.060	-0.095	-0.110
Y-98m (2.0)	-0.012	-0.020	-0.026
Y-99 (1.48)	-0.008	-0.016	-0.023
Te-136 (17.6)	-0.038	-0.025	-0.012
Te-137 (2.49)	-0.021	-0.023	-0.021
I-137 (24.5)	-0.336	-0.164	-0.064
I-138 (6.23)	-0.074	-0.087	-0.068
I-139 (2.28)	-0.033	-0.055	-0.069

Table 11 reactor stable period uncertainties

	Period		Relative uncertainty [%]		
	[s]	Total	Decay constant	Fission yield	Branching ratio
U-235 thermal	99.8	4.4	0.3	3.7	2.4
	19.5	5.0	0.4	4.4	2.5
	6.9	5.0	0.5	4.5	2.1
Pu-239 thermal	102.9	6.0	0.5	5.1	3.0
	19.5	7.1	0.7	6.1	3.5
	6.9	6.9	1.0	6.0	3.2
Pu-239 fast	97.5	11.7	0.5	11.2	3.3
	20.4	13.6	0.7	13.0	3.8
	7.1	13.0	1.0	12.5	3.6
U-238 fast	100.7	8.6	0.4	8.3	2.1
	20.1	8.8	0.4	8.5	1.9
	7.0	8.1	0.5	7.9	1.5

Table 12 Independent fission yields and their uncertainties given in JENDL/FPY-2011

	U-235 thermal	Pu-239 thermal	Pu-239 fast	U-238 fast
Ge-86	0.00628 (16*)	<0.00001 (64)	<0.00001 (64)	0.00006 (64)
Se-87	0.00730 (4)	0.00137 (64)	0.00180 (64)	0.00849 (32)
Br-88	0.01386 (2)	0.00465 (4)	0.00486 (64)	0.00901 (45)
Br-91	0.00223 (11)	0.00020 (64)	0.00033 (64)	0.00760 (64)
Rb-94	0.01564 (2.8)	0.00704 (16)	0.00648 (64)	0.02540 (32)
Rb-95	0.00763 (4)	0.00432 (23)	0.00289 (64)	0.01598 (32)
Rb-96	0.00038 (8)	0.00039 (64)	0.00060 (64)	0.01171 (32)
Y-98m	0.01874 (32)	0.02013 (32)	0.01808 (32)	0.02622 (32)
Sb-137	0.00074 (64)	0.00000 (64)	0.00000 (64)	0.00038 (64)
Te-137	0.00392 (8)	0.00129 (64)	0.00115 (64)	0.01570 (32)
I-137	0.02619 (4)	0.02299 (6)	0.01888 (16)	0.03537 (16)

* Uncertainty in percent.

Figure captions

Figure 1. Relation between prompt neutron multiplication factor and reactor stable period for thermal fission

Figure 2. Decay chain effect on reactor stable period corresponding prompt neutron multiplication factor for thermal fission. The Decay chain effect is defined as a relative difference between two reactor stable periods; one is calculated with the decay chain effect consideration and the other is calculated without its consideration.

Figure 3. Relative contributions of fission product nuclides as ancestors of neutrons at $t = 0$ in uranium-235 thermal fission ($T = 100[\text{sec}]$)

Figure 4. Relative contributions of fission product nuclides as ancestors of neutrons at $t = 0$ in uranium-235 thermal fission ($T = 20[\text{sec}]$)

Figure 5. Relative contributions of fission product nuclides as ancestors of neutrons at $t = 0$ in uranium-235 thermal fission ($T = 7[\text{sec}]$)

Figure 6. Constrained and unconstrained sensitivities of reactor stable period to fission yield for uranium-235 thermal fission ($T=100[\text{sec}]$)

Figure 7. Nuclide-wise and Nuclear data-wise uncertainties of reactor stable period in the uranium-235 thermal fission case

Figure 8. Nuclide-wise and Nuclear data-wise uncertainties of reactor stable

period in the plutonium-239 thermal fission case

Figure 9. Nuclide-wise and Nuclear data-wise uncertainties of reactor stable period in the plutonium-239 fast fission case

Figure 10. Nuclide-wise and Nuclear data-wise uncertainties of reactor stable period in the uranium-238 fast fission case

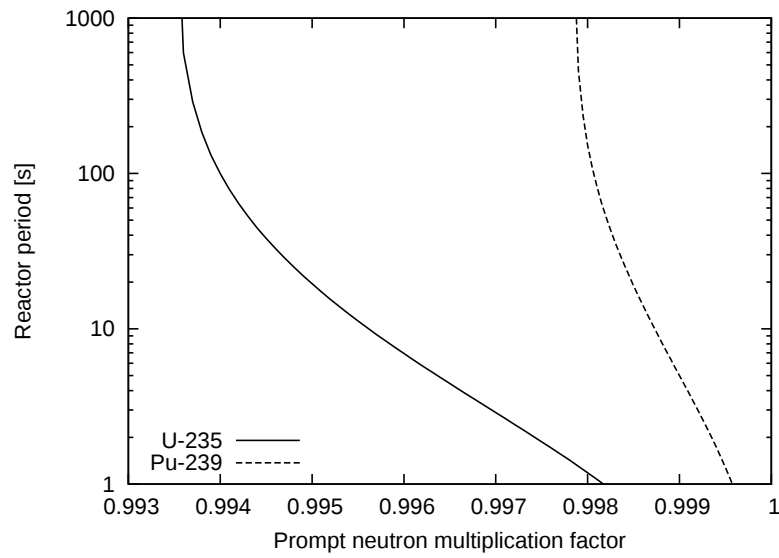


Figure 1 Relation between prompt neutron multiplication factor and reactor stable period for thermal fission

G.Chiba:

Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

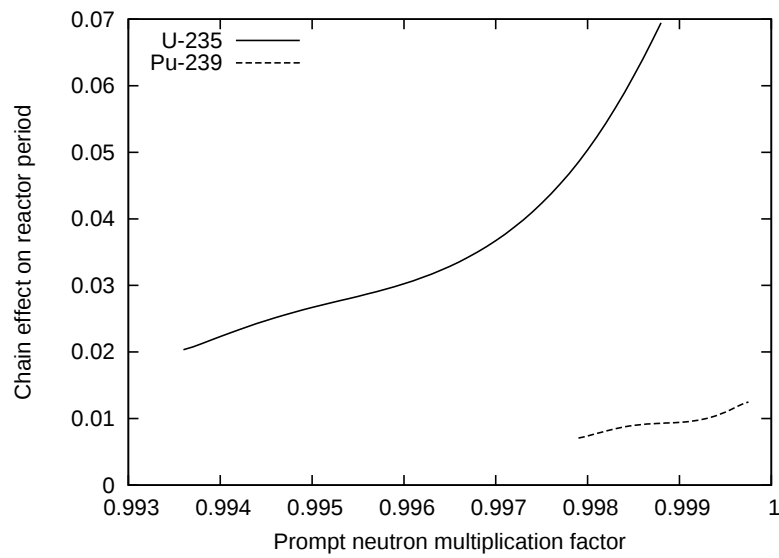


Figure 2 Decay chain effect on reactor stable period corresponding prompt neutron multiplication factor for thermal fission. The Decay chain effect is defined as a relative difference between two reactor stable periods; one is calculated with the decay chain effect consideration and the other is calculated without its consideration.

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Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

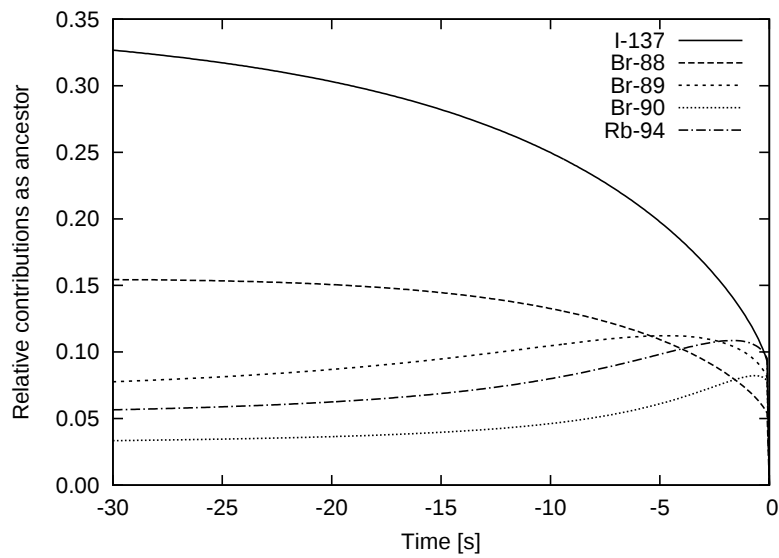


Figure 3 Relative contributions of fission product nuclides as ancestors of neutrons at $t = 0$ in uranium-235 thermal fission ($T = 100[\text{sec}]$)

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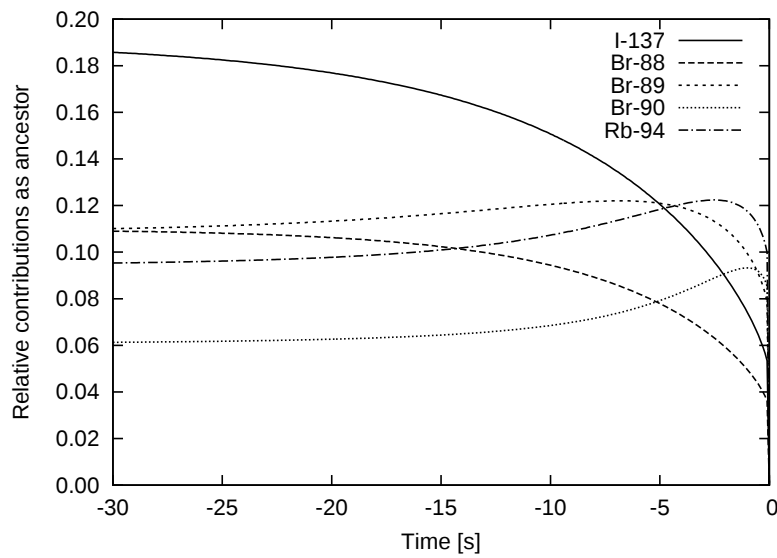


Figure 4 Relative contributions of fission product nuclides as ancestors of neutrons at $t = 0$ in uranium-235 thermal fission ($T = 20[\text{sec}]$)

G.Chiba:

Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

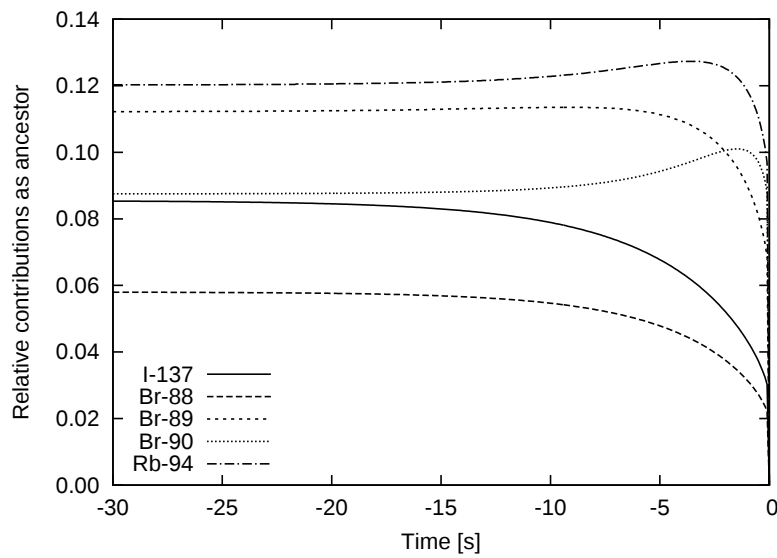


Figure 5 Relative contributions of fission product nuclides as ancestors of neutrons at $t = 0$ in uranium-235 thermal fission ($T = 7[\text{sec}]$)

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Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

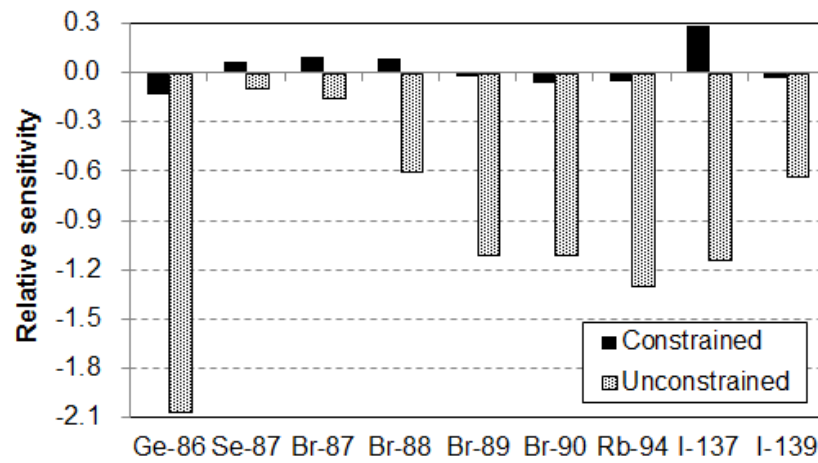


Figure 6 Constrained and unconstrained sensitivities of reactor stable period to fission yield for uranium-235 thermal fission ($T=100[\text{sec}]$)

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Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

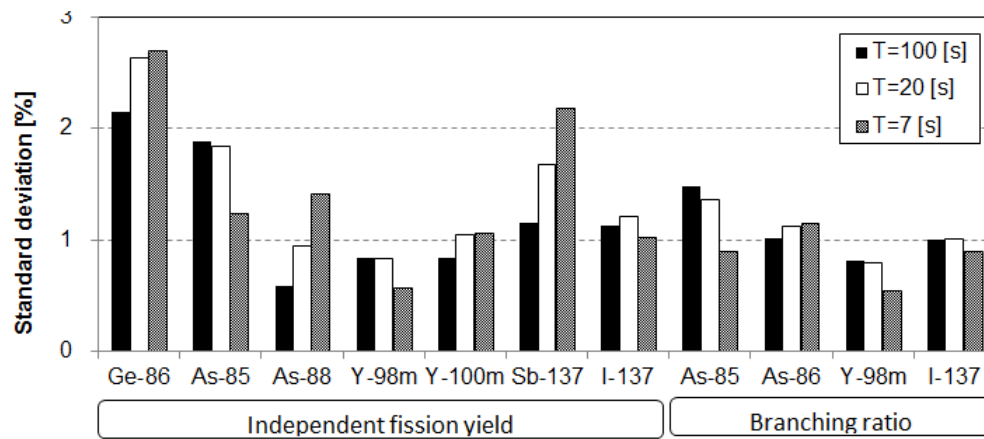


Figure 7 Nuclide-wise and Nuclear data-wise uncertainties of reactor stable period in the uranium-235

thermal fission case

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Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity
using one-point adjoint kinetics equation

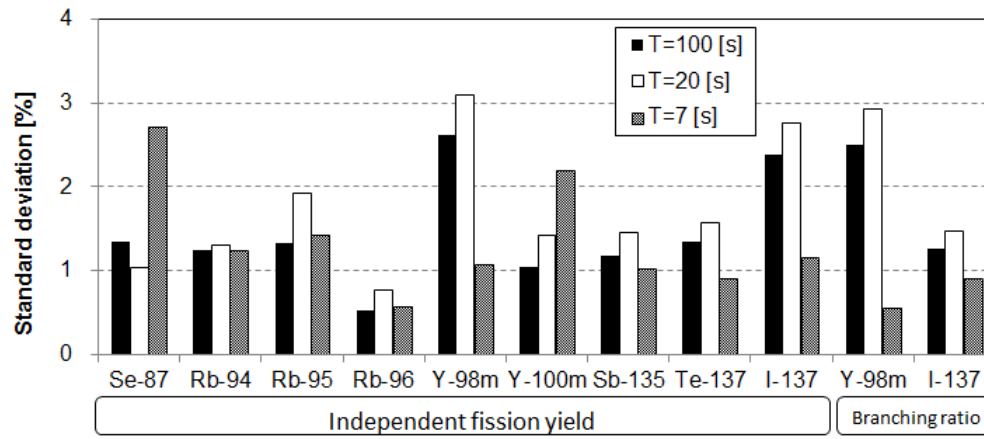


Figure 8 Nuclide-wise and Nuclear data-wise uncertainties of reactor stable period in the plutonium-239

thermal fission case

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Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

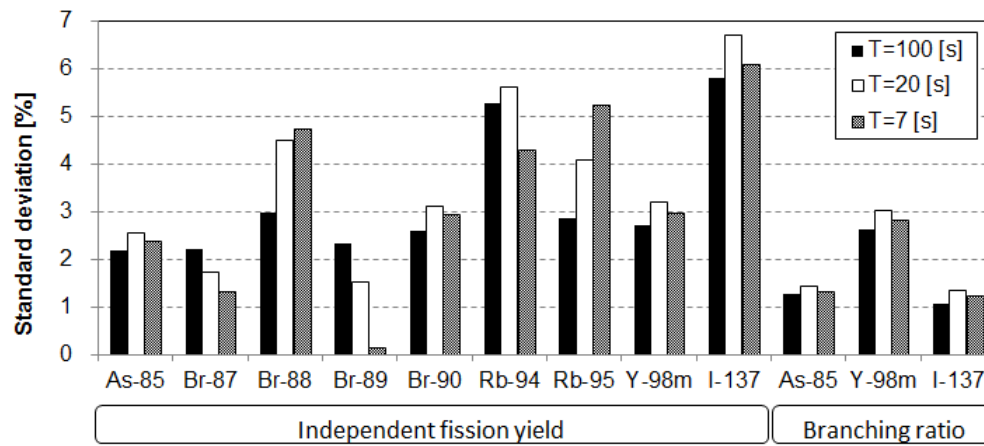


Figure 9 Nuclide-wise and Nuclear data-wise uncertainties of reactor stable period in the plutonium-239

fast fission case

G.Chiba:

Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity using one-point adjoint kinetics equation

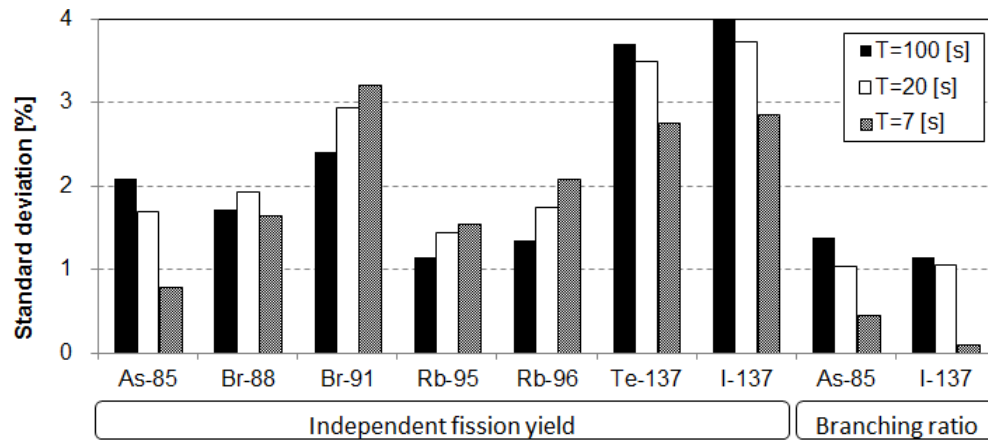


Figure 10 Nuclide-wise and Nuclear data-wise uncertainties of reactor stable period in the uranium-238

fast fission case

G.Chiba:

Sensitivity and uncertainty analysis for reactor stable period induced by positive reactivity
using one-point adjoint kinetics equation