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Finite-Element Solution of Horizontally Polarized Shear Wave Scattering in an Elastic Plate

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Abstract—A method of the solution of scattering of horizontally polarized shear waves in an elastic plate is described. The approach is a combination of the finite-element method and the analytical method. In this approach, both the propagating and evanescent higher order modes are taken into account, and the restriction in the previous work that the number of assumed waveguide modes be equal to the number of boundary finite-element nodal points is removed. This approach is applicable to the frequency range in which the plate waveguide propagates multimodes. Numerical examples on the scattering by a step discontinuity, a wedge-shaped crack, and a metal strip are given.

I. INTRODUCTION

SCATTERING of guided waves by discontinuities in an elastic plate is a basic problem in nondestructive evaluation and also has important implications with regard to electrical signal-processing functions, and the scattering of horizontally polarized shear (SH) waves has been investigated extensively [1]–[5]. Recently, the numerical methods based on the finite-element method (FEM) have been developed for the analysis of the scattering of SH waves by arbitrarily shaped discontinuities in an elastic plate. Sabbagh *et al.* [6] have analyzed the scattering of SH waves by a step discontinuity joining two plates using a combined method of the FEM and circuit theory. In their approach it is assumed that the plate waveguide propagates a single mode only, and all the higher order modes in the waveguide are neglected. Abduljabbar *et al.* [7] have analyzed the scattering of SH waves by an infinitely thin crack normal to the surface of a plate using a combined method of the FEM and analytical technique. In their approach the higher-order modes are taken into account, but the stresses along the boundary separating the interior finite-element region from the exterior regular region, in which the scattered field is expanded in a superposition of a finite number of normal modes, are assumed to be piecewise uniform. This combined method requires that the number of the nodal points along the interface boundary between the interior and the exterior regions should be equal to that of the normal modes in the waveguide. Koshiba *et al.* [8] have analyzed the scattering of Lamb waves in an elastic plate using the combined finite-element and analytical technique. In [8]

only the fundamental Lamb wave is taken into account, and all the higher order modes in the waveguide are neglected. Edmunds *et al.* [9] have used the least-squares collocation approach to solve fracture mechanics problems, removing the restriction that the number of terms in a stress function expansion (analogous to the number of waveguide modes in the present problem) be equal to the number of boundary collocation points.

In this paper, an improved formulation of the combined finite-element and analytical technique is described for the analysis of the scattering of SH waves by arbitrarily shaped discontinuities in an elastic plate. In this approach both the propagating and the evanescent higher order modes are taken into account and the stresses along the interface boundary separating the interior finite-element region from the exterior region are discretized by utilizing the shape functions [7], [8], [10]–[14] which are used for a standard procedure in the FEM. Also, the number of the nodal points along the interface boundary and that of the normal modes are independent of each other and the nodal points can be arbitrarily spaced along the interface boundary. This approach is applicable to the frequency range in which the plate waveguide propagates multimodes. To show the validity and usefulness of this formulation, computed results are given for a step discontinuity, a wedge-shaped crack, and a metal strip. Accuracy of the solution is investigated in detail.

II. BASIC EQUATIONS

We consider the plate waveguide junction as shown in Fig. 1, where the boundaries Γ_1 and Γ_2 connect the discontinuity region to the plate waveguides 1 and 2, respectively, the boundaries Γ_3 and Γ_4 are the stress-free surface, and the region Ω with the boundaries Γ_1 to Γ_4 completely encloses the discontinuities.

Assuming that there is no variation in the z -direction, we have the following basic equations for SH waves [1]:

$$\partial T_{zx}/\partial x + \partial T_{zy}/\partial y - j\omega\rho v_z = 0 \quad (1)$$

and

$$j\omega T_{zx} = \mu \partial v_z/\partial x \quad (2a)$$

$$j\omega T_{zy} = \mu \partial v_z/\partial y \quad (2b)$$

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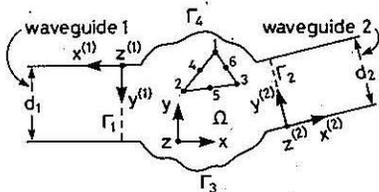


Fig. 1. Discontinuity in elastic plate.

where v_z is the z component of the particle velocity, T_{zx} and T_{zy} are the stresses, ω is the angular frequency, ρ is the mass density, and μ is the Lamé constant.

III. MATHEMATICAL FORMULATION

A. Finite-Element Approach

Dividing the region Ω into a number of second-order triangular elements with six nodal points as shown in Fig. 1, the particle velocity v_z within each element may be written as

$$v_z = \{N\}^T \{v_z\}_e \quad (3)$$

where $\{v_z\}_e$ is the particle velocity vector corresponding to the nodal points within each element, $\{N\}$ is the shape function vector [7], [8], [10]–[14], and $T, \{\cdot\}$, and $\{\cdot\}^T$ denote a transpose, a column vector, and a row vector, respectively. The advantage of an arbitrary triangular shape in approximating to any boundary shape has been demonstrated in [10]. Also, the usefulness of the second-order triangular element has been discussed in [12] and [13].

Using a Galerkin procedure on (1) and integrating by parts, we obtain

$$\iint_{\Omega_e} [(\partial\{N\}/\partial x)T_{zx} + (\partial\{N\}/\partial y)T_{zy} + j\omega\rho_e\{N\}v_z] dx dy - \int_{\Gamma_e} \{N\}T_{zn} d\Gamma = \{0\} \quad (4)$$

where the first and second integrations on the left side are carried over the element subdomain Ω_e and the contour Γ_e of Ω_e , respectively, $\{0\}$ is a null vector, and

$$T_{zn} = T_{zx}n_x + T_{zy}n_y \quad (5)$$

Here n_x and n_y are the x and y components of an outward normal unit vector to Γ_e , respectively.

Noting that T_{zn} is continuous across Γ_e and $T_{zn} = 0$ on Γ_3 and Γ_4 , from (2) to (4) the following global matrix equation is derived

$$[A]\{v_z\} = \sum_{i=1}^2 \sum_e' j\omega \int_{\Gamma_e} \{N\}_i T_{zx,i}(x^{(i)} = 0, y^{(i)}) dy^{(i)} \quad (6)$$

where

$$[A] = \sum_e \iint_{\Omega_e} [\mu_e (\partial\{N\}/\partial x) (\partial\{N\}^T/\partial x) + \mu_e (\partial\{N\}/\partial y) (\partial\{N\}^T/\partial y) - \omega^2 \rho_e \{N\} \{N\}^T] dx dy \quad (7)$$

Here $\{v_z\}$ is the nodal particle velocity vector, Σ_e and Σ_e' extend over all different elements and the elements related to Γ_i ($i = 1, 2$), respectively, $T_{zx,i}(x^{(i)} = 0, y^{(i)})$ is the stress on Γ_i , and $\{N\}_i$ is the shape function vector on Γ_i , namely $\{N\}_i = \{N(x^{(i)} = 0, y^{(i)})\}$.

Using the shape function vector $\{N\}_i$, the particle velocity $v_{z,i}$ and the stress $T_{zx,i}$ on Γ_i may be discretized as follows:

$$v_{z,i}(x^{(i)} = 0, y^{(i)}) = \{N\}_i^T \{v_z\}_{i,e} \quad (8)$$

$$T_{zx,i}(x^{(i)} = 0, y^{(i)}) = \{N\}_i^T \{T_{zx}\}_{i,e} \quad (9)$$

where $\{v_z\}_{i,e}$ and $\{T_{zx}\}_{i,e}$ are the particle velocity vector and the stress vector corresponding to the nodal points within each element related to Γ_i , respectively.

Substituting (8) and (9) into (6), we obtain

$$[A] \begin{bmatrix} \{v_z\}_I \\ \{v_z\}_B \end{bmatrix} = \begin{bmatrix} \{0\} \\ [B]\{T_{zx}\}_B \end{bmatrix} \quad (10)$$

where

$$\{v_z\}_B = \begin{bmatrix} \{v_z\}_1 \\ \{v_z\}_2 \end{bmatrix} \quad (11)$$

$$\{T_{zx}\}_B = \begin{bmatrix} \{T_{zx}\}_1 \\ \{T_{zx}\}_2 \end{bmatrix} \quad (12)$$

$$[B] = \begin{bmatrix} [B]_1 & [0] \\ [0] & [B]_2 \end{bmatrix} \quad (13)$$

and

$$[B]_i = j\omega \sum_e' \int_{\Gamma_e} \{N\}_i \{N\}_i^T dy^{(i)}, \quad i = 1, 2. \quad (14)$$

Here the components of the $\{v_z\}_I$ vector are the values of v_z at the nodal points in Ω except Γ_1 and Γ_2 , the components of the $\{v_z\}_i$ and $\{T_{zx}\}_i$ vectors are the values of v_z and T_{zx} at the nodal points on Γ_i , respectively, and $[0]$ is a zero matrix.

B. Analytical Approach

The internal fields in the waveguide i ($i = 1, 2$) in Fig. 1 are represented by the sum of the normal modes as [1], [2], [15]

$$v_{z,i}(x^{(i)}, y^{(i)}) = \sum_n [a_{in} \exp(-j\beta_{in}x^{(i)}) + b_{in} \exp(j\beta_{in}x^{(i)})] f_{in}(y^{(i)}) \quad (15a)$$

$$-T_{zx,i}(x^{(i)}, y^{(i)}) = \sum_n Y_{in} [a_{in} \exp(-j\beta_{in}x^{(i)}) - b_{in} \exp(j\beta_{in}x^{(i)})] g_{in}(y^{(i)}) \quad (15b)$$

where

$$\beta_{in} = \sqrt{k_{si}^2 - (n\pi/d_i)^2} \quad (16)$$

$$Y_{in} = \mu_i \beta_{in} / \omega \quad (17)$$

$$f_{in}(y^{(i)}) = g_{in}(y^{(i)}) = \sqrt{l_n/d_i} \cos(n\pi y^{(i)}/d_i) \quad (18)$$

$$k_{si} = \omega \sqrt{\rho_i/\mu_i} \quad (19)$$

and

$$l_i = \begin{cases} 1, & n = 0 \\ 2, & n \neq 0. \end{cases} \quad (20)$$

Here a_{in} and b_{in} are the amplitudes of the n th mode ($n = 0, 1, 2, \dots$) in the waveguide i propagating (or decaying) toward the $+x^{(i)}$ and $-x^{(i)}$ directions, respectively.

Now, assuming that the m th mode ($m = 0, 1, 2, \dots$) of unit amplitude is incident from the left of waveguide 1 in Fig. 1, the amplitudes of normal modes may be written as

$$b_{1n} = \begin{cases} 1, & n = m \\ 0, & n \neq m \end{cases} \quad (21a)$$

$$b_{2n} = 0. \quad (21b)$$

Considering (15) and (20), $v_{z,i}$ and $T_{zx,i}$ on Γ_i may be expressed as

$$\begin{aligned} v_{z,i}(x^{(i)} = 0, y^{(i)}) &= \delta_{i1} 2 f_{1m}(y^{(1)}) \\ &+ \int_0^{d_i} \sum_n (1/Y_{in}) f_{in}(y^{(i)}) f_{in}(y_0^{(i)}) \\ &\cdot [-T_{zx,i}(x^{(i)} = 0, y_0^{(i)})] dy_0^{(i)} \end{aligned} \quad (22)$$

$$\begin{aligned} -T_{zx,i}(x^{(i)} = 0, y^{(i)}) &= -\delta_{i1} 2 Y_{1m} g_{1m}(y^{(1)}) \\ &+ \int_0^{d_i} \sum_n Y_{in} g_{in}(y^{(i)}) g_{in}(y_0^{(i)}) \\ &\cdot v_{z,i}(x^{(i)} = 0, y_0^{(i)}) dy_0^{(i)} \end{aligned} \quad (23)$$

where δ_{i1} is the Kronecker δ .

Using (8) and (9), (22) and (23) can be discretized as follows:

$$\{v_z\}_i = \delta_{i1} \{f\}_1 - [F]_i \{T_{zx}\}_i \quad (24)$$

$$-\{T_{zx}\}_i = \delta_{i1} \{g\}_1 + [G]_i \{v_z\}_i \quad (25)$$

where

$$\{f\}_1 = 2 \{f_m\}_1 \quad (26)$$

$$\{g\}_1 = -2 Y_{1m} \{g_m\}_1 \quad (27)$$

$$[F]_i = \sum_n (1/Y_{in}) \{f_n\}_i \sum_e' \int_e f_{in}(y_0^{(i)}) \cdot \{N(x^{(i)} = 0, y_0^{(i)})\}^T dy_0^{(i)} \quad (28)$$

and

$$[G]_i = \sum_n Y_{in} \{g_n\}_i \sum_e' \int_e g_{in}(y_0^{(i)}) \cdot \{N(x^{(i)} = 0, y_0^{(i)})\}^T dy_0^{(i)}. \quad (29)$$

Here the components of the $\{f_n\}_i$ and $\{g_n\}_i$ vectors are the values of $f_{in}(y^{(i)})$ and $g_{in}(y^{(i)})$ at the nodal points on Γ_i , respectively.

C. Combination of Finite-Element and Analytical Relations

Using (11) and (12), from (10) and (24) we obtain the following final matrix equation:

$$\begin{bmatrix} [A] & [0] \\ & [B] \\ [0] & [1] \end{bmatrix} \begin{bmatrix} \{v_z\}_I \\ \{v_z\}_B \\ -\{T_{zx}\}_B \end{bmatrix} = \begin{bmatrix} \{0\} \\ \{0\} \\ \{f\} \end{bmatrix}. \quad (30)$$

Similarly, from (10) and (25) we obtain the following final matrix equation:

$$\begin{bmatrix} [A] & [0] \\ & [B] \\ [0] & -[G] \end{bmatrix} \begin{bmatrix} \{v_z\}_I \\ \{v_z\}_B \\ -\{T_{zx}\}_B \end{bmatrix} = \begin{bmatrix} \{0\} \\ \{0\} \\ \{g\} \end{bmatrix} \quad (31)$$

where

$$\{f\} = \begin{bmatrix} \{f\}_1 \\ \{0\} \end{bmatrix} \quad (32)$$

$$\{g\} = \begin{bmatrix} \{g\}_1 \\ \{0\} \end{bmatrix} \quad (33)$$

$$[F] = \begin{bmatrix} [F]_1 & [0] \\ [0] & [F]_2 \end{bmatrix} \quad (34)$$

$$[G] = \begin{bmatrix} [G]_1 & [0] \\ [0] & [G]_2 \end{bmatrix} \quad (35)$$

and [1] is a unit matrix.

The values of v_z at the nodal points on Γ_i ($i = 1, 2$), namely $\{v_z\}_i$ are computed from (30) or (31), and then by using (8), $v_{z,i}$ on Γ_i is calculated from these values. The solutions $v_{z,i}$ allow the determination of the reflection coefficient R_{mn} and the transmission coefficient T_{mn} of the n th propagating mode for the m th incident mode as fol-

lows:

$$R_{mn} \equiv a_{1n} = \sqrt{Y_{1n}/Y_{1m}} \left[-\delta_{mn} + \int_0^{d_1} g_{1n}(y^{(1)}) v_{z,1}(x^{(1)}) = 0, y^{(1)}) dy^{(1)} \right] \quad (36)$$

$$T_{mn} \equiv a_{2n} = \sqrt{Y_{2n}/Y_{1m}} \int_0^{d_2} g_{2n}(y^{(2)}) v_{z,2}(x^{(2)}) = 0, y^{(2)}) dy^{(2)}. \quad (37)$$

The condition of power conservation may be written as

$$\sum_{n=0}^{n_1-1} |R_{mn}|^2 + \sum_{n=0}^{n_2-1} |T_{mn}|^2 = P_{\text{total}} = 1 \quad (38)$$

where n_i is the number of the propagating modes in the waveguide i .

IV. COMPUTED RESULTS

First, we consider the symmetric step joining two plates and subdivided one half of the discontinuity region into second-order triangular elements as shown in Fig. 2, where the zeroth mode is incident from the left of the plate with thickness d_1 , $d_1/d_2 = 1.7$, 96 (N_E) elements are used, and the number of the nodal points (N_p) is 233. Table I shows the numbers n_1 and n_2 of the propagating modes in the plates with thicknesses d_1 and d_2 , respectively. Table II shows the real and imaginary parts of the reflection coefficient R_{00} of the zeroth mode at the step, where the computed results are obtained by using (30). Table III shows the energy error ($1 - P_{\text{total}}$), where the computed results are obtained by using (30) and (31). N_{iM} ($i = 1, 2$) is the number of the normal modes in the waveguide i used in (28) and (29). Here we set $N_{1M} = N_{2M} \equiv N_M$. In these tables, the results of $N_E = 384$ ($N_p = 849$) and of $N_E = 846$ ($N_p = 1849$) are also presented. From Table II it is found that for smaller values of $k_s d_2$, both values of real and imaginary parts converge with $N_E = 96$ (see the values for $k_s d_2 = 1.0, 5.0$, and 10.0), but for larger values of $k_s d_2$, the values of imaginary part do not converge with $N_E = 96$ (see the values for $k_s d_2 = 20.0$ and 30.0). The convergence is obtained in the case of $N_E = 384$. From Table III it is found that the energy error can be reduced by increasing the number of elements. The larger the value of N_M becomes, the larger the energy error also becomes. This is due to the fact that when discretizing the normal modes with larger values of n in (28) and (29), more nodal points on Γ_i ($i = 1, 2$) in Fig. 2 are necessary. In practice, it is sufficient to consider the propagating modes and a few evanescent higher order modes in (28) and (29). The difference between the values calculated from (30) and the values calculated from (31) is relatively small, but, generally, the energy error in the analysis using (31) is larger than that in the analysis using (30). Therefore, we present below only the results ob-

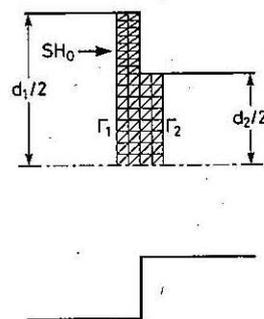


Fig. 2. Typical division of symmetric step.

TABLE I
NUMBERS OF PROPAGATING MODES IN THE
PLATES IN FIG. 2

$k_s d_2$	n_1	n_2
1.0	1	1
5.0	2	1
10.0	3	2
20.0	6	4
30.0	9	5

tained by using (30). It is generally difficult to determine *a priori* the discretization fineness required to achieve sufficient accuracy. The finite-element method with a suitable mesh refinement strategy [11], [14] may be useful for accurate analysis.

Next, we consider a surface crack in a plate. Results for an infinitely thin crack are given in graphical form by Abduljabbar *et al.* [7]. Our results agreed perfectly with the results in [7] to the accuracy that can be discerned on the graphs.

Fig. 3(a)-(c) show the magnitude of the reflection coefficient R_{mn} of a wedge-shaped crack as a function of the wedge apex angle $\tan \theta$ for the zeroth ($m = 0$), first ($m = 1$), and second ($m = 2$) incident modes, respectively, where $k_s d = 13.5$ and the reflection coefficient of the mode of order less than m can be computed from the relation $R_{mn} = R_{nm}$ [7]. The number of the nodal points along the interface boundary corresponding to the boundary Γ_i ($i = 1, 2$) in Fig. 1 is 41, and 10 normal modes in the waveguide i are considered in (28). The reflection coefficient is considerably influenced by the wedge apex angle. At an appropriate value of θ , the conversion coefficient for the fourth reflected mode becomes larger than the conversion coefficients for the other reflected modes.

Lastly, we consider a metal strip on one surface of a fused quartz plate and assume that the zeroth mode is incident [16]. Fig. 4 shows the magnitude of the reflection coefficient R_{00} of a metal strip as a function of the normalized strip thickness h/λ , where λ is the wavelength of the incident wave, $\lambda = 2\pi/k_s$, $d/\lambda = 0.25$, and the normalized strip width $a/\lambda = 0.25$. The reflectivity of this SH wave is considerably large compared with the Rayleigh-wave reflection from a metal strip on a semi-infinite substrate [17].

TABLE II
REAL AND IMAGINARY PARTS OF REFLECTION COEFFICIENT R_{00} OF ZEROth MODE

N_E	$k_s d_2$	Real Part			Imaginary Part		
		$N_M = 15$	$N_M = 30$	$N_M = 50$	$N_M = 15$	$N_M = 30$	$N_M = 50$
96	1.0	0.261	0.261	0.261	0.040	0.040	0.040
	5.0	0.439	0.439	0.439	0.030	0.030	0.030
	10.0	0.399	0.400	0.400	0.020	0.020	0.020
	20.0	0.406	0.406	0.406	0.016	0.016	0.015
	30.0	0.414	0.415	0.415	0.020	0.020	0.020
384	1.0	0.261	0.261	0.261	0.040	0.040	0.040
	5.0	0.440	0.440	0.440	0.030	0.030	0.030
	10.0	0.400	0.400	0.400	0.020	0.020	0.020
	20.0	0.406	0.406	0.406	0.012	0.012	0.012
	30.0	0.414	0.414	0.414	0.010	0.010	0.010
864	20.0	0.407	0.407	0.407	0.012	0.012	0.012
	30.0	0.414	0.414	0.414	0.009	0.009	0.009

TABLE III
ENERGY ERROR IN THE ANALYSIS OF STEP DISCONTINUITY IN FIG. 2

N_E	$k_s d_2$	Equation (30)			Equation (31)		
		$N_M = 15$	$N_M = 30$	$N_M = 50$	$N_M = 15$	$N_M = 30$	$N_M = 50$
96	1.0	3.2×10^{-8}	6.0×10^{-7}	3.1×10^{-7}	-3.6×10^{-6}	-3.4×10^{-4}	-4.3×10^{-5}
	5.0	1.2×10^{-6}	1.0×10^{-5}	-4.3×10^{-6}	-2.3×10^{-6}	-3.0×10^{-4}	-1.1×10^{-4}
	10.0	7.4×10^{-7}	7.0×10^{-5}	9.8×10^{-5}	-1.8×10^{-6}	9.8×10^{-5}	-5.8×10^{-4}
	20.0	1.6×10^{-5}	5.1×10^{-4}	3.0×10^{-4}	4.2×10^{-5}	3.0×10^{-4}	-1.1×10^{-3}
	30.0	6.9×10^{-5}	2.2×10^{-3}	2.2×10^{-3}	-4.3×10^{-5}	-8.8×10^{-5}	-2.2×10^{-3}
384	1.0	1.9×10^{-9}	1.9×10^{-9}	6.2×10^{-9}	-2.0×10^{-7}	-2.2×10^{-7}	-3.4×10^{-6}
	5.0	7.2×10^{-9}	7.3×10^{-8}	6.0×10^{-7}	-1.2×10^{-7}	-1.3×10^{-7}	1.9×10^{-5}
	10.0	3.9×10^{-8}	4.2×10^{-8}	2.0×10^{-6}	-7.5×10^{-8}	-1.1×10^{-7}	1.3×10^{-4}
	20.0	8.8×10^{-7}	8.1×10^{-7}	2.3×10^{-5}	-5.3×10^{-7}	1.2×10^{-5}	4.6×10^{-4}
	30.0	4.1×10^{-6}	4.5×10^{-6}	3.2×10^{-6}	-4.8×10^{-6}	8.2×10^{-5}	1.0×10^{-3}
864	20.0	1.7×10^{-7}	1.7×10^{-7}	4.9×10^{-6}	-1.1×10^{-7}	-1.1×10^{-7}	2.0×10^{-4}
	30.0	7.3×10^{-7}	7.3×10^{-7}	1.7×10^{-5}	-9.9×10^{-7}	-9.8×10^{-7}	4.8×10^{-4}

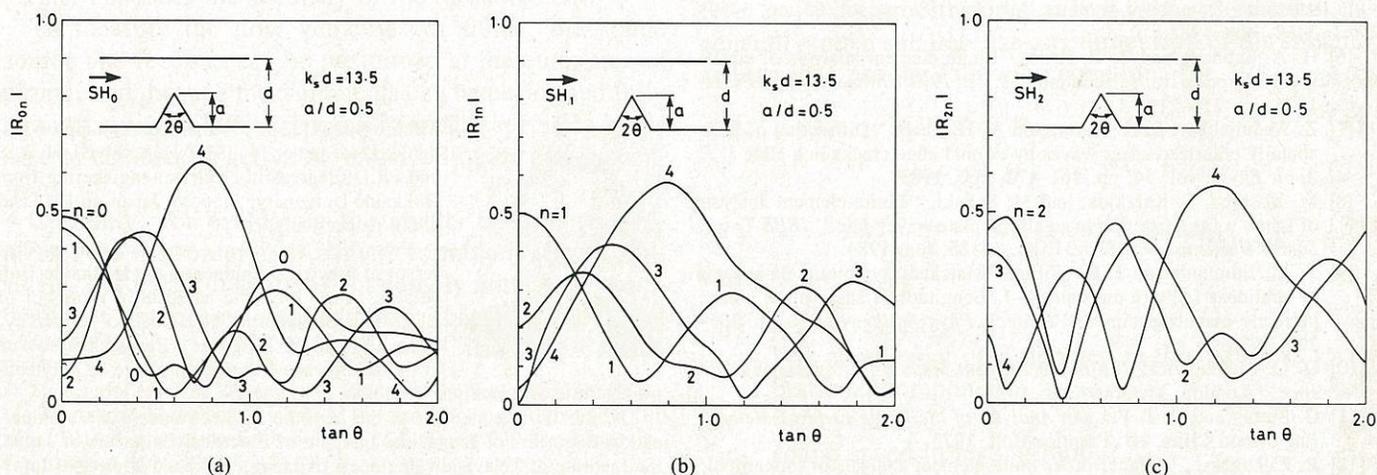


Fig. 3. Reflection coefficient of wedge-shaped crack for (a) zeroth, (b) first, and (c) second incident modes.

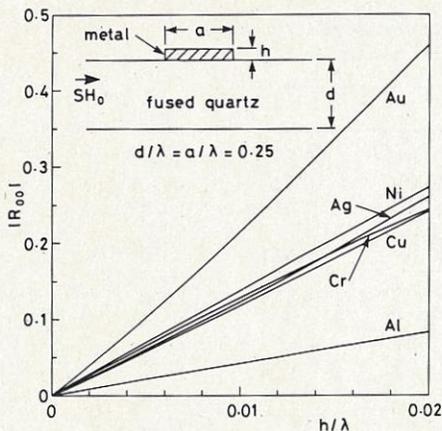


Fig. 4. Reflection coefficient of metal strip for zeroth incident mode.

V. CONCLUSION

A method of analysis, based on the finite-element approach and the analytical approach, was developed for the solution of scattering of SH waves in an elastic plate. This method is useful for inhomogeneous discontinuities of arbitrary shape. Numerical examples are presented for a step discontinuity, a wedge-shaped crack, and a metal strip.

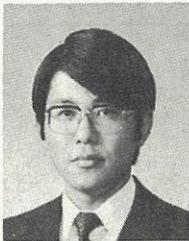
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